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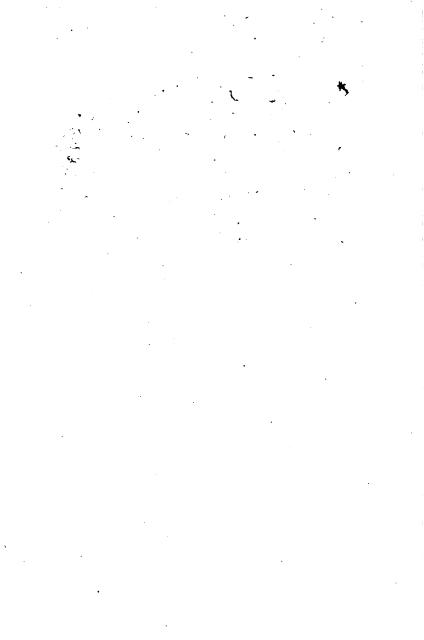


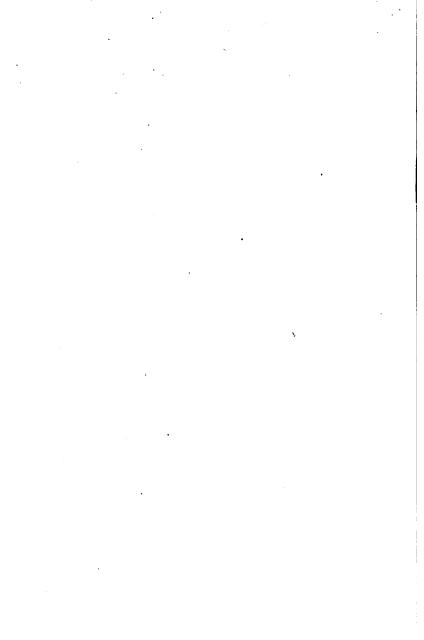
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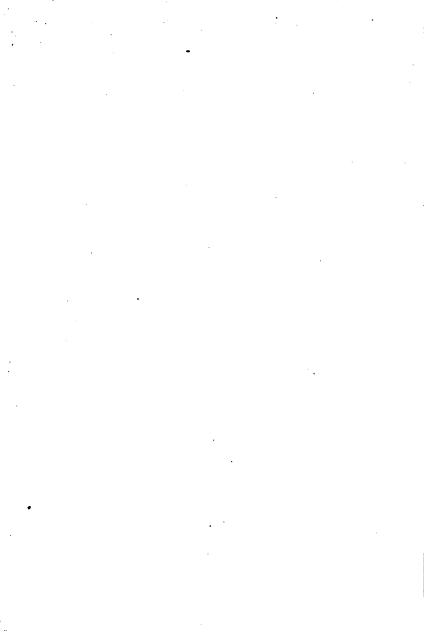
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HAND-BOOK OF TABLES

FOR

ELECTRICAL ENGINEERS.

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HAND-BOOK OF TABLES

FOR

ELECTRICAL ENGINEERS.

DEFINITIONS.

(From Brackett & Anthony's Physics.)

MEASUREMENTS.

All the phenomena of nature occur in matter and are presented to us in space and time. Time and space are fundamental conceptions; they do not admit of definition. Matter is equally indefinable; its distinctive characteristic is its persistence in whatever state of rest or motion it may happen to have, and the resistance which it offers to any attempt to change that state. This property is called inertia. If we adopt arbitrary units of length, time, and mass (or quantity of matter), we can express the measure of all other quantities in terms of these so-called fundamental units. A unit of any other quantity, thus expressed, is called a derived unit.

UNITS.

Units of Length.—The unit of length in the United States is the foot. The unit of length usually adopted in scientific work is the centimeter. It is the one-hundreth part of the length of a certain piece of platinum, declared to be the standard by legislative act, and preserved in the archives of France.

Unit of Time.—The unit of time is the mean time second, which is the **stan* of a mean solar day.

Unit of Mass.—The unit of mass in the United States is the avoirdupois pound. The unit of mass usually adopted in scientific work is the gram. It is equal to the one-thousandth part of a certain piece of platinum, called the kilogram, preserved as a standard in the archives of France. This standard was intended to be equal in mass to one cubic decimeter of water at its greatest density.

Dimensions of Units.—Any derived unit may be represented by the product of certain powers of the symbols representing the fundamental units of length, mass, and time. Any equation showing what powers of the fundamental units enter into the expression for the derived unit is called its dimensional equation. In a dimensional equation time is represented by T, length by L, and mass by M. To indicate the dimensions of any quantity the symbol representing that quantity is enclosed in brackets.

Mass.—In many cases it is convenient to speak of the quantity of matter in a body as a whole. It is then called the *mass* of the body.

Density.—The density of any substance is defined as the limit of the ratio of the quantity of matter in any volume within the substance to that volume, when the volume is diminished indefinitely.

Particle.—A body constituting a part of a material system, and of dimensions such that they may be considered infinitely small in comparison with the distances separating it from all other parts of the system, is called a particle.

Motion.—The change in position of a material particle is called its motion.

Path.—The moving particle must always describe a continuous line or path.

Velocity.—The rate of motion of a particle is called its velocity. If the particle move in a straight line, and describe equal spaces in any arbitrary equal times, its velocity is constant. A constant velocity is measured by the ratio of the

space traversed by the particle to the time occupied in traversing that space.

Speed.—If the path of the particle be curved, or if the spaces described by the particle in equal times be not equal, its velocity is variable and is called the *speed*.

Momentum.—The momentum of a body is a quantity which varies with the mass and with the velocity of the body jointly, and is measured by their product.

Acceleration.—When the velocity of a particle varies, its rate of change is called the *acceleration* of the particle. Acceleration is either positive or negative, according as the velocity increases or diminishes. If the path of the particle be a straight line, and if equal changes in velocity occur in equal times, its acceleration is *constant*.

Simple Harmonic Motion.—If a point moves in a circle with a constant velocity, the point of intersection of a diameter and a perpendicular drawn from the moving point to this diameter, will have a simple harmonic motion.

Period.—The *period* is the time between any two successive recurrences of a particular condition of the moving point.

Phase.—The *phase* is the interval of time, expressed as a fraction of the period, which has elapsed since the point has passed through the middle of its path in the positive direction.

Displacement.—The displacement is the distance from the center of motion. We further define rotation in the positive direction as that rotation in the circle which is contrary to the motion of the hands of a clock, or counter-clockwise. Motion from left to right in the diameter is also considered positive. Displacement to the right of the center is positive, and to the left is negative.

Force.—Whenever any change occurs or tends to occur in the momentum of a body, we ascribe it to a cause called a force.

Field of Force.—A field of force is a region such that a particle constituting a part of a mutually interacting system, placed at any point in the region, will be acted on by a force, and will move, if free to do so, in the direction of the force. The particle so moving would, if it had no inertia, describe

what is called a *line of force*, the tangent to which at any point is the direction of the force at that point.

Inertia.—Inertia is not of itself a force, but the property of a body, enabling it to offer a resistance to a change of motion.

Work.—When a force causes motion through space, it is said to do work.

Energy.—A body may, in consequence of its motion or position with respect to other bodies, have a certain capacity for doing work. This capacity for doing work is its energy. Potential energy is due to the position of the body. Kinetic energy is due to the motion of the body.

Difference of Potential.—The difference of potential between two points in a field of force is measured by the work done in moving a test unit of the quantity to whose presence the force is due from one point to the other.

Absolute Potential.—The absolute potential at a point in a field of force is measured by the work done in moving a test unit of the quantity to whose presence the force is due from an infinite distance to that point.

Equipotential Surface.—A surface to which the lines of force are perpendicular is called an equipotential surface.

Moment of Force.—The moment of force about a point is defined as the product of the force and the perpendicular drawn from the point upon the line of direction of the force.

Couple.—The combination of two forces, equal and oppositely directed, acting on the ends of a rigid bar, is called a couple.

Moment of Couple.—The moment of couple is the product of either of the two forces into the perpendicular distance between them.

Center of Inertia.—If we consider any system of equal material particles, the point of which the distance from any plane is equal to the average distance of the several particles from that plane, is called the center of inertia.

Center of Gravity.—When the force acting is the force gravity the center of inertia is usually called the center of gravity.

Moment of Inertia.—The moment of inertia of any body about an axis is defined as the summanation of the products of the masses of the particles making up the body into the squares of their respective distances from the axis.

Stress and Strain.—When a body is made the medium for the transmission of force, there is a *stress* in the medium. This stress is always accompanied by a corresponding change of form of the body, called a *strain*.

Set.—If the strain be carried beyond the limit of perfect elasticity, the body is permanently deformed. This permanent deformation is called set.

Solid.—A solid requires the stress acting upon it to exceed a certain limit before any permanent set occurs, and it makes no difference how long the stress acts provided it lie within the limits.

Fluid.—A fluid may be deformed by the slightest shearing stress, provided time enough be allowed for the movement to take place.

Specific Gravity.—The *specific gravity* of a body is defined as the ratio of its weight to the weight of an equal volume of pure water at a standard temperature.

Temperature.—Two bodies are said to be at the same temperature when, if they be brought into intimate contact, no heat is transferred from one to the other. A body is at a high temperature relatively to other bodies when it gives up heat to them.

Unit of Heat.—The English unit of heat is the heat necessary to raise one pound of water at 60° F., one degree Fahrenheit. The unit of heat generally adopted in scientific works is the heat required to raise the temperature of one kilogram of water from zero to one degree C. It is called the calorie.

Specific Heat.—The quantity of heat required to raise the temperature of one kilogram of a substance from zero to one degree is called the *specific heat* of the substance.

MAGNETISM.

Masses of iron ore are sometimes found which possess the property of attracting pieces of iron and a few other substances. Such masses are called natural magnets or lodestone. A bar of steel may be so treated as to acquire similar properties. It is then called a *magnet*.

Poles.—In an ordinary bar-magnet there are two small regions, near the ends of the bar, at which the attractive powers of the magnet are most strongly manifested. These regions are called the *poles* of the magnet.

Magnetic Axis.—A line joining these two regions is called the magnetic axis.

Unit Magnetic Pole.—If two perfectly similar magnets, infinitely thin, uniformly and longitudinally magnetized, be so placed that their positive poles are unit distance apart, and if these poles repel one another with unit force, the magnet poles are said to be of unit strength.

Magnetic Moment.—The product of the strength of the positive pole of a uniformly and longitudinally magnetized magnet into the distance between its poles is called its magnetic moment.

Intensity of Magnetization.—The quotient of the magnetic moment of such a magnet by its volume, or the magnetic moment of unit of volume, is called the *intensity of magnetization*.

Magnetic Shell.—A magnetic shell may be defined as an infinitely thin sheet of magnetizable matter, magnetized transversely; so that any line in the shell normal to its surfaces may be looked on as an infinitesimally short and thin magnet. These imaginary magnets have their like poles contiguous. The product of the intensity of magnetization at any point in the shell into the thickness of the shell at that point is called the strength of the shell at that point.

Declination.—The *declination* is the angle between the magnetic meridian, or the direction assumed by the axis of a magnetic needle suspended to move freely in a horizontal plane, and the geographical meridian.

Dip.—The dip is the angle made with the horizontal by the axis of a magnetic needle suspended so as to turn freely in a vertical plane containing the magnetic meridian.

Horizontal Intensity.—The horizontal intensity is the strength of the earth's magnetic field resolved along the horizontal line in the plane of the magnetic meridian.

ELECTRICITY IN EQUILIBRIUM.

Unit Quantity of Electricity.—Let there be two equal and similar charges concentrated at points unit distance apart in air, such that the repulsion between them equals the unit of force, then each of the charges is a unit charge, or a unit quantity of electricity.

Capacity.—The electrical capacity of a conductor is defined to be the charge which the conductor must receive to raise it from zero to unit potential, while all other conductors in the field are kept at zero potential.

Specific Inductive Capacity.—The fact that the capacity of a condenser of given dimensions depends upon the medium used as the dielectric was first discovered by Cavendish and afterwards rediscovered by Faraday. The property of the medium upon which this fact depends is called its specific inductive capacity.

ELECTRICITY IN MOTION.

Electromotive Force.—The power of maintaining a difference of potential is ascribed to an E. M. F. existing in the circuit.

Current.—The transfer of electricity in the circuit is called the electrical *current*, and the rate of transfer is called the current strength, and often simply the current. The current as here defined is independent of the nature of the conductor, and is the same for all parts of the circuit.

Electro-Magnetic Unit of Current.—That current is defined as the *unit current* which will set up the same magnetic field as that due to a magnetic shell of which the edge coincides with the circuit and the strength is unity.

Ohm's Law.—It was shown on theoretical consideration in 1827, by Ohm, of Berlin, that in a homogeneous conductor which is kept constant, the current varies directly with the difference of potential between the terminals.

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Resistance.—We may define the ratio of the electromotive force to the current in any circuit as the resistance in that circuit.

Specific Conductivity and Specific Resistance.—If two points be kept at a constant difference of potential, and joined by a homogeneous conductor of uniform cross-section, it is found that the current in the conductor is directly proportional to its cross-section and inversely as its length. The current also depends upon the nature of the conductor. If conductors of similar dimensions, but of different materials, are used, the current in each is proportional to a quantity called the specific conductivity of the material. The numerical value of the current set up in a conducting cube, with edges of unit length, by unit difference of potential between two opposite faces, is the measure of the conductivity of the material of the cube. The reciprocal of this member is the specific resistance of the material.

Kirchhoff's Laws.—Kirchhoff's laws may be stated as follows: (1.) The algebraic sum of all the currents meeting at any point of junction of two or more branches is equal to zero. This first law is evident, because, after the current has become steady, there is no accumulation of electricity at the junctions. (2.) The sum, taken around any number of branches forming a closed circuit, of the products of the currents in those branches into their respective resistances is equal to the sum of the electromotive forces in those branches. This law can easily be seen to be only a modified statement of Ohm's law.

Self-Induction.—When a current is set up in any circuit, the different parts of the circuit act on one another in the relation of primary and secondary circuits. In a long straight wire, for example, the current which is set up through any small area in the cross-section of the wire tends to develop an opposing electro-motive force through every other area in the same cross-section. The true current will thus be temporarily weakened, and will require a certain time to attain its full strength. On the other hand, when the circuit is broken, the induced electro-motive force is in the same direction as the electro-motive force of the circuit. Since the time occupied by the change of the true current from its full value to zero, when

the circuit is broken, is very small, the induced electro-motive force is very great. The current formed at breaking is called the *extra current*, and gives rise to a spark at the point where the circuit is broken. The extra current may be heightened by anything which will increase the change in the number of lines of force, as by winding the wire in a coil and by inserting in the coil a piece of soft iron. This action of a circuit on itself is called *self-induction*.

Induced Currents.—It has been shown by experiment that the movement of a magnet in the neighborhood of a closed circuit will give rise, in general, to an electro-motive force in the circuit, and that the current due to this electro-motive force will be in the direction opposite to that current which, by its action upon the magnet, would assist the actual motion of the magnet. This current is called an induced current. From the equivalence between a magnetic shell and an electrical current, it is plain that a similar induced current will be produced in a closed circuit by the movement near it of an electrical current or any part of one. Since the joining up or breaking the circuit carrying a current is equivalent to bringing up that same current from an infinite distance, or removing it to an infinite distance. it is further evident that similar induced currents will be produced in a closed circuit when a circuit is made or broken in its presence.

Ampere's Law for Mutual Action of Currents.—Ampere's first case of equilibrium shows that the forces due to two currents identical in strength and in position but opposite in direction are equal and opposite. Ampere's second case of equilibrium shows that the action of the elements of the curved conductor is the same as that of their projections on the straight conductor. The third case of equilibrium: the deduction from this observation is that no closed circuit tends to displace an element of current in the direction of its length. From the fourth case of equilibrium, is deduced the law that the force between two current elements is inversely as the square of the distance between them.

Electrolysis.—In certain cases, the existence of an electrical current in a circuit is accompanied by the decomposition into their constituents of chemical compounds forming part of the

circuit. This process is called *electrolysis*. Bodies which can be decomposed were called by Faraday, to whom the nomenclature of this subject is due, *electrolytes*. The current is usually introduced into the electrolyte by solid terminals called *electrodes*. The one at the higher potential is called the positive electrode or anode; the other, the negative electrode, or cathode. The two constituents into which the electrolyte is decomposed are called *ions*. One of them appears at the anode, and is called anion; the other, at the cathode, and is called the cation.

Faraday's Laws.—(1.) The amount of an electrolyte decomposed is directly proportional to the quantity of electricity which passes through it; or, the rate at which a body is electrolyzed is proportional to the current strength. (2.) If the same current be passed through different electrolytes, the quantity of each ion evolved is proportional to its chemical equivalent. If we define an electro-chemical equivalent as the quantity of any ion which is evolved by unit current in unit time, then the two laws may be summed up by saying: The number of electrochemical equivalents evolved in a given time by the passage of any current through any electrolyte is equal to the number of units of electricity which pass through the electrolyte in the given time.

LAWS OF DYNAMIC ELECTRIC CIRCUITS.

(From Clark & Sabine.)

- 1. The strength of a galvanic current is equal to the quantity of electricity flowing per second, and is the same in every point of an undivided conductor.
- 2. The strength of the current is proportional to the electromotive force, when the resistance remains constant.—(Ohm.)
- 3. The current strength is inversely proportional to the resistance of the conductor, and therefore directly proportional to its conducting power.—(Ohm.)
- 4. The current strength is equal to the electromotive force divided by the resistance.
- 5. The current strength obtained with a battery of given surface is at its maximum when the plates are so divided that the internal resistance of the battery is equal to that of the circuit without.—(Jacobi.)

- 6. The sum of the current strengths in all those wires which converge to a point is equal to nothing.—(Kirchhoff.)
- 7. The sum of all the products of the intensities and resistances in all the wires which form an enclosed figure is equal to the sum of all the electromotive forces in the same circuit.—
 (Kirchhoff.)
- 8. If, in any system of circuits, containing any electromotive forces, a conductor exists in which the current strength is equal to nothing, the currents in the remaining circuits will not be altered, in the least, if the circuit of the conductor in question be separated or removed together with whatever electromotive force it may contain.
- 9. If the conductor in question contains no electromotive force, the currents will not be altered if, after its removal, the points between which it previously existed be connected directly with each other.—(Bosscha.)
- 10. If, on the other hand, it contained an electromotive force, the points can only be joined again, whilst retaining the balance, by inserting between them an equivalent electromotive force, but irrespective of the resistance which may accompany it.—(Bosscha.)
- 11. In a system of linear conductors, containing electromotive forces, the current set up in any conductor, A, by any electromotive force contained in any other conductor, B, will be identically the same as that which would be set up in B by an equal electromotive force in A.—(Bosscha.)
- 12. If, in a system of electromotive forces and conductors, there be two of the latter, say A and B, in which the electromotive force in A occasions no current in B, whatever current may be circulating in B will not be affected if A be interrupted or removed; nor will the current in A be altered if B be interrupted or removed, however the electromotive forces in the other circuits may be arranged.—(Bosscha.)
- 13. In any linear conductor through which a current of electricity is flowing, the difference of potential, between any two points with a given resistance between them is the same as that between any other two points having between them an equal resistance.—(Ohm.)

LAWS OF VOLTAIC INDUCTION.

- 1. In a secondary closed circuit, the excited induction current is proportional to the current strength in the primary circuit.
- 2. The induction currents arising from the action of a galvanic current upon itself are, both on breaking and making the circuit, equally great so long as the inducing current strength remains equal.—(Edlund.)
- 3. When a metallic closed circuit and a conductor through which an electric current is circulating are either brought nearer to each other or separated, a current is induced in the metallic closed circuit. This current is in the reverse direction to that which would have been necessary to effect the approach or separation of itself.—(Lenz.)
- 4. The electromotive force which a magnet excites in a helix of wire is, other things being equal, proportional to the number of convolutions of the wire.—(Lenz.)
- 5. The electromotive force which a magnet excites in a surrounding helix is equal, whatever may be the radius of the coil. Therefore, the currents induced in the different rings of wire are inversely proportional to their diameters.—(Lenz.)
- 6. The electromotive force excited by a magnet in a helix of given number of turns is the same, whatever may be the thickness or conducting power of the wire.
- 7. The strengths of the induction currents in different spirals of equal number of turns are proportional to their conducting powers.
- 8. The longer the connecting wires are, so much more numerous should be the convolutions in order to obtain the maximum current.
- 9. The more turns which can be put next to each other close by the magnet or magnetized armature, the fewer turns will be necessary to give a maximum current.
- 10. The maximum of an induction current is proportional to the strength of the inducing magnet.—(Lenz.)
- 11. The retardation of the development of magnetism in soft iron cores which are wholly covered by helices, depends principally upon the opposite currents induced in the helices themselves. The magnetism of the simultaneous currents induced in the periphery of the core, and the coercive force of iron, are of less influence.—(Beets.)

- 12. The retardation of the disappearance of the magnetism from soft iron cores which are wholly covered with galvanic helices, depends however principally upon the formation of currents in the periphery of the soft iron cores.—(Beets.)
- 13. The retardations of development and disappearance of magnetism in soft iron cores which are only partially covered with helices, depends principally upon the magnetic inertia of the iron.

LAWS OF MAGNETISM.

- 1. A magnetic field is any space in the neighborhood or under the influence of a magnet.—(B. A. Report.)
- 2. The direction of the force in the field is the direction in which any pole is urged by the magnetism of the field; this is the direction which a short, balanced, freely-suspended magnet would assume.
- 3. A uniform magnet field is one in which the intensity is equal throughout, and hence the lines of force parallel.— (Thomson.)
- 4. Opposite poles attract each other; similar poles repel each other.
- 5. The forces directed from any magnetic point upon equal masses are reciprocally proportional to the square of the distance.—(Musschenbroek.)
- 6. When two magnets are very small and the distance between them very great in proportion to their length, the magnetic action between them is reciprocally proportional to the cube of their distance.—(Gauss.)
- 7. The force directed from any magnet point upon any other mass upon which it acts is reciprocally proportional to the square of the distance. The total action between them both is, however, reciprocally proportional to the third power of the distance, when the latter is great.—(Gauss.)
- 8. Magnetic forces between a suspended magnet and any mass upon which it acts are proportional to the square of the number of oscillations which (under their mutual action alone) the same magnet makes in a given time.—(Coulomb.)
- 9. Magnetic forces between a suspended magnet and any magnetic mass are inversely proportional to the square of the time which the suspended magnet takes to complete one oscillation.—(Coulomb.)

- 10. The attraction of a magnet for an armature is proportional to the square of its free magnetism.
- 11. The magnetism excited at any given transverse section of a magnet is proportional to the square root of the distance between the given section and the nearest end of the magnet.—(Dub.)
- 12. The free magnetism at any given transverse section of a magnet is proportional to the difference between the square root of half the length of the magnet and the square root of the distance between the given section and the nearest end.— (Dub.)

LAWS OF ELECTRO-MAGNETISM.

- 1. If we imagine a positive current to flow through the axis of an ordinary corkscrew, the tip of the latter, in any position, represents the direction assumed by the north end of a magnet. If a current circulate in the corkscrew-helix in the direction in which it is turned, a soft iron core in its center will have its north end towards the tip.—(L. Clark.)
- 2. The total effect of any infinitely long and straight conductor upon any magnetic element is inversely proportional to the perpendicular distance between element and the conductor.

 —(Biot and Savart.)
- 3. A magnetic element in the axis of a circular current is attracted or repelled from the center with a force which is directly proportional to the superficial content of the circle and inversely to the third power of the distance of the element from the periphery.—(Weber.)
- 4. A circular current flowing in the plane of the magnetic meridian deflects a magnetic needle (which is infinitely short in comparison with the radius of the current) so that the tangent of the angle of deflection is proportional to the strength of the current.—(Weber.)
- 5. The magnetic intensity of a single deflected needle is without influence upon the angle of deflection.—(Weber.)
- 6. If the circular conductor be turned after the deflected needle until the latter again coincides with the plane of the former, the current strength is proportional to the sine of the angle through which the conductor is turned.
- 7. In electro-magnets, the south pole is always found at that end where the positive current enters a right-handed helix.

- 8. The free magnetism of the end-faces of an electro-magnet is proportional to the current strength in its helix.—(Dub.)
- 9. The attraction between electro-magnets is proportional to the square of the strength of the magnetizing current.
- 10. The material and the thickness of the helix wire of an electro-magnet are, when the current is equal, without influence upon its magnetism.—(Lenz.)
- 11. The free magnetism of an electro-magnet, with a given current strength, is directly proportional to the number of turns of its helix.—(Jacobi.)
- 12. Its attraction is proportional to the square of the number of convolutions.—(Dub.)
- 13. The attraction between two electro-magnets is proportional to the sum of the products of the current strength and number of convolutions of both helices.
- 14. The force with which a bar of soft iron is attracted by a galvanic helix is proportional to the square of the product of current strength and number of convolutions of the helix.— (Dub.)
- 15. The force with which a saturated steel magnet is attracted by a galvanic helix is directly proportional to the product of the current strength and number of convolutions.
- 16. The free magnetism of a solid cylindrical soft iron core of given length is, other things being equal, proportional to the square root of its diameter.—(Nicklès.)
- 17. The free magnetism at the poles of a horse-shoe magnet is, other things being equal, proportional to the square root of the length.
 - 18. The free magnetism of any given transverse section of an electro-magnet is proportional to the difference between the square root of half the length and the square root of the distance of the given section from the nearest end.—(Dub.)
 - 19. The poles of an electro-magnet attract most favorably when their faces have the same area as the transverse section of the magnet.
 - 20. The attraction between an electro-magnet and its armature increases when the mass of the armature is increased.
 - 21. The magnetizing powers of coils of one and the same metal, with the same surface of battery plates, arranged so as to give a maximum strength of current in each case, are as the square roots of the weights of the metallic wire used.—(Menzzer.)

FORMULÆ AND DIMENSIONS OF UNITS.

The formulæ of these tables are the algebraic expression of the definitions which have preceded. In the case of the Fundamental Units and the Derived Mechanical Units they are in the form in which they are commonly used for calculation, but in the case of the Magnetic and Electrical Units more special expressions are preferred, ones in which the force, F, is expressed in its mechanical equivalent involving the constants of conversion.

FUNDAMENTAL UNITS.

Unit.	Formula.	Dimensions.
Length Mass Time	m.	L M

DERIVED MECHANICAL UNITS.

Unit.	Formula.	Dimensions.
Area	A = S ²	L²
Volume	$V = s^3$	Гз
Velocity	$V = \frac{s}{t}$	L T - 1
Acceleration	$\mathbf{f} = \frac{\mathbf{v} - \mathbf{v_0}}{\mathbf{t}}$	LT-2
Momentum	$m v = \frac{m s}{t}$	M L T - 2
Density	$d = \frac{m}{V}$	M L - 3
Force	$\mathbf{F} = \mathbf{m} \; \mathbf{f} = \mathbf{m} \; \frac{\mathbf{v} - \mathbf{v_0}}{\mathbf{t}}$	M L T - 2
Weight	$\mathbf{w} = \mathbf{m} \mathbf{f} = \mathbf{m} \mathbf{g}$	MLT-2
Work	W = Fs = mfs	M L2 T - 2

DERIVED MECHANICAL UNITS—Continued.

Unit.	Formula.	Dimensions.
Simple Harmonic Motion	$s = a \cos \frac{2 \pi t}{T}$	
	$v = -\frac{2\pi a}{T} sine^{\frac{2\pi t}{T}}$	
	$f = -\frac{4\pi^2}{T^2}$ a cos. $\frac{2\pi t}{T}$	
Kinetic Energy	$K = \frac{m v^2}{2}$	M L ² T - ²
Potential Energy	$P = \sum m f s$	M L 2 T - 2.
Energy	$E = K + P = \frac{m v^2}{2} + \Sigma m fs$	M L ² T ^{- 2}
Moment of Couple	= F s = m f s	M L2 T - 2
Angular Velocity	$* = \frac{1}{t}$	T-1
Angular Acceleration	$* = \frac{1}{t^2}$	T - 2
Moment of Inertia	$I = \Sigma m s^2$	M L ²
Moment of Momentum	$=\Sigma \frac{m S^2}{t}$	M L2 T - 1
Intensity of Pressure	$\frac{\mathbf{F}}{\mathbf{A}} = \frac{\mathbf{m}}{\mathbf{s}^2} \mathbf{f}$	M L - 1 T - 2

DERIVED MAGNETIC UNITS.

Unit.	Formula.	Dimensions.
Magnetic Pole	$= \sqrt{F_{S^2}}$	M2 L2 T-1
Magnetic Moment	$=8 \sqrt{\mathbf{F} \mathbf{s}^2}$	M ¹ / ₂ L ⁵ / ₂ T - 1
Intensity of Magnetization	$=8\frac{1/\overline{F}s^{\frac{2}{3}}}{s^{3}}$	M2 L-1 T-1
Magnetic Density	$=\frac{\sqrt{F s^2}}{s^2}$	M1 L-1T-1
Magnetic Shell	$=\frac{8^3\sqrt{F_8}}{8^3}$	M ¹ L ¹ T ' 1
Horizontal Intensity	$= \frac{\mathbf{F}}{\mathbf{V}\mathbf{F}\mathbf{s}^2}$	M2 L - 2 T - 1
Magnetic Potential	$=\frac{\mathbf{F}\mathbf{s}}{\sqrt{\mathbf{F}\mathbf{s}^2}}$	M2 L2 T-1

^{*}In these formulæ the angles are measured in radians.

DERIVED ELECTROSTATIC UNITS.

Unit.	Formula.	Dimensions.
Current	$=\frac{\sqrt{F}s^2}{t}$	M ¹ / ₂ L ³ / ₂ T - 2
Electromotive force	$=\frac{\mathbf{W}}{\mathbf{V}\mathbf{F}\mathbf{S}^2}$	M ¹ L ¹ T - 1
Resistance	$\frac{\mathbf{W}}{\mathbf{V}\mathbf{F}\mathbf{s}^2} \div \frac{\mathbf{V}\mathbf{F}\mathbf{s}^2}{\mathbf{t}}$	Γ-17
Quantity	$=\sqrt{\overline{F}\overline{s^2}}$	M ¹ / ₂ L ³ / ₂ T-1
Capacity	$\sqrt{\mathbf{F}\mathbf{s}^2} \div \frac{\sqrt{\mathbf{F}\mathbf{s}^2}}{\mathbf{t}}$	L
Difference of Potential	$\frac{\mathbf{W}}{\mathbf{V}\mathbf{F}\mathbf{s}^2}$	M ¹ / ₂ L ¹ / ₂ T-1
Specific Inductive Capacity	$\frac{\sqrt{\mathbf{F}\mathbf{g}^2}}{\sqrt{\mathbf{F_1}\mathbf{s_1}^2}}$	

DERIVED ELECTRO-MAGNETIC UNITS.

Unit.	Formula.	Dimensions.
Current	Fs	M ¹ / ₂ L ¹ / ₂ T - 1
Electromotive force	W Fst	M ¹ / ₂ L ³ / ₂ T - 2.
Resistance	$\frac{\mathbf{W}}{\mathbf{F}\mathbf{s}\mathbf{t}} \div \mathbf{F}\mathbf{s}$	L T - 1
Quantity	Fst	$M^{\frac{1}{2}}L^{\frac{1}{2}}$
Capacity	$\mathbf{Fst} + \frac{\mathbf{W}}{\mathbf{Fst}}$	L-1T-2
Difference of Potential	W Fst	M2 L2 T-2

TABLE FOR TRIGONOMETRICAL TRANSFORMATIONS.

Cosine. tangent. Coangent. Coangent. Cocant. Coccant. Coccant. Coccant. Coccant. Coccant. Coccant. Cosine x $y'1 + \tan^3 x$ $y'1 + \cot^3 x$ y'	-
$ \begin{array}{c ccccccccccccccccccccccccccccccccccc$	Sille.
$ \frac{1}{\sqrt{1 + \tan z}} \frac{\cot z}{\sqrt{1 + \cot z}} \frac{1}{x} \frac{1}{\sec z} $ Tangent $x \frac{1}{\cot z}$ $y = \frac{1}{\sqrt{1 + \cot z}}$ $y = \frac{1}{\sqrt{1 + \cot z}} $ $ \frac{1}{\sqrt{1 + \tan z}} \frac{1}{x} \frac{1}{\sqrt{1 + \cot z}} \frac{1}{x} \frac{1}{\sqrt{1 + \cot z}} $ Secant $x \frac{\sqrt{1 + \tan z}}{\cot x}$ $y = \frac{1}{\sqrt{1 + \cot z}}$	Sinex
Tangent x	$V \frac{1-\sin x}{x}$
$\frac{1}{\tan x} \qquad \text{Cotangent } x \qquad \frac{1}{\sqrt{86c^3 x - 1}} \qquad V$ $\frac{\sqrt{1 + \tan^3 x}}{\sqrt{1 + \tan^3 x}} \qquad \frac{\sqrt{1 + \cot^3 x}}{\sqrt{1 + \cot^3 x}} \qquad \frac{86c. x}{\sqrt{86c. x - 1}}$	$\frac{\sin x}{\sqrt{1-\sin^2 x}} \qquad \frac{\sqrt{1}}{\sqrt{1-\sin^2 x}}$
$\frac{V1 + \tan^{3}x}{V1 + \tan^{3}x} \qquad \frac{V1 + \cot^{2}x}{\cot x}$ Becant x $\frac{V1 + \tan^{3}x}{\tan x} \qquad V1 + \cot^{3}x \qquad \frac{\sec x}{V\sec^{3}x - 1}$	$\frac{\gamma 1 - \sin z}{\sin x}$
$\frac{\sqrt{1+\tan^2x}}{\tan x} \qquad \frac{\sqrt{1+\cot x^2x}}{\sqrt{\sec^2x-1}}$	$\frac{1}{V 1 - \sin^2 x}$
	$\frac{1}{\sin x}$

MEASURES OF LENGTH.

NAME OF UNIT.	Inches.	Feet.	Yards.	Meters.	Chrins.	Kilometers.	Miles.	Knots.
Inches		.083 33	.027 78	.025 399	.001 263	.000 025 4	.000 015	8 .000 013 7
Feet	12,000 00	_	333 33	304 795	015151	.000 304 8	.000	.000 164 3
Yards	36.000 00			914 384	.045 454	.000 914 4	.000 568	0004928
Meters	39.370 79	3.280 90	1,093 63	1.	.049 710	.001 000 0	.000 621	0005390
Chains	792.000 00	_	••	20,116437	-	.020 116 4	.012500	0108427
Kilometers	39 370.79	3 280.899 16	8	1 000 000 000	19.710 479	, -i	.621 381	.539 001 0
Miles	63 360.000 00	00 5 280.000 00	1 760.000 00	1 609.314 926 80.000 000	30.000 000	1.6093149	<u>-</u> ;	.867 422 3
Knots	73 044.000 00	6 087.000 00	2 029.000 00	$044.000\ 00 6\ 087.000\ 00 2\ 029.000\ 00 1\ 855.284\ 082 92.227\ 272$	9.227 272	1.8552840	1.1528409	1.

LOGARITHMS OF MEASURES OF LENGTH.

NAME OF UNIT.	Inches.	Feet.	Yards.	Meters.	Chains.	Kilometers.	Miles.	Knots.
Inches	0.000 0000	$\bar{2}.920801$	2.443 732	2.404 817	3.101 403	5.404 817	5.198 657	$\overline{5}.136721$
Feet	1.079 181	0.000 0000	1.522874	$\overline{1.484007}$			4.277 380	4.215638
Yards	1.556 303	0.477 121	0.000 0000	$\overline{1.961128}$	$\overline{2.657572}$	$\overline{4.961128}$	4.754 501	4.692671
Meters	1.595 174	0.515993	0.038 871	0.000 000			4.793301	4.731589
Chains	2.898 725	1.819 544	1.342 423	1.303551	0.000 000.0		2.096 910	$\overline{2}.035138$
Kilometers	4.595 174	3.515 993	3.038 871	3.000 000	1.696 448	0.000 0000	1.793357	$\overline{1.731589}$
Miles	4.801815	3.722 634	3.245513	3.206 641	_	0.206641	0.000 0000	1.938 230
Knots	4 863 585	3.784 403	3.307 282	3.268 410	1.964859	0.268411	0.061 768	0.000 0000

MEASURES OF AREA.

NAME OF UNIT.	Square	Square	Square	Square	Square
	Centimeters.	Inches.	Feet.	Yards.	Meters.
Square Centimeters. Square Inches. Square Feet. Square Yards. Square Meters.	1, 6.451 6 928.989 8 361, 10 000.000 0	.155 1. 144.000 1 296.000 1 550.030	.001 076 .006 944 1. 9.000 000	.000 119 61 .000 771 60 .111 111 11 1.196 100 00	.000 100 .000 645 .092 898 .836 100

LOGARITHMS OF MEASURES OF AREA.

NAME OF URIT.	Square Centimeters.	Square Inches.	Square Feet.	Square Yards.	Square Meters.
Square Centimeters	0.000 000	1.190 332	3.031 812	4.077 767	4.000 000
Square Inches	0.809 667	0.000 0000	$\bar{3}.841610$	4.887 392	4.809 560
Square Feet	2.968 010	2.158 362	0.000 0000	$\overline{1.045757}$	2.968 006
Square Yards	3.922 258	3.112 605	0.954 242	000 0000	$\overline{1.922258}$
Square Meters	4.000 000	3.190340	1.031974	0.077 767	0.000 000

MEASURES OF VOLUME.

NAME OF UNIT.	Cubic Centimeters.	Cubic Inches.	Liters.	Gallons.	Cubic Feet.	Cubic Yards.	Cubic Meters
Cubic Centimeters Cubic Inches Liters Gallons Cubic Feet. Cubic Yards Cubic Meters	1. 16.386 1 000.000 3 785.210 28 315.336 764 505.000 1 000 000.000	.061 02 1. 61.027 00 231.000 00 1 728.000 00 46 656.000 00 61 027.000 00	.001 .016 39 1. 3.785 21 28.315 33 764.505 1 000.	.000 264 .004 33 .264 189 1. 7.480 5 201.974 264.189	.000 035 3 .000 578 7 .035 317 .133 681 1. 27.000 0 35.316 9	.000 001 31 .000 021 40 .001 308 .004 952 .037 037 03	.000 001 0 .000 016 4 .001 000 0 .003 785 2 .028 315 3 .764 505

LOGARITHMS OF MEASURES OF VOLUME.

Cubic Meters.			3.000 000				
Cubic Yards.	$\overline{6.11727}$	5.330414	$\bar{3}.116608$	3.694 78]	2.568 636	0.000 000	0.116608
Cubic Feet.	5.547 775	4.762 453	2.547 983	$\overline{1.126009}$	0.000 0000	1.431364	1.547983
Gallons.	4.421 604	3.636 488	$\overline{1.421914}$	0.000 0000	0.873931	2.305 296	2.421 914
Liters.	3.000 000	2.214579	0.000 0000	0.578090	1.452022	2.883 396	3.000 000
Cubic Inches.	2.785 472	0.000 0000	1.785522	2.363612	3.237 544	4.668 908	4.785522
Cubic Centimeters.	0.000 000	1.214 474	3.000 000	3.578 090	4.452 022	5.883 397	6.000 000
NAME OF UNIT.	Cubic Centimeters	Cubic Inches	Liters	Gallons	Cubic Feet	Cubic Yards	Cubic Meters

MEASURES OF WEIGHT.

NAME OF UNIT.	Grains.	Grams.	Ounces Avoirdupois.	Pounds Troy.	Pounds Avoirdupois.	Kilograms.	Long Tons.
sı	1.	.064 80	.002 28	.000 174	.000 143	.000 064 8	
rama	15.432		.035 27	.002 68	.002 204	.001 000 0	
Avd	437.500	28.350	ı.	.075 95	.062 500	.028 350	.000 028
Troy	5 760.000	373.250	13.166	-:	.822 857	.373 250	.000367
Lbs. Avd	2 000:000	453.603	16.000	1.2153	,	.453 603	.000 447
rams.	15 432.	1 000:000	35.273	2.6792	2.204 571		.000 984
Tons.	15 680 000.000	1 016 070.502	35 840.000	2 722.222 2	2 240.000 000	1 016.070 502	1.

LOGARITHMS OF MEASURES OF WEIGHT.

Long Tons.				$\overline{4.564666}$			
Kilograms.	5.811 575	3.000 000	$\overline{2}.452553$	$\overline{1.572000}$	$\overline{1.656676}$	0.000 000	3.006924
Pounds Avoirdupois.			$\overline{2}.795880$				
Pounds Troy.			$\bar{2}.880528$				
Ounces Avoirdupois.	$\bar{3}.357935$	2.547405	0.000 000	1.119 454	1.204120	1.547 442	4.554 368
Grams.	$\bar{2}.811575$	0.000 000	1.452 553	2.572 000	2.656 676	3.000 000	6.006 924
Grains.	0.000 000	1.188422	2.640 978	3.760 422	3.845 098	4.188 422	7.195346
NAME OF UNIT.	Grains	Grams	Oz. Avd	Lbs. Troy	Lbs. Avd	Kilograms.	Long Tons.

MEASURES OF PRESSURE.

NAME OF UNIT.	Atmos- pheres.	Pounds on Square Inch.	Inches of Mercury.	Feet of Water at 60° F.	Millimeters of Mercury.	Pounds on Square Foot	Kilograms on Square Meter.
Atmospheres Pounds on Square Inch Inches of Mercury. Feet of Water at 60° F. Millimeters of Mercury. Pounds on Square Foot Kilograms on Square Meter	1. .068 03 .033 42 .029 47 .001 316 .000 472 6	14.7 1. 491 3 .433 2 .019 34 .006 947 .001 423	29.922 2.036 1. .881 8 .039 37 .014 14	33.93 2.309 1.134 1. .044 64 .016 03 .003 283	760.000 25.398 22.399 1. 359.2 .073.55	2 116,000 143,946 70,700 62,363 2,784 1.	10 333 000 702.925 345.331 304.565 13.596 4.883

LOGARITHMS OF MEASURES OF PRESSURE.

NAME OF UNIT.	Atmos- pheres.	Pounds on Square Inch.	Inches of Mercury.	Feet of Water at 60° F.	Millimeters of Mercury.	Pounds on Square Foot.	Kilograms on Square Meter.
Atmospheres	0.000 0000	1.167 317	0.000 000 1.167 317 1.475 991 1.530 584	1.530 584	2.880 814	3.325 516	4.014 226
Pounds on Square Inch	2.832 700	0.000 0000	2.832 700 0.000 000 0.308 778 0.361 897	0 361 897	1.713 491	2.158200	2.846 909
Inches of Mercury	2.524 006	1.691 347	2.524 006 1.691 347 0.000 000 0.054 613	0.054613	1.404 800	1.849 419	2.538 238
Feet of Water at 60° F	2,469 380	2,469 380 1.636 688	1.945 370 0 000 000	0000000	1.350 229	1.794 927	2.483679
Millimeters of Mercury	3.119256	2.286456	3.119 256 2.286 456 2.595 165 2.649 735	2.649 735	0.000 000	0.444 669	1.133413
Pounds on Square Foot	4.674 494	3.841 797	4.674 494 3.841 797 3.150 449 2.204 934	2.204934	1 555 336	0.000 000	0.688 687
Kilograms on Square Meter	5.985 741	3.153 205	5 985 741 3.153 205 3.461 649 3.516 271	3.516 271	2.866 642	$\bar{1}.311330$	0.000 000

TELEGRAPH KNOTS INTO MILES.

Table for the Conversion of Knots of 2029 Yards into Statute Miles of 1760 Yards.

Knots.	0	-	61	တ	4	<u>ب</u>	ဖ	-	x 0	5 3
0		1.1528	2.305 7		4.6114	5.7642	6.917 0	8.0699	9.212.7	10.375 6
10	11.528 4	12.6812	13.8341		16.1398	17.2926	18.4454	19.5983	20.7511	21.9040
20	23.0568	24.2096	25.362 5	•	27.668 2	28.821 0	29.9738	31.1267	32.279 5	33.4324
30	34.585 2	35.7380	36.8909	•	39.1966	40.3494	41.5022	42.6551	43.8079	44.9608
9	46.1136	47.2664	48.4193	49.5721	50.7250	51.8778	53.0306	54.1835	55.3363	56.4892
22	57.6420	58.7948	59.947 7	61.1005	62.2534	63.4062	64.5590	65.7119	66.8647	68.0176
99	69.1704	70.323 2	71.4761	72.6289	73.7818	74.934 6			78.393 1	79.5460
20	80.6988	81.8516	83.004 5	84.1573	85.310 2	86.4630			89.921 5	91.0744
08	92.227 2	93.380 0	94.5329	95.685 7	96.838 6	97.9914			101.4499	102.6028
8	103.7556	104.908 4	106.0613	107.2141	108.3670	109.5198			112.9783	114.1312

DECIMAL EQUIVALENTS OF PARTS OF AN INCH.

ths.	₃¹₂ds.	daths.	Mils.	∤sths.	₃}ds.	åths.	Mils.
		1	15.625			33	515.625
	1	2	31.250		17	34	531.250
,	2	2 3 4	46.875	9	18	35 36	546.875
1	z		62.500	9	18		562.500
		5	78.125			37	578.125
j	3	6	93.750		19	38	593.750
	_	7	109.375			39	609.375
2	4	8	125.000	10	20	40	625.000
		9	140.625			41	640.625
	5	10	156.250	i I	21	42	656.250
		11	171.875			43	671.875
3	6	12	187.500	11	22	44	687.500
		13	203.125			45	703.125
	7	14	218.750		23	46	718.750
		15	234.375			47	734.375
4	8	16	250.000	12	24	48	750.000
		17	265.625			49	765.625
	9	18	281.250		25	50	781.250
		19	296.875			51	796.875
5	10	20	312.500	13	26	52	812.500
		21	328.125			53	828.125
	11	22	343.750		27	54	843.750
		23	359.375			55	859.375
6	12	24	375 000	14	28	56	875.000
		25	390.625			57	890.625
	13	26	406.250		29	58	906.250
_ [27	421.875			59	921.875
7	14	28	437.500	15	30	60	937.500
		29	453.125	<u> </u>		61	953.125
	15	30	468.750	l l	31	62	968.750
_		31	484.375			63	984.375
8	16	32	500.000	16	32	64	1000.000

TABLE OF THE DENSITY AND VOLUME OF WATER FROM 9° C. TO 100° C.

According to M. Despretz (the density and volume at 4° taken as unity).

Temperature.	Volume.	Density.	Temperature.	Volume.	Density.
9°	1.001 631 1	0.998 371	15°	1.000 875 1	0.999 125
8	1.001 373 4	0.998 628	16	1.001 021 5	0.998 979
-7 -6 -5	1.001 135 4	0.998865	17	1.001 206 7	0.998 794
6	1.000 918 4	0.999 082	18	1.001 39	0.998 612
5	1.000 698 7	0.999 302	19	1.001 58	0.998 422
-4	1.000 561 9	0.999 437	20	1.001 79	0.998 213
3	1.000 422 2	0.999 577	21	1.002 00	0.998 004
-2	1.000 307 7	0.999 692	22	1.002 22	0.997 784
—1	1.000 213 8	0.999 786	23	1.002 44	0.997 566
0	1.000 126 9	0.999 873	24	1.002 71	0.997 297
1	1.000 073 0	0.999 927	25	1.002 93	0.997 078
$\frac{2}{3}$	1.000 033 1	0.999 966	26	1.003 21	0.996 800
3	1.000 008 3	0.999 999	27	1.003 45	0.996 562
4 5	1.000 000 0	1.000 000	28	1.003 74	0.996 274
5	1.000 008 2	0.999 999	29	1.004 03	0.995 986
6	1.000 030 9	0.999 969	30	1.004 33	0.995 688
7	1.000 070 8	0.999 929	40	1.007 73	0.992 329
8	1.000 121 6	0.999 878	50	1.012 05	0.988 093
9	1.000 187 9	0.999 812	60	1.016 98	0.983 303
10	1.000 268 4	0.999 731	70	1.022 55	0.977 947
11	1 000 359 8	0.999 640	80	1.028 85	0.971 959
12	1.000 472 4	0.999 527	90	1.03566	0.965 567
13	1.000 586 2	0.999 414	100	1.043 15	0.958634
14	1.000 714 6	0.999 285			

THE COMPARISON OF DIFFERENT THERMOMETERS.

Two temperatures may be easily obtained and are constant when produced, namely, the boiling point of water and the melting point of ice.

On the scale of the Reaumur thermometer the boiling point is called 80° and the melting point of ice 0°. Zero is also the same point on the Centigrade scale, but the boiling point is placed at 100°. On the Fahrenheit scale the melting point of ice is placed at 32°, 0° being considered at the time the lowest obtainable temperature, and the boiling point is called 212°.

Therefore, if we wish to convert a temperature on any one of these scales to the equivalent temperature on another, we use one of the following formulæ:

$$t^{\circ}R. = \frac{\pi}{4}t^{\circ}C. = 32 + \frac{\pi}{4}t^{\circ}F.$$

 $t^{\circ}C. = \frac{\pi}{4}t^{\circ}R. = 32 + \frac{\pi}{4}t^{\circ}F.$
 $t^{\circ}F. - 32^{\circ}F. = \frac{\pi}{4}t^{\circ}R. = \frac{\pi}{4}t^{\circ}C.$

TABLE OF COMPARISON OF DIFFERENT THERMOMETERS.

Fahrenheit.	Reaumur.	Centigrade.	Fahrenheit.	Reaumur.	Centigrade.	Fabrenbeit.	Reaumur.	Centigrade.	Fahrenheit.	Reaumur.	Centigrade.
212	80.0	100.0	192	71.1	88.8	172	62.2	77.7	152	53.3	66.6
211	79.5	99.4	191	70.6	88.3	171	61.7	77.2	151	52.8	66.1
210	79.1	98.8	190	70.2	87.7	170	61.3	76.6	150	52.4	65.5
209	78.6	98.3	189	69.7	87.2	169	60.8	76.1	149	52.0	65.0
208	78.2	97.7	188	69.3	86.6	168	60.4	75.5	148	51.5	64.4
207 206 205 204 203	77.7 77.3 76.8 76.4 76.0	97.2 96.6 96.1 95.5 95.0	187 186 185	68.8 68.4 68.0 67.5 67.1	86.1 85.5 85.0 84.4 83.8	167 166 165 164 163	60.0 59.5 59.1 58.6 58.2	75.0 74.4 73.8 73.3 72.7	147 146 145 144 143	51.1 50.6 50.2 49.7 49.3	63.8 63.3 62.7 62.2 61.6
202	75.5	94.4	182	66.6	83.3	162	57.7	72.2	142	48.8	61.1
201	75.1	93.8	181	66.2	82.7	161	57.3	71.6	141	48.4	60.5
200	74.6	93.3	180	65.7	82.2	160	56.8	71.1	140	48.0	60.0
199	74.2	92.7	179	65.3	81.6	159	56.4	70.5	139	47.5	59.4
198	73.7	92.2	178	64.8	81.1	158	56.0	70.0	138	47.1	58.8
197	73.3	91.6	177	64.4	80.5	157	55.5	69.4	137	46.6	58.3
196	72.8	91.1	176	64.0	80.0	156	55.1	68.8	136	46.2	57.7
195	72.4	90.5	175	63.5	79.4	155	54.6	68.3	135	45.7	57.2
194	72.0	90.0	174	63.1	78.8	154	54.2	67.7	134	45.3	56.6
193	71.5	89.4	173	62.6	78.3	153	53.7	67.2	133	44.8	56.1

TABLE OF COMPARISON OF DIFFERENT THERMOMETERS—Continued.

Fahrenheit.	Reaumur.	Centigrade.	Fahrenheit.	Reaumur.	Centigrade.	Fahrenheit.	Reaumur.	Centigrade.	Fahrenheit.	Reaumur,	Centigrade.
132 131 130 129 128	44.4 44.0 43.5 43.1 42.6	55.5 55.0 54.4 53.8 53.3	93 92 91 90 89	27.1 26.6 26.2 25.7 25.3	33.8 33.3 32.7 32.2 31.6	54 53 52 51 50	9.7 9.3 8.8 8.4 8.0	12.2 11.6 11.1 10.5 10.0	15 14 13 12 11	-7.5 -8.0 -8.4 -8.8 -9.3	-9.5 -10.0 -10.5 -11.1 -11.6
127 126 125 124 123	42.2 41.7 41.3 40.8 40.4	52.7 52.2 51.6 51.1 50.5	88 87 86 85 84	24.8 24.4 24.0 23.5 23.1	31.1 30.5 30.0 29.4 28.8	49 48 47 46 45	7.5 7.1 6.6 6.2 5.7	9.4 8.8 8.3 7.7 7.2	10 9 8 7 6	-9.7 -10.2 -10.6 -11.1 -11.5	-12.2 -12.7 -13.3 -13.8 -14.4
122 121 120 119 118	40.0 39.5 39.1 38.6 38.2	50.0 49.4 48.8 48.3 47.7	83 82 81 80 79	22.6 22.2 21.7 21.3 20.8	28.3 27.7 27.2 26.6 26.1	44 43 42 41 40	5.3 4.8 4.4 4.0 3.5	6.6 6.1 5.5 5.0 4.4	5 4 3 2 1	-12.0 -12.4 -12.8 -13.3 -13.7	-15.0 -15.5 -16.1 -16.6 -17.2
117 116 115 114 113	37.7 37.3 36.8 36.4 36.0	47.2 46.6 46.1 45.5 45.0	78 77 76 75 74	20.4 20.0 19.5 19.1 18.6	25.5 25.0 24.4 23.8 23.3	39 38 37 36 35	3.1 2.6 2.2 1.7 1.3	3.8 3.3 2.7 2.2 1.6	$ \begin{array}{c} 0 \\ -1 \\ -2 \\ -3 \\ -4 \end{array} $	-14.2 -14.6 -15.1 -15.5 -16.0	-17.7 -18 3 -18.8 -19.4 -20.0
112 111 110 109 108	35.5 35.1 34.6 34.2 33.7	44.4 43.8 43.3 42.7 42.2	73 72 71 70 69	18.2 17.7 17.3 16.8 16.4	22.7 22.2 21.6 21.1 20.5	34 33 32 31 30	0.8 0.4 0.0 -0.4 -0.8	0.5 0.0 0.5 1.1	- 5 6 7 8 9	-16.4 -16.8 -17.3 -17.7 -18.2	-20.5 -21.1 -21.6 -22.2 -22.7
107 106 105 104 103 102	33.3 32.8 32.4 32.0 31.5	41.6 41.1 40.5 40.0 39.4	68 67 66 65 64	16.0 15.5 15.1 14.6 14.2	20.0 19.4 18.8 18.3 17.7	29 28 27 26 25	-1.3 -1 7 -2.2 -2.6 -3.1 -3.5	$ \begin{array}{r} -1.6 \\ -2.2 \\ -2.7 \\ -3.3 \\ -3.8 \\ -4.4 \end{array} $	-10 -11 -12 -13 -14 -15	-18.6 -19.1 -19.5 -20.0 -20.4	-23.3 -23.8 -24.4 -25.0 -25.5 -26.1
101 100 99 98	31.1 30.6 30.2 29.7 29.3	38.8 38.3 37.7 37.2 36.6	63 62 61 60 59	13.7 13.3 12.8 12.4 12.0	17.2 16.6 16.1 15.5 15.0	24 23 22 21 20	$ \begin{array}{r r} -4.0 \\ -4.4 \\ -4.8 \\ -5.3 \end{array} $	$ \begin{array}{r} -1.4 \\ -5.0 \\ -5.5 \\ -6.1 \\ -6.6 \\ -7.2 \end{array} $	-16 -17 -18 -19	$\begin{array}{r} -20.8 \\ -21.3 \\ -21.7 \\ -22.2 \\ -22.6 \\ -23.1 \end{array}$	-26.1 -26.6 -27.2 -27.7 -28.3 -28.8
97 96 95 94	28.8 28.4 28.0 27.5	36.1 35.5 35.0 34.4	58 57 56 55	11.5 11.1 10.6 10.2	14.4 13.8 13.3 12.7	19 18 17 16	-5.7 -6.2 -6.6 -7.1	-7.2 -7.7 -8.3 -8.8	-20	-20.1	-20.8

TABLES OF SPECIFIC GRAVITIES.

METALS.

Metal.	Specific Gravity.	Weight per Cubic Foot.	Specific Heat.	Melting Point in Degrees Fahr.
Aluminum, Cast	2.51	156.06	.214 3	
" Hammered.	2.67^{1}	166.67	.2110	• • • • • • • • • • • • • • • • • • • •
Antimony	6.7022	418.37	.050 8	810.
Arsenic	5.7632	359.76	.081 4	365.
Barium	4.8	249.70		
Bismuth	9.8222	613.14	.030 8	497.
Cadmium	8.6045	537.10	.056 7	500.
Calcium	1.5664	97.76		
Chromium	7.36	455.70		
Cobalt	8.6	536.86	.107 0	
Copper	8.8957	555.27	.0951	1 996.
Rolled	8.8782	554.21		
" Cast	8.7882	548.59		
" Drawn	8.946 38	558.47		
" Hammered	8.958 78	559.25		
" Pressed	8.9319	557.52		
" Electrolytic	8.9149	556.46		
Gold	19.258^{2}	1 202.18	.032 4	2 016.
Iron, Bar	7.483 9	467.18	.130	2 786.
" Wrought	7.79	486.29	.113	3 286.
Steel	7.85	490.03	.116	3 286.
Lead	11.44510	714.45	.031 4	612.
Magnesium	2.24^{11}	139.83	.249 9	
Manganese	6.9^{12}	430.73	.114	3 000.
Mercury	13.56818	846.98	.031 9	38
Nickel	7.832	488.91	.109 1	280 0.
Platinum	20.3 ²	1 267.22	.032 4	328 6.
Potassium	$.865^{14}$	54.00	.169 6	136.
Silver	10.522^{11}	656.84	.057 0	1 873.
Sodium	.97214	60.68	.293 4	194.
Strontium	2.504^{4}	156.31		•••••
Tin	7.291^{2}	455.14	.056 2	442.
Zinc	6.861 ²	428.29	.095 5	773.

^{1.} Wohler.

^{6.} Bunsen.

^{7.} Hatchett.

^{11.} Playfair & Joule.

^{2.} Brisson.

^{12.} Bergman.

^{3.} Clarke.

^{8.} Brezenius.

^{13.} Watts' Dictionary.

^{4.} Matthiessen.

^{9.} Marchand & Scheerer.

^{14.} Guy-Lussac & Thenard.

^{5.} Stromeyer.

^{10.} Musschenbroek.

LIQUIDS.

Liquid.	Specific Gravity.	Temperature.
Alcohol	0.815 71	At 50° F.
Benzine	0.883	At 59° F.
Chloroform	1.491	At 62.6° F.
Carbon Bisulphide	1.2931	At 32° F.
Ether	0.7204	At 60.8° F.
Glycerine	1.2636	At 59° F.
Hydrochloric Acid	1.270	
Mercury	13.596	At 32° F.
Nitric Acid	1.552	At 59° F.
Oil of Turpentine	0.855 to 0.864	At 68° F.
Linseed Oil	0.940	
Olive Oil	0.915	
Sulphuric Acid	1.854	At 32° F

GASES

Gas.	At 0° C. and 760 mm. pressure compared to water.	Compared to air at similar pressure and Temperature.
Air	0.001 292 8	1.000 00
Oxygen	$0.001\ 429\ 3$	1.105 63
Nitrogen	0.001 255 7	0.971 37
Hydrogen	0.000 089 54	0.069 26
Carbonic Dioxide	0.001 976 7	1.529 10
Mixed Gases from Electrolysis of Water	0.000 536 1	0.414 72
Aqueous Vapor		0.623 00

WEIGHTS OF SUBSTANCES PER CUBIC FOOT.

Name of Substance.	Average Weight. Pounds.
Asphaltum	87.
Brick, common, hard	125.
Brickwork, pressed brick	140.
" ordinary	112.
Coal, Anthracite, solid, of Pennsylvania	93.
" broken, loose	54.
" Bituminous, solid	84.
" broken, loose	49.
Coke, loose, of good coal	62.
Cork	12.4
Cork	76.
" " moderately rammed.	95.
" as a soft, flowing mud	
Gneiss, common	168.
Granite	170.
Glass, Crown	168.5
" flint.	
_	57.2
Ice at 0Lime, thoroughly shaken	75.
Masonry, of granite or limestone, well dressed	165.
Masoniy, or granice or innesione, well dressed	103.
Mortar, hardened	80 to 1
Oughtr	165.4
Quartz	
Sulphur	131.0
Wax	58.7
Wood, ebony	74.9
" birch	43.7
оак	46.8
" pine	31.2

PROPERTIES OF COPPER WIRE.

By F. A. C. PERRINE, D.Sc.

Early in 1889 I found it necessary to revise certain tables of the resistance of copper wires in our catalogues, and to adopt a standard of conductivity which should represent the best results which had been obtained; on investigation it was found that the most reliable results were those to be found in Fleeming Jenkins' tabulation of Dr. Matthiessen's experiments, and from which I adopted as our standard the case "one mil foot at 0° C. measures 9.718 B. A. ohms." The most accurate temperature correction I found to be expressed in the formula

Conductivity at $C = 1 - .0038701 t + .000009009 t^2$

and the specific gravity was taken as 8.9, water being at its greatest density 62.425 pounds per cubic foot.

On September 16th, 1890, the Standard Wiring Table Committee of the American Institute of Electrical Engineers presented a report in which they have recommended practically the same results, as follows:

"The subject of Matthiessen's standard alone is so confused and involved, and the discrepancies in regard to it are so great between the best authorities that the Committee has devoted its attention almost entirely to this subject up to the present time.

"A very thorough investigation of Matthiessen's work has been made by a sub-committee, consisting of Professor William E. Geyer, George B. Prescott, Jr., and the Chairman, Francis B. Crocker, and the conclusion has been reached that the most correct and satisfactory 'Matthiessen's Standard,' and the one which we now recommend for general adoption, is stated as follows: A soft copper wire one meter long and one millimeter in diameter ('meter-millimeter') has an electrical resistance of .02057 B. A. units at 0° Centigrade.

"From this the resistance of a soft copper wire one foot long and one-thousandth of an inch in diameter ('mil-foot') is found to be 9.720 B. A. units at 0° C.

"In order to convert these values into legal ohms, we may assume one B. A. unit to be equal to .9889 legal ohms, and the

meter-millimeter value then becomes .02034 legal ohms, and the mil-foot value becomes 9.612 legal ohms.

"The resistance of copper at temperature other than 0° Centigrade may be determined by using Matthiessen's formula $C_t = C_0 (1-.00387 t +.000009009 t^2)$ in which C_t is the conductivity at the given temperature, C_0 is the conductivity at 0° and t is the given temperature in degrees Centigrade. It should be carefully noted, however, that this formula refers to conductivity. Therefore, in order to apply it to resistance, it is necessary to take the reciprocal, and this should not be done by merely changing signs, which is not mathematically correct, although usually given in that way. The correct modification of Matthiessen's formula, when referred to resistance, is

$$R_t = R_0 (1 + .00387 t + .00000597 t^2)$$

"The sub-committee, after careful consideration, came to the conclusion that Matthiessen's 'mile standard' (one statute mile of copper wire 15-inch in diameter has a resistance of 13.59 B. A. units at 15.5° C.) is not the correct one, although very commonly used. Matthiessen himself did not place much confidence in this 'mile standard.' The Committee, acting under instructions from a meeting of the Institute, held September 16th, 1890, has based all standards and values in this report upon soft or annealed copper since its properties are reasonably constant and reliable. Whereas, the Committee has purposely excluded from its recommendations all standards and values based upon hard copper, although several were given by Matthiessen, because the hardness of copper is merely relative, and the resistance of hard copper may vary between wide and uncertain limits depending upon the degree of hardness.

"As to the fact often brought up, that copper may be found which tests one or two per cent higher conductivity or less resistance than Matthiessen's standard, we are of the opinion that this is no real objection, provided the value of the standard is definite and generally accepted. A standard which is not the highest attainable value may even be considered an advantage, since the average commercial wires will approximate to it more closely.

"Although we believe the standard we recommend will answer the purpose temporarily and probably permanently, nevertheless, we think that if a thoroughly correct and complete redetermination of the standard resistance of copper could be accomplished, it would be a benefit to electrical science and industry. Favorable offers in this direction have already been received by this Committee from Johns Hopkins University, Cornell University, and Columbia College, and it is likely that this redetermination may be undertaken.

"The following statement of the most important and reliable figures and facts given by Matthiessen will serve to show the derivation of the standard which we recommend.

"A hard-drawn copper wire 1 meter long weighing 1 gram ('meter-gram') has a resistance of .1469 B. A. units at the temperature of 0° Centigrade.*

"Matthiessen also gives the resistance of a hard-drawn copper wire 1 meter long and 1 millimeter in diameter ('metermillimeter') as .02104 B. A. units at 0° C.*

"This implies a specific gravity of 8.89 for the copper used by Matthiessen, but unfortunately he neglected to actually determine the specific gravity.

"Matthiessen's figures for relative conducting power are: †

Silver	100
Hard or unannealed copper	99.95
Soft or annealed copper	102.21

"From these the resistance of Matthiessen's hard copper is found to be 1.0226 times that of soft copper, therefore the resistance of a soft copper wire 1 meter long and 1 millimeter diameter ('meter-millimeter') is .02057 B. A. units at 0° C., which is the standard we recommend.

"From this the resistance of 1 cubic centimeter of soft copper is found to be .000001616 B. A. units at 0° C.

"And the resistance of soft copper wire 1 foot long and .001 inch in diameter ('mil-foot') is 9.720~B. A. units at 0° C.

"Taking one B. A. unit as .9889 legal ohms any of the above values may be converted into legal ohms. To find the conductivity of copper at temperatures other than 0° C., Matthiessen's formula may be used, viz.:

$$C_t = C_0 (1 - .00387 t + .000009009 t^2)$$
 or
 $R_t = R_0 (1 + .00387 t + .00000597 t^2)$

^{*}Philosophical Magazine, May, 1865.

[†]Philosophical Transactions, 1864.

TABLE.

Standard Resistance at 0° C. of	B. A. U.	Legal Ohms.
"Meter-millimeter," Soft Copper" "Cubic Centimeter," " " " " " " " " " " " " " " " " " "	.02057 .000001616 9.720	.02034 .000001598 9.612

"F. B. CROCKER,
"Chairman."

Shortly after this report was presented, I took an average of my tests on 682 samples, the result of a year's work, and found that the average conductivity of the whole number was 98.98 per cent., or practically 99 per cent. All of this copper was from Calumet and Hecla bars rolled and drawn at our own mill at Trenton, and it represents daily practice, since no selection was made of the samples, and all results are included in the average.

That commercial copper should give 99 per cent. the conductivity of a standard, I believe to be one of the strongest arguments in favor of that standard for the practical electrical engineer, since it will allow the use of tables calculated therefrom without correction, one per cent. being well within the limits of practice in manufacture.

The tables in this book, having been calculated before this report was presented, have not been corrected to the value "one mil-foot at 0° C. measures 9.720 B. A. units," since the value used varies from it by only .02 per cent.

RESISTANCE OF 1 MIL FOOT OF COPPER WIRE AT DIFFERENT TEMPERATURES FAHRENHEIT.

Temperature in Degrees.	B. A. Units.	Legal Ohms.	Temperature in Degrees.	B. A. Units.	Legal Ohms.	Temperature in Degrees.	B. A. Units.	Legal Ohms.
0 1 2 3 4	9.067 73 9.087 49 9.107 29 9.127 13 9.147 01	8.967 07 8.986 62 9.006 20 9.025 82 9.045 47	34 35 36 37 38	9.759 85 9.780 84 9.801 86 9.822 91 9.844 00	9.651 52 9.672 27 9.693 06 9.713 88 9.734 73	68 69 70 71 72	10.493 37 10.515 57 10.537 80 10.560 08 10.582 38	10.376 89 10.398 84 10.420 83 10.442 86 10.464 92
5 6 7 8 9	9.166 91 9.186 86 9.206 84 9.226 86 9.246 91	9.065 16 9.084 89 9.104 64 9.124 44 9.144 27	39 40 41 42 43	9.865 13 9.886 29 9.907 49 9.928 72 9.949 99	9.755 63 9.776 55 9.797 52 9.818 51 9.839 55	73 74 75 76 77	10.604 73 10.627 11 10.649 52 10.671 97 10.694 46	10.487 02 10.509 15 10.531 31 10.553 51 10.575 75
10 11 12 13 14	9.267 00 9.287 12 9.307 28 9.327 48 9.347 71	9.164 13 9.184 03 9.203 97 9.223 94 9.243 95	48	9.971 30 9.992 64 10.014 02 10.035 43 10.056 88	9.860 62 9.881 72 9.902 86 9.924 03 9.945 25	82	10.716 98 10.739 54 10.762 14 10.784 77 10.807 43	10.598 02 10.620 33 10.642 68 10.665 05 10.687 47
15 16 17 18 19	9.367 98 9.388 28 9.408 62 9.428 99 9.449 40	9.304 18 9.324 33 9.344 51	49 50 51 52 53	10.078 36 10.099 88 10.121 44 10.143 03 10.164 66	9.966 49 9.987 77 10.009 09 10.030 44 10.051 83	86 87	10.830 13 10.852 87 10.875 64 10.898 45 10.921 30	10.709 92 10.732 40 10.754 92 10.777 48 10.800 07
20 21 22 23 24	9.469 85 9.490 33 9.510 85 9.531 40 9.551 99	9.405 28 9.425 60 9.445 96	54 55 56 57 58	10.186 32 10.208 02 10.229 75 10.251 53 10.273 33	10.073 25 10.094 71 10.116 20 10.137 73 10.159 30	88 89 90 91 92	10.944 18 10.967 09 10.990 05 11.013 04 11.036 06	10.822 70 10.845 36 10.868 06 10.890 79 10.913 56
25 26 27 28 29	9.572 62 9.593 28 9.613 97 9.634 71 9.655 48	9.548 30	63	10.295 17 10.317 05 10.338 97 10.360 92 10.382 90	10.180 90 10.202 53 10.224 20 10.245 91 10.267 65	93 94 95 96 97	11.059 12 11.082 21 11.105 35 11.128 51 11.151 72	10.936 36 10.959 20 10.982 08 11.004 99 11.027 93
30 31 32 33	9.676 28 9.697 12 9.718 00 9.738 91	9.589 48 9.610 13		10.404 92 10.426 98 10.449 07 10.471 20	10.289 43 10.311 24 10.333 09 10.354 97	99 100	11.174 95 11.198 23 11.221 54	11.050 91 11.073 93 11.096 98

JOHN A. ROEBLING'S SONS CO.

TABLE OF SQUARES

		TABUL	
		BROWN AND SHARPE.	_
	Roebli	ING. AREA.	
Number of Gauge. Diameter	<u>.</u>	AREA.	
Number of Gauge. Diameter	Circula	MIII	
NIIN G. BiU		166 191	
000000 4	.60. 211 600 184 90	00. 145 304 244 6 409.640 167 679.2 104 320	6.
0000	$ \begin{array}{c cccc} 130. & 154 & 44 \\ 393. & 131 & 0 \\ 362. & 109 & 5 \end{array} $	044. 102 049 209 4 301 860 105 534.0 65 73	3. 9.
	331.	74 023 164 289,300 66 373.0 41 33 278 62 901,900 6 297,630 52 633.4 32 78	38. 34.
0 1 2	283. 69 263. 50	23 102.3 20 6	17.
3 4	244. 50	0 623.	167.
5 6	192.	36 804. 24 600. 037 6 128.430 13 094.0 8	153.6 467.1
· 8	162.	26 244. 17 205.30 101.890 8 234.1 5	128.0 067.1
10		18 225. 14 400. 11 309,035 0 71.961 5 176.8 3	225.4
$11 \\ 12 \\ 13$	105. 92.	8 404. 5 020.000	2 028.4 1 608.6
14	80.	5 184. 3 117.252 6 450.3257 2 048.2 1 624.3	1 275.7 1 011.7
15 16 17	63. 54.	2 209. 1 320.257 4 35.500 1 021.5	802. 636. 504.
18 19	47.	962.115 0 28.462 642.47	400. 317.
20 21	35. 32. 28.	1 024. 615.735 0 22.571 404.01 4090.875 0 20.100 404.01 200.41	251. 199.
22 23 24	25. 23.	529.	158 125
25	20. 18.	324. 226.980 6 14.193 159.79 126.72	78
26 27 28	15.	256. 176.715 10.025 79.71	62 49
30	14.	190. 25 143.135 2 7.930 50.13	39
31 33	13.0	0 121.00 95.030 6.304 31.52	1
. 3	10.0	70.882 3 5.000	
3			

AND AREAS.

Wire	Standard.	LISH LEGAL	Enc	or Stubs.	IRMINGHAM	В			
Number of Wire Gauge.	AREA.		eter fils.	AREA.	A	cter fils			
Number Gauge,	Square Mils.	Circular Mils.	Diameter in Mils.	Squ are Mils.	Circular Mils.	Diameter in Mils.			
00000	169 093.478 4	215 296.	464.						
0000	146 574.489 6	186 624.	432.	***************************************	**********	:::::			
000	06 4 400. 160 000. 125 664.000 0 175 0 372. 138 384. 108 686.793 6	.875 0 372. 138 384. 108 686.793 6	4 400. 160 000. 125 664.0	6 4 400. 160 000. 125 664.000 0	161 883.506 4	206 116.	454.		
00			141 862.875 0	180 625.	425. 380.				
0	95 115.081 6	121 104.	348.	113 411.760 0	144 400.	DOU.			
ļ	82 448.150 4	104 976.	324.	90 792.240 0	115 600.	340.			
	70 686.000 0	90 000.	300.	70 686.000 0	90 000.	300.			
	59 828. 630 4	76 176.	276.	63 347.222 4	80 656.	284.			
	49 876.041 6	63 504.	252.	52 685.417 4	67 081.	59.			
	42 273.369 6	53 824.	232.	44 488.197 6	56 644.	238.			
	35 299.017 6	44 944.	212.	38 013.360 0	48 400.	20.			
1	28 952.985 6	36 864.	192.	32 365.548 6	41 209.	203.			
	24 328.550 4	30 976.	176.	25 446.960 0	32 400.	80.			
		0 160. 25 600. 20 106.240 0					21 382.515 0	27 225.	65.
ļ	16 286.054 4	20 736.	144.	17 203.401 6	21 904.	48.			
1	12 867,993 6	16 384.	128.	14 102.642 4	17 956.	34.			
ī	10 568.342 4	13 456.	116.	11 309.760 0	14 400.	20.			
1	8 494.886 4	10 816.	104.	9 331.337 4	11 881.	09.			
1	6 647.625 6	2. 8 464. 6 647.625 6	92. 8 464. 6 647.625	92. 8 464. 6 647.625	7 088.235 0	9 025.	95.		
1	5 026.560 0	6 400.	80.	5 410.620 6	6 889.	83.			
1	4 071.513 6	5 184.	72.	4 071.513 6	5 184.	72.			
Ī	3 216,998 4	4 096.	64.	3 318.315 0	4 225.	65.			
1	2 463.014 4	3 136.	56.	2 642.085 6	3 364.	58.			
1	1 809.561 6	2 304.	48.	1 885.745 4	2 401.	49.			
1	1 256.640 0	1 600.	40.	1 385.445 6	1 764.	42.			
2	1 017.878 4	1 296.	36.	962.115 0	1 225.	35.			
2	804.249 6	1 024.	32.	804.249 6	1 024.	32.			
2	615.753 6	784.	28.	615.753 6	784.	28.			
2	452.390 4	576.	24.	490.875 0	625.	25.			
2	380.133 6	484.	22.	380.133 6	484.	22.			
2	314.160 0	400.	20.	314.160 0	400.	20.			
2	254.469 6	324.	18.	254 469 6	324.	18.			
2	211.241 184	268.96	16.4	201.062 4	256.	16.			
2	172.034 016	219.04	14.8	153.938 4	196.	14.			
2	145.267 584	184.96	13.6	132.732 6	169.	13.			
3	120,763 104	153.76	12.4	113.097 6	144.	12.			
3	105.683 424	134.56	11.6	78.540 0	100.	10			
3	91.609 056	116.64	10.8	63.617 4	81.	9.			
3	78.540 900	100.00	10.0	50.265 6	64.	8.			
3	66.476 256	84 64	9.2	38.484 6	49.	7.			
3	55.417 824	70.56	8.4	19.635 0	25.	5.			
' 3	45.364 704	57.76	7.6	12.566 4	16.	-4.			

RESISTANCE PER 1,000

Wire		Roel	BLING.		В	ROWN AN	ND SHAR	PE.
er of v ge.	55° 1	Fahr.	70° 1	Fahr.	55° I	fahr.	70° I	ahr.
Number of Wire	B. A.	Legal	B. A.	Legal	B. A.	Legal	B. A.	Legal
Gauge.	Units.	Ohms.	Units.	Ohms.	Units.	Ohms.	Units.	Ohms.
000000 00000 0000 000 000	.048 24 .055 21 .066 09 .077 90 .093 17	.054 59 .065 36 .077 03	.049 81 .056 99 .068 23 .080 41 .096 18	.067 47 .079 52	.048 24 .060 83 .076 71	.060 16	.049 81 .062 80 .079 18	.049 25 .062 10 .078 31
0	.108 3	.107 1	.111 8	.110 6	.096 73	.095 66	.099 85	.098 74
1	.127 4	.126 0	.131 6	.130 1	.122 0	.120 6	.125 9	.124 2
2	.147 6	.145 9	.152 3	.150 6	.153 8	.152 1	.158 7	.157 0
3	.171 5	.169 6	.177 0	.175 0	.193 9	.191 8	.200 2	.198 0
4	.201 6	.199 4	.208 2	.205 8	.244 5	.241 8	.252 5	.249 6
5	.238 2	.235 6	.245 9	.243 2	.308 4	.304 9	.318 3	.314 8
6	.276 9	.273 8	.285 9	.282 7	.388 9	.384 6	.401 4	.397 0
7	.325 8	.322 2	.336 4	.332 7	.490 4	.484 9	.506 1	.500 6
8	.389 0	.384 6	.401 6	.397 1	.618 3	.611 4	.638 2	.631 2
9	.466 0	.460 9	.481 1	.475 8	.779 6	.770 9	.804 6	.795 8
10	.560 1	.553 9	.578 2	.571 8	.983 3	.972 4	1.015	1.040
11	.708 9	.701 0	.731 8	.723 7	1.240	1.260	1.280	1.266
12	.925 9	.915 6	.955 8	.945 2	1.563	1.546	1.614	1.596
13	1.206	1.198	1.245	1.231 0	1.971	1.950	2.035	2.012
14	1.595	1.577	1.646	1.628 0	2.486	2.458	2.566	2.537
15	1.969	1.947	2.033	2.010	3.134	3.100	3.235	3.200
16	2.572	2.543	2.655	2.626	3.952	3.909	4.080	4.035
17	3.501	3.462	3.614	3.574	4.984	4.929	5.145	5.088
18	4.621	4.570	4.771	4.718	0.284	6.215	6.487	6.415
19	6.072	6.005	6.269	6.199	7.925	7.837	8.180	8.089
20	8.833	8.240	8.602	8.507	9.993	9.882	10.31	10.20
21	9.969	9.858	10.29	10.18	12.60	12.46	13.00	12.86
22	13.02	12.87	13.44	13.29	15.89	15.71	16.40	16.22
23	16.83	16.15	16.86	16.67	20.04	19.82	20.68	20.45
24	19.30	19.08	19.92	19.70	25.26	24.99	26.08	25.79
25	25.52	25.24	26.34	26.05	31.86	31.50	32.88	82.52
26	31.51	31.16	32.52	32.16	40.18	89.73	41.47	41.01
27	35.32	84.93	36.46	36.06	50.66	50.10	52.30	51.72
28	39.88	89.43	41.16	40.71	63.88	63.17	65.95	65.21
29	45.37	44.87	46.83	46.31	80.56	79.66	83.16	82.23
30	52.08	51.50	53.76	53.17	101.6	100.5	104.8	103.7
81	56.01	55.39	57.82	57.18	128.1	126.6	132.2	130.7
32	60.40	59.73	62.35	61.66	161.5	159.7	166.8	164.9
33	84.36	83.43	87.09	86.12	203.6	201.4	210.2	207.9
34	102.1	100.9	105.4	104.20	256.9	254.0	265.2	262.2
35	113.1	111.8	116.8	115 5	323.9	320 3	334.4	330:6
36	126.0	124.6	130.1	128.7	408.3	403.8	421.5	416.8

FEET COPPER WIRE.

Bu	RMINGHA	m or Stu	BS.	Engi	ISH LEG	al Stan	DARD.	Wire
55°]	Fahr.	70° 1	Fahr.	55°]	ahr.	. 70° 1	ahr.	er of ge.
B. A.	Legal	B. A.	Legal	B. A.	Legal	B. A.	Legal	Number of Wire
Units.	Ohms.	Units.	Ohms.	Units.	Ohms.	Units.	Ohms.	Gauge.
.049 53 .056 51 .070 69	.055 89	.051 13 .058 33 .072 98		.047 41 .054 70 .063 80 .073 77 .084 29	.054 09 .063 09	.048 95 .056 47 .065 86 .076 15 .087 02	.048 40 .055 84 .065 13 .075 80 .086 05	000000 00000 0000 000 00
.088 3	.087 32	.091 16	.090 15	.097 24	.096 16	.100 4	.099 27	0
.113 4	.112 2	.117 1	.115 8	.113 4	.112 2	.117 1	.115 8	1
.126 6	.125 2	.130 7	.129 2	.134 0	.132 5	.138 3	.136 8	2
.152 2	.150 5	.157 1	.155 4	.160 7	.159 0	.166 0	.164 1	3
.180 2	.178 2	.186 0	.184 0	.189 6	.187 5	.195 8	.193 6	4
.210 9	.208 6	.217 7	.215 3	.227 1	.224 6	.234 5	.281 9	5
.247 7	.245 0	.255 8	.252 9	.276 9	.273 8	.285 9	.282 7	6
.315 1	.311 6	.325 3	.321 6	.329 5	.325 9	.340 2	.336 4	7
.374 9	.370 8	.387 1	.382 9	.398 8	.394 3	.411 6	.407 0	8
.466 0	.460 9	.481 1	.475 8	.492 3	.486 8	.508 2	.502 6	9
.568 5	.562 2	.586 9	.580 4	.623 0	.616 1	.643 2	.636 1	10
.708 9	.701 0	.731 8	.723 7	.758 6	.750 2	.783 1	.774 5	11
.859 2	.849 6	.886 9	.877 1	.943 8	.933 3	.974 3	.963 5	12
1.131	1.118	1.168	1.155	1.206	1.193	1.245	1.231	13
1.482	1.465	1.530	1.513	1.595	1.577	1.646	1.628	14
1.969	1.947	2.083	2.010	1.969	1.947	2.033	2.010	15
2.416	2.389	2.494	2.466	2.492	2.464	2.572	2.544	16
3.034	3.001	3.133	8.098	3.256	3 219	3.360	3.323	17
4.252	4.204	4.389	4.340	4.430	4.382	4.574	4 523	18
5.787	5.723	5.974	5.908	6.380	6.309	6.586	6.513	19
8.333	8.240	8.602	8.507	7.876	7.789	8.113	8.041	20
9.969	9.858	10.29	10.18	9.969	9.858	10.29	10.18	21
13.02	12.87	13.44	13.29	13.02	12.87	13.44	13.29	22
16.33	16.15	16.86	16.67	17.72	17.52	18.29	18.09	23
21.09	20.86	21.77	21.53	21.09	20.86	21.77	21.58	24
25.52	25.24	26.34	26.05	25.52	25.24	26.34	26.05	25
31.51	31.16	32.52	32.16	31.51	31.16	32.52	\$2.16	26
39.88	39.43	41.16	40.71	37.95	37.53	39.18	\$8.75	27
52.08	51.50	53.76	53.17	46.60	46.08	48.11	47.57	28
60.40	59.73	62.35	61.66	55.19	54.58	56.97	56.34	29
70.89	70.10	73.18	72.37	66.39	65.65	68.54	67.77	30
102.1	100.9	105.4	104.2	75.86	75.02	78.31	77.44	31
126.0	124.6	130.1	128.7	87 52	86.55	90.35	89.34	32
159.5	157.7	164.7	162.8	102.1	100.9	105.4	104.2	33
208.3	206.0	215.1	212.7	120.6	119.3	124.5	123.1	34
408.3	403.7	421.5	416.8	144.7	143.1	149.4	147.7	35
638.0	630.9	658.6	651.3	176.7	174.7	182.5	180.4	36

CONDUCTIVITY OF METALS.

Coëfficients for the temperature: t in degrees Centigrade.

Metal.	Coëfficient.
Copper Gold Zine Cadmium Tin Lead Arsenic Antimony Bismuth	$\begin{array}{ c c c c c c }\hline C = 100 - 0.382 \ 78 \ t + 0.000 \ 984 \ 8 \ t^2 \\ C = 100 - 0.387 \ 01 \ t + 0.000 \ 900 \ 9 \ t^2 \\ C = 100 - 0.367 \ 45 \ t + 0.000 \ 844 \ 3 \ t^2 \\ C = 100 - 0.367 \ 47 \ t + 0.000 \ 827 \ 4 \ t^2 \\ C = 100 - 0.368 \ 71 \ t + 0.000 \ 757 \ 5 \ t^2 \\ C = 100 - 0.360 \ 29 \ t + 0.000 \ 613 \ 6 \ t^2 \\ C = 100 - 0.387 \ 56 \ t + 0.000 \ 914 \ 6 \ t^2 \\ C = 100 - 0.389 \ 96 \ t + 0.000 \ 887 \ 9t^2 \\ C = 100 - 0.398 \ 26 \ t + 0.001 \ 036 \ 4 \ t^2 \\ C = 100 - 0.352 \ 16 \ t + 0.000 \ 572 \ 8 \ t^2 \\ C = 100 - 0.511 \ 82 \ t + 0.001 \ 291 \ 6 \ t^2 \\ \end{array}$

INFLUENCE OF THE TEMPERATURE ON THE RE-SISTANCE AND THE CONDUCTIVITY OF PURE COPPER.

Temperature, Centigrade.	Resistance.	Conductivity.	Temperature, Centigrade.	Resistance.	Conductivity.	Temperature, Centigrade.	Resistance.	Conductivity.
0 1 2 3 4	1.000 00 1.003 81 1.007 56 1.011 35 1.015 15	0.996 24 0.992 50 0.988 78	11 12 13 14 15		0.959 70 0.956 03 0.952 47 0.948 93 0.945 41	22 23 24 25 26	1.085 53 1.089 54 1.093 56 1.097 63 1.101 61	0.917 82 0.914 45
5 6 7 8 9	1.030 48 1.034 35	0.977 71 0.974 06 0.970 42	16 17 18 19 20 21	1.069 59 1.073 56 1.077 42	0.941 90 0.938 41 0.934 94 0.931 48 0.928 14 0.924 52	27 28 29 30	1.105 67 1.119 72 1.113 82 1.117 82	0.897 84

TABLE OF TENSILE STRENGTH FOR COPPER WIRE.

		···			
Size of Wire, B. & S.	Breaking Weight of	Breaking Weight of	Size of Wire, B. & S.	Breaking Weight of	Breaking Weight of
Gauge.	Hard-Drawn.	Annealed.	Gauge.	Hard-Drawn.	Annealed.
0000 000 00 00 0	Lbs. 9 971 7 907 6 271 4 973 3 943	Lbs. 5 650 4 480 3 553 2 818 2 234	9 10 11 12 13	Lbs. 617 489 388 307 244	1bs. 349 277 219 174 138
2	3 127	1 772	14	193	109
3	2 480	1 405	15	153	87
4	1 967	1 114	16	133	69
5	1 559	883	17	97	55
6	1 237	700	18	77	43
7	980	555	19	61	34
8	778	440	20	48	27



FUSING EFFECTS OF ELECTRIC CURRENTS.

By W. H. PREECE, F.R.S.

[See "Proc. Roy. Soc.," Vol. XLIX., March 15, 1888.]

The Law—C = ad $\frac{3}{2}$, where, C current; a, constant; and d, diameter—is strictly followed; and the following are the final values of the constant, "a," for the different metals as determined by Mr. Preece:

	Inches.	Centimeters.	Millimeters.
Copper	10,244	2,530	80.0
	7,585	1,873	59.2
	5,172	1,277	40.4
	5,230	1,292	40.8
Platinoid	4,750	1,173	37.1
	3,148	777.4	24.6
	1,642	405.5	12.8
	1,318	325.5	10.3
	1,379	340.6	10.8

With these constants the following tables have been calcuated:

TABLE SHOWING THE AMPERES REQUIRED TO FUSE WIRES OF VARIOUS SIZES AND MATERIALS.

luminum Platinum Silver a=5172. a=5220	Copper Aluming
	8=7585
_	171.600
83.730	122.80
54.370	79.75
35.330	1.18
24.230	5.53
	4.75
12.490	18.32
9.311	13.66
7.142	10.470
5.805	8.51

table. Pure copper wire makes the best and most reliable cut-out or fuse, and should never be less than one Nore.—The size of "cut-outs," or fuses for electric-lighting circuits, can be taken at once from the second inch in length between the terminals to which it is fixed so as to prevent the cooling effect of the terminals.

TABLE GIVING THE DIAMETER OF WIRES OF VARIOUS MATERIALS WHICH WILL BE FUSED BY A CURRENT OF GIVEN STRENGTH.

W. H. PREECE, F.R.S.

$$\mathbf{d} = \begin{pmatrix} \mathbf{C} \\ \mathbf{a} \end{pmatrix}^{\frac{2}{3}}$$

es.				DIAME	TER IN I	NCHES.		·····	
Current in Amperes.	Copper s=10,244.	Aluminum 8=7585.	Platinum a=5172	German Silver a=5230.	Platinoid a=4750.	Iron . a=3148.	Tin a=1642.	Tin-lead Alloy a=1318.	Lead a=1379.
1	0.002 1	0.002 6	0.003 3	0.003 3	0.003 5	0.004 7	0.007 2	0.008 3	0.008 1
2	0.003 4	0.004 1	0.005 3	0.005 3	0.005 6	0.007 4	0.011 3	0.013 2	0.012 8
3	0.004 4	0.005 4	0.007 0	0.006 9	0.007 4	0.009 7	0.014 9	0.017 3	0.016 8
4	0.005 3	0.006 5	0.008 4	0.008 4	0.008 9	0.011 7	0.018 1	0.021 0	0.020 3
5	0.006 2	0.007 6	0.009 8	0.009 7	0.010 4	0.013 6	0.021 0	0.024 3	0.023 6
10	0.009 8	0.012 0	0 015 5	0.015 4	0.016 4	0.021 6	0.033 4	0.038 6	0.037 5
15	0.012 9	0.015 8	0.020 3	0.020 2	0.021 5	0.028 3	0.043 7	0.050 6	0.049 1
20	0.015 6	0.019 1	0.024 6	0.024 5	0.026 1	0.034 3	0.052 9	0.061 3	0.059 5
25	0.018 1	0.022 2	0.028 6	0.028 4	0.030 3	0.039 8	0.061 4	0.071 1	0.069 0
30	0.020 5	0.025 0	0.032 3	0.032 0	0.034 2	0.045 0	0.069 4	0.080 3	0.077 9
35	0.022 7	0.027 7	0.035 8	0.035 6	0.037 9	0.049 8	0.076 9	0.089 0	0.086 4
40	0.024 8	0.030 3	0.039 1	0.038 8	0.041 4	0.054 5	0.084 0	0.097 3	0.094 4
45	0.026 8	0.032 8	0.042 3	0.042 0	0.044 8	0.058 9	0.090 9	0.105 2	0.102 1
50	0.028 8	0.035 2	0.045 4	0.045 0	0.048 0	0.063 2	0.097 5	0.112 9	0.109 5
60	0.032 5	0.039 7	0.051 3	0.050 9	0.054 2	0.071 4	0.110 1	0.127 5	0.123 7
70	0.036 0	0.044 0	0.056 8	0.056 4	0.060 1	0.079 1	0.122 0	0.141 3	0.137 1
80	0.039 4	0.048 1	0.062 1	0.061 6	0.065 7	0.086 4	0.133 4	0.154 4	0.149 9
90	0.042 6	0.052 0	0.067 2	0.066 7	0.071 1	0.093 5	0.144 3	0.167 1	0.162 1
100	0.045 7	0.055 8	0.072 0	0.071 5	0.076 2	0.100 3	0.154 8	0.179 2	0.173 9
120	0.051 6	0.063 0	0.081 4	0.080 8	0.086 1	0.113 3	0.174 8	0.202 4	0.196 4
140	0.057 2	0.069 8	0.090 2	0.089 5	0.095 4	0.125 5	0.193 7	0.224 3	0.217 6
160	0.062 5	0.076 3	0.098 6	0.097 8	0.104 3	0.137 2	0.211 8	0.245 2	0.237 9
180	0.067 6	0.082 6	0.106 6	0.105 8	0.112 8	0.148 4	0.229 1	0.265 2	0.257 3
200	0.072 5	0.088 6	0.114 4	0.113 5	0.121 0	0.159 2	0.245 7	0.284 5	0.276 0
225	0.078 4	0.095 8	0.123 7	0.122 8	0.130 9	0.172 2	0.265 8	0.307 7	0.298 6
250 275 300	$\begin{array}{c} 0.084\ 1 \\ 0.089\ 7 \\ 0.095\ 0 \end{array}$	0.102 8 0.109 5 0.116 1	0.132 7 0.141 4 0.149 8		0.140 4 0.149 7 0.158 6	0.184 8 0.196 9 0.208 6	$\begin{array}{c} 0.285\ 1 \\ 0.303\ 8 \\ 0.322\ 0 \end{array}$	0.330 1 0.351 8 0.372 8	0.320 3 0.341 3 0.361 7

WIRING TABLES.

Calculated by F. A. C. PERRINE, D.Sc.

The first section of these tables is calculated from the expression of Ohm's law $R = \frac{E}{C}$, and gives the resistances for currents from one to one hundred amperes at voltages varying by half volts from one-half to ten volts, and the resistances for currents from one to two hundred amperes at voltages varying by single volts from ten to twenty volts. The second section furnishes the actual resistance of copper wire drawn according to the Brown & Sharpe gauge for various distances at 70° F.

From the first section we can get the required resistance of any circuit absorbing an electromotive force with a given current, and from the second the wire which will be of the required resistance.

Rule.—The first column of the tables of loss of voltage on any circuit represents, with the uppermost cross-row of figures, amperes. The figures in the other columns represent resistances of circuits carrying different currents at the loss of voltage given by the table. Thus:

What must be the resistance of a circuit carrying 98 amperes to show a drop of 3.5 volts? Ans. .0357 ohms.

Now, to obtain the requisite size of wire necessary to carry 98 amperes 550 feet (that is, for a distance of 225 feet—the total length of circuit then being 550 feet), it is necessary to look in the tables showing resistances of the various sizes of wires at different lengths, and obtain a wire whose resistance at 550 feet equals .0357 ohms. Doing this, we find that the resistance of a No. 000 B. & S. wire, 550 feet in length, would be .03454 ohms. Therefore, we would select a No. 000 B. & S. copper wire to carry 98 amperes 550 feet, with a drop (or loss) of 3.5 volts.

Example.—Required, the size wire to carry 87 amperes 1,850 feet, on a 110 volt circuit, the drop being 5 per cent.

Ans. The absolute loss of voltage on this circuit is 5.5 volts. The resistance of a circuit carrying 87 amperes with 5.5 volts loss, from the tables, is found to be .0632 ohms. Upon inspec-

tion of the tables, giving the resistance of wire, it is found that none show so low a resistance as .0632 ohms for 1850 feet. If now we multiply the required resistance by 2, we may find a wire which would carry $\frac{1}{2}$ the current under the conditions named; thus: $.0632 \times 2 = .1264$ ohms. Now, upon inspection of the tables, we can find no wire 1850 feet in length showing .1264 ohms resistance, and so we try with the multiple 3 to divide the line into 3 circuits each carrying $\frac{1}{2}$ of the current; thus: .0632 ohms \times 3 = .1896 ohms. The nearest approach to this resistance for 1850 feet is a No. 0 wire. Therefore three No. 0 B. & S. wires or their equivalent would carry 87 amperes 1850 feet, with a loss of 5.5 volts.

SHOWING RESISTANCE OF ANY CIRCUIT CARRYING A GIVEN NUMBER OF AMPERES WITH A GIVEN LOSS OF ELECTROMOTIVE FORCE. TABLES

AT .5 VOLTS LOSS.

6	.0556	.0263	.0172	.0128	.010	.008 5	.007 2	.0063	.005	.005
&	.062 5	.027 8	.0178	.013 2	.010	9 800.	.007 3	.0064	.005 7	.0051
7	.0714	.029 4	.018 5	.0135	.010	8 800.	.007 5	.006 5	.005 7	.005 1
9	.083 3	0312	.019 2	.0139	6 010.	6 800.	9 200.	9 900:	.005 8	.005 2
2	1000	.033 3	.020	.0143	.01111	1 600.	.007 7	2 900:	.005 9	.0053
4	.1250	.035 7	.0208	.0147	.0114	2 600.	8 200.	2 900.	.005 9	.005 3
89	.1667	.038 5	.021 7	.015	.0116	.009	6 200.	8 900:	0 900.	.005 4
61	.2500	.0417	.022 7	.0156	.0119	9 600.	.008	6900.	.0061	.005 4
-	.500 0	.0454	.0238	.016	.0122	8 600.	.008 2	0 200.	2 900	.005 5
0	8	0200	.025 0	.0167	.0125	0010.	.0083	.007 1	.0062	.005 5
Current.	0	10	8	8	\$	ಜ	8	20	8	6

AT 1 VOLT LOSS.

Current.	0	-		es	4	ro.	9	7	∞	6
0	8	1.0000	.500 0	.333 3	.2500	200 0	.1667	.1429	.1250	.1111
10	1000	6 060	.083 3	6 9 20.	.0714	.0667	.062 5	.0588	.055 6	.0526
20	.050	.047 6	.045 5	.043 5	.0417	.0400	.038 5	.037	.035 7	.0345
္က	.0333	.0323	.0313	.0303	.0294	.0286	.0278	.027 0	.0263	.0256
4	.025 0	.024 4	.0238	.0233	.022 7	.022 2	.021 7	.021 3	.020	.0204
යි	.020	010.	.0192	0189	.0185	.0182	9 210.	.017 5	.017 2	.0169
8	7 910.	.0164	.0161	.0159	.0156	.0154	.015 2	.0149	.0147	.0145
22	.0143	.0141	.0139	.0137	.013 5	.0133	.013 2	.0130	.0128	.0127
08	.0125	.0123	.0122	.0120	.0119	.0118	.0116	.0115	.0114	0112
8	.0111	.0110	.010	8 010.	.010	.010 5	.010	.0103	.010	.010
100	.010	6600	8 600.	- 2 600:	9 600	.009 5	4 600.	.009	.009	.0092

AT 1.5 VOLTS LOSS.

Current.	0	1	23	8	4	2	9	7	8	6
0	8	1.5000	.7500	.5000	.3750	.3000	.250 0	.2143	.1875	.1667
10	.1500	.1364	.1250	.1154	.107 1	.100 0	.093 7	.088	.0833	.0789
ଛ	.0750	.071 4	.068 2	.0652	.062 5	0 090:	.057 7	.055 5	.053 6	.0517
8	.050	.0484	.0469	.0454	1.44	.0429	.041 7	.040 5	.039 5	.038 5
40	.037 5	9 980.	.035 7	.0349	.034 1	.033 3	.0326	.0319	.031 2	.030 6
20	.030 0	.029 4	.028 8	.0283	.027 8	.027 3	.0268	.0263	.0259	.025 4
8	.0250	.024 6	.024 2	.0238	.023 4	.023 1	.022 7	.022 4	.022 1	.021
20	.021 4	.021 1	.020 8	.020 5	.0203	.020 0	7 610.	019 5	.019	0610.
8	.018 7	.018 5	.0183	.018 1	.0178	.017 6	.017 4	.017 2	0110	0169
8	.0167	0165	.0163	.016 1	0 910	.0158	.015 6	.015 5	.0153	.015 1

AT 2 VOLTS LOSS.

Current.	0	-	61	က	7	ı.o	9	7	∞	6
0	8	2.0000	1.0000	7 999.	.5000	.400 0	.333 3	.285 7	.2500	.222 2
10	.200	.1818	.1667	.1538	.1429	.133 3	.1250	.1176	.1111	.1053
20	.100 0	.095 2	6 060	0 280.	.0833	0800	6 9 20.	.074 1	.071 4	0690
30	.0667	.064 5	.062 5	9 090.	.0588	.057 1	.055 5	.0540	.0526	.0513
40	.050	.0488	.047 6	.046 5	.045 5	.044 4	.0435	.0426	.041 7	.0408
20	.0400	.039 2	.038 5	.037 7	.037 0	.0364	.035 7	.035 1	.0345	.033 9
8	.033 3	.0328	.0323	.031 7	.031 2	8 080.	.0303	8 620.	.029 4	0290
22	.0286	.0282	.027 8	.027 4	.027 0	.0267	.0263	0260	.n25 6	.025 3
8	.0250	.0247	.024 4	.024 1	.0238	.023 5	.023 3	.023 0	.022 7	.022 5
8	.022 2	.0220	.021 7	.021 5	.0213	.021 0	.020	.020	.020	.020

AT 2.5 VOLTS LOSS.

	οc	9	8	-	0	4	07	9	-	87
6	.277	.131	0.08	96	.051	.0424	.036	.031	.028	.025
80	.312.5	.1389	.089 2	.0658	.0521	.0431	.0368	.032 0	.028 4	.025 5
_ 1	.3571	.1470	.0926	9 290.	.0532	.0438	.0373	0325	.028 7	.0258
9	.4166	.1562	.0961	.069 4	.0543	.0446	.037	.0329	.029 1	0.0260
2	0 0000	.1667	1000	.071 4	.055 5	.045	.0384	.033 3	.029 4	.0263
4	.6250	.1786	.1042	.073 5	.0568	.0463	.039 1	.0338	.029 7	.0266
က	.833 3	.1923	.1087	.075 7	.058 1	.047 2	.039 7	.0342	.030 1	0269
7	1.2500	.2083	.1136	.0781	.059 5	.048 1	.0403	.034 7	.030 5	.027 2
-	2.5000	.227 2	.1190	9 080.	6 090.	.049 0	.0410	.035 2	030 6	.027 5
0	8	.250 0	.1250	.0833	.062 5	0020	7 140.	.035 7	.031 2	.027 8
Current.	0	10	82	တ္တ	40	20	8	2	- 08	8

AT 3 VOLTS LOSS.

Current.	0	1	2	ဇာ	4	2	9	7	80	6
0	8	3.0000	1.5000	1.000 0	.750 0	0 009.	.500 0	.4286	.3750	.333 3
10	.300 0	.272.7	.250 0	.2308	.2143	200 0	.187 5	.1765	.1667	.1579
20	.1500	.1429	.1364	.1304	.1250	.120 0	.1154	.1111	.1071	.1034
30	.1000	8 960.	.093 7	6 060:	.088	.085 7	.0833	.081	6 8 20.	6 920.
9	.075.0	.0732	.071 4	8 690.	2 890.	2 990.	.065 2	.0638	.062 5	.0612
22	0000	.0588	7 2 20.	.0566	.055 6	.0546	.0536	.0526	.051 7	8 020.
8	.050	.049 2	.0484	.047 6	.0469	.0462	.045 5	.0448	.044	.043 5
20	.0429	.0423	.0417	.041 1	.040 5	0400	.039 5	0390	.038 5	.038
8	.037 5	.037 0	.036	.0362	.035 7	.0353	.034 9	.034 5	.034 1	0337
8.	.033 3	.0330	0326	.0323	.0319	.031 6	.031 2	.030	9 080.	0303

AT 3.5 VOLTS LOSS.

	0	-	61	က	4	ro	9	7	∞	6
0	8	3.5000	1.7500	1.1667	.8750	.7000	.583 3	.500 0	.437 5	.388
10	3500	.318 2	.291 7	269 2	.250 0	.233 3	.2188	.205	.1944	.1842
	1750	.1667	.1591	.152 2	.1458	.1400	.1346	.1296	.1250	.1207
	1167	.1129	.1094	.1060	-1029	1000	.097 2	.0946	.092	2 680.
40	.087 5	.085 4	.0833	.081 4	.079 5	8 2 2 0 .	.076	.074 5	.0729	.0714
	0 0 0 0 0	9 890.	.0673	0 990.	.064 8	.063 6	.062 5	.061 4	.060 3	.0593
	.0583	.057 4	.056 5	.0556	.0547	.0538	.053 0	.052 2	.0515	.050 7
	.050	.0493	.048 6	.0479	.0473	.0467	.0460	.045 5	.044 9	.0443
	.0437	.043 2	.042 7	.042 2	.0417	.0412	.040	.040 2	.0398	.039 3
	6 880.	.038 5	0380	.037 6	.037 2	.0368	.036 5	.036 1	.035 7	.0354

AT 4 VOLTS LOSS.

Current.	0	-	61	က	4	2	9	-	«	6
0	8	4.0000	2.0000	1.3333	1.0000	0 008	7 999.	.5714	.500 0	.444
10	.400 0	.3636	.333 3	.307 7	.285 7	.266 7	.2500	.235 3	.222 2	.2105
20	.200	.1905	.1818	.1739	.1667	1600	.1538	.148 2	.1428	.1379
- 08	.1333	.1290	.125 0	.121 2	.1176	.1143	.1111	.1081	.1053	.1026
9	.100 0	9 260.	.095 2	.093 0	6 060	6 880.	0 280.	.0851	.0833	.0816
20	080.	.0784	9920.	.075 5	.0741	.0727	.071 4	.070	0 690.	.0678
8	.066 7	.065	.064 5	.063 5	.062 5	.061 5	9 090.	.059 7	.0588	0580
20	.057 1	.0563	.055 6	.0548	.054 1	.0533	.0526	.0519	.0513	050.0
8	020.	.0494	.0488	.0482	.047 6	.047 1	.046 5	.0460	.045 5	.0449
06	.044 4	.0440	.0435	.0430	.0426	.0421	.041 7	.0412	.0408	.040

AT 4.5 VOLTS LOSS.

Current.	0	1	2	8	4	2	9	7	•	6
0	8	4.5000	2.2500	1.5000	1.1250	0.006.	7500	.6428	.5625	.500 0
10	.4500	.409 1	.3750	.3461	.3214	.300	2812	.264 7	2500	.2368
ಜ	-2250	.2143	204 5	1957	.187 5	.180	.1731	.1667	1607	.1552
8	0.021	.1452	.1406	.1364	.1323	.1285	.1250	.121 6	.1184	.1154
40	.1125	1097	.107 1	.1047	.1023	.100 0	8 260.	.0957	.093 7	8 160.
56	0.060	.0882	.086 5	.0849	.083 3	.0818	.080	9820.	9 2 2 2 0	.0763
99	.0750	.0738	.0726	.071 4	.0703	.069	.068 2	.067 2	.0662	.065 2
2	.0643	.0634	.062 5	.061	8 090.	0000	.059 2	.0584	.057 7	0569
8	.0562	.0556	.0549	.0542	.053 5	.0529	.0523	.051 7	.051 1	050.
8	0020	.049 4	.0489	.0484	.047 9	.047 4	.0469	.0464	.0459	.0455

AT 5 VOLTS LOSS.

Current.	0	-	63	es	4	ro	9	7	•	6
0	8	5.0000	2.5000	1.6667	1.2500	1.0000	.8333	.7143	.6250	.555 5
10	.500 0	.454 5	.4167	.3846	.3571	.333 3	.3125	294 1	.277 8	.263 2
82	.2500	.2381	.227 2	.217 4	.2083	2000	.1923	.185 2	.1786	.1724
30	.1667	.1613	.1562	.1515	.147 0	.1429	.1389	.1351	.1316	.1282
40	.1250	.1220	.1190	.1163	.1136	.1111	.1087	.1064	.1042	.1020
ا ا	.100	0.860	.0961	.0944	.0926	6 060	.0893	7 780.	.0862	.0848
8	.0833	.0820	9 080.	4 620.	.0781	6 9 20.	.0758	.0746	.073 5	.0725
2	.071 4	.070	.069 4	.068 5	9 290.	.066 7	.0658	.0649	.064 1	.0633
8	.0625	.061 7	.061	.060 2	0595	.0588	.058 1	.057 5	.0568	.0562
8.	.0556	.0550	.0543	.053 7	.0532	.0526	.052 1	.0515	.0510	0505

AT 5.5 VOLTS LOSS.

Current.	•	-	63	က	4	·c	9	7	∞	6
0	8	5.5000	2.7500	1.8333	1.3750	1.1000	916.	7857	.687 5	.6111
10	.5500	.500 0	.4583	.423 0	.392 9	.3667	.343 7	.323 5	.305 6	2895
ဂ္ဂ	.2750	9 192.	.250 0	.239 1	.229 2	.220 0	.2115	.203 7	.1964	.1897
8	.1833	.1774	171.9	1667	.1618	.1571	.1528	.1486	1447	.1410
- -	.137 5	.1341	.1309	.127 9	.1250	.122 2	9611.	.1170	.1146	.1122
20	.1100	.107 8	.1058	.1038	101 9	.1000	.098	.0965	.0948	.093 2
8	.091 7	.090	.0887	.087 3	.085	.0846	.083 3	.082	6 080.	7 620.
2	.078 5	0777 5	.0764	.0753	.0743	.0733	.0724	.071 4	.070 5	9 690:
8	.068 7	6 290.	.067 1	.0663	.065 5	7 490.	.0640	.063 2	.0625	.0618
6	.061 1	.060 4	.0598	0591	.058 5	6 220.	.0573	.0567	.0561	.0556

AT 6 VOLTS LOSS.

Current.	•	-	7	60	4	2	9	7	∞	6
0	8	6.000 0	3.0000	2.0000	1.5000	1.2000	1.0000	.857 1	.7500	7 999.
10	0009	.5455	.500 0	.4615	.428 6	.400 0	.375 0	.352 9	33333	.3158
ଛ	.300 0	.285 7	.2727	.2609	.250 0	.2400	.2308	.222 2	.2143	2069
30	2000	.1936	.187 5	.1818	.1765	.1714	.1667	.1622	.157 9	.1538
9	.150 0	.1463	.1429	.139 5	.1364	.1333	.1305	.127 7	.1250	.1224
20	.1200	.117.7	.1154	.113 2	.1111	.1091	1071	.1053	.103 5	.1017
8	.100	.098.4	8 960.	.095 2	.093 8	.0923	6 060.	9 680.	.0882	0870
2	.085 7	.084 5	.0833	.082 2	.081	080.	0 620	0.820	6 920.	0 9 20.
&	.0220	.074 1	.073 2	.0723	.071 4	9 020.	8 690.	0 690.	.068 2	.067 4
- 6	.066 7	0 990.	.065 2	.0645	.0638	.063 2	.062 5	.0619	.0612	9090.

AT 6.5 VOLTS LOSS.

Current.	0	-	8	8	4	2	9	7	80	6
0	8	6.5000	3.2500	2.1667	1.6250	1.3000	1.0833	.928 5	8125	722.2
91	.650 0	.5909	.541 7	.500 0	.4643	4333	.4063	.382 4	.361 1	.3421
ສ	.325 0	.309 5	.295 5	.282 6	.2708	.260 0	.250 0	2407	.2321	224 1
30	2167	200 7	2031	.1970	.191	.185 7	.1806	.1757	1710	.1667
40	.1625	.1585	.1548	.151 2	.1477	1444	.1413	.1383	.1354	.1327
32	.130 0	.127 5	.1250	.1226	.1204	.118 2	.1161	.1140	.1120	.1102
8	.1083	.1066	.1048	1032	.101	.1000	.098 5	0 260.	.095 7	2 460
2	.0929	.091 5	.0903	0 680.	8 280.	.086 7	.085 5	.084 4	.0833	.0823
8	.0813	.080	.0793	.0783	.077 4	.076 5	.075 6	.0747	073 9	.0730
8	0722	.071 4	9 0 2 0.	6 690.	.0691	.068 4	.067 7	0 290.	.0663	.065 7

AT 7 VOLTS LOSS.

urrent.	0	-	61	က	4	ı,	9	7	∞	6
0	8	7.000 0	3.5000	2.3333	1.7500	1.4000	1.1667	1.000 0	.8750	8 222
10	.7000	.6364	.5833	.538 5	.500 0	.466 7	.437 5	.4118	.388	.3684
8	.3500	.333 3	.3182	.304 5	291 7	.280 0	269 2	.2593	.250 0	.2414
30	.233 3	.2258	.2188	.212	.205 9	200 0	.r944	.1892	.1842	1795
9	.1750	.1707	1667	.1628	.1591	.155 6	.1522	.1490	.1458	.1429
20	.1400	.1373	.1346	.1321	.1296	.1273	.1250	.1228	.1207	.1186
8	.1167	.1148	.1129	.1111	.1094	.107 7	.1061	.1045	.1030	.1014
22	.100 0	9 860.	.097 2	.095 9	.0946	.0933	.0921	6 060.	7 680.	9880.
8	.087 5	.0864	.085 4	.084 4	.0833	.0824	.081 4	.080	.079 5	.0787
8	.0778	6 9 2 0 .	.0761	.0753	.0745	.0737	072 9	.072 2	.071 4	.070

AT 7.5 VOLTS LOSS.

Current.	•	-	5	es	4	2	9	-	× ×	6
0	8	7.5000	3.7500	2.5000	1.8750	1.5000	1.2500	1.0714	.937 5	.833 3
10	.750 0	.6818	.625 0	.5769	.535 7	.500 0	.468 7	.4412	.4167	.394 7
20	.3750	.357 1	.3409	.3261	.3125	.300 0	.288 5	.2778	9 292.	.2586
30	.2500	.242 0	.234 4	.227 3	.220 6	.2143	.2083	.2027	.197 4	.1923
40	.187 5	.1829	.1786	.1744	.1705	.1667	.1630	.159 6	.1562	.1530
26	.1500	.1471	.1442	.1415	.1389	.1364	.1339	.1316	.1293	.127 1
8	.1250	.1230	.121 0	.1190	.1172	.1154	.1136	9 111.	.1103	.1087
20	.1071	.1056	.1042	.1028	1014	1000	2 860	.097 4	.0962	.095 0
08	.093 7	0.0926	.0915	4 060.	.089 3	.0882	.087 2	.0862	.085 2	.0843
8	.0833	.082 4	.081 5	9 080.	8 620.	6 8 20.	.0781	.077 3	.076 5	.0758

AT 8 VOLTS LOSS.

Current.	0	-	2	8	4	£	9	7	8	6
0	8	8.000 0	4.0000	2.6667	2.000 0	1.600 0	1.333.3	1.1429	1.000 0	888.9
2	0 008.	.7273	2 999.	.615 4	.571 4	533.3	2000	470 6	444	421 1
ଛ	.400	.3810	.363 6	347 8	3333	3200	307.7	2963	285 7	975.9
င္က :	.2667	.2581	.250 0	.2424	.235 3	.228 6	222 2	2162	210 6	205.1
육	.200 0	.1951	.1905	.1860	.1818	.1778	.1739	.1702	.1667	.1633
22	.1600	.1569	.1538	.1510	148 2	145.5	142.9	1403	137.9	135.6
8	.1333	.1311	.1290	.1270	.1250	.1230	.121 2	1194	117.7	1159
2	.1143	.1127	.1111	.1096	.1081	1067	.1053	1039	102.6	1013
3 3	.1000	8 860.	9 260.	.0964	.095 2	.094	.093 0	.092 0	6 060	6 680
€	6880	.087 9	0 280.	0 980.	.0851	.0842	.0833	.082 5	.0816	8080

AT 8.5 VOLTS LOSS.

	i			AT 8.	S VOLTE	S LOSS.				
Current.	0	-	67	က	4	5	9	7	8 0	6
0	8	8.5000	4.2500	2.8333	2.1250	1,700 0	1.416.7	1 2143	1 069.5	-044.4
01	.8500	.7727	.7083	.653.8	.607	5667	5312	200	479.9	447.4
02 []	.4250	.4048	.3864	.369 6	3542	3400	326.9	3148	303.6	993.1
_	.283 3	.274 2	.265 6	.257 6	2500	2429	2361	2 666	253 7	9170
8	.212.5	.207 3	.202 4	1977	.193 2	1889	.1848	1808	1771.	.1735
50	.1700	.1667	.163 5	.1604	.157 4	1545	151.8	1491	1466	1441
09 //	.1417	.1393	.1371	.1349	.1328	.1308	1288	126.9	1250	193.9
22	.1214	7611.	.1181	.1164	.1149	.1133	.1118	1104	1090	107.6
€	.1062	.1049	.1037	.1024	.1012	.100	8 860.	2 260	9960	0.05
3 .	- 0.094 4	.093 4	.0924	.0914	4 060.	.089 5	.088 5	087 6	086.7	085.0

AT 9 VOLTS LOSS.

Current.	0	1	61	ಣ	4	ъ	9	7	•	6
0	8	9.0000	4.5000	3.0000	2.2500	1.8000	1.5000	1.285 7	1.1250	1.0000
10	0 006:	.8182	.750 0	.6923	.6429	0 009.	.562 5	.529 4	.500 0	.4737
20	.450 0	.4286	.4091	.3913	.375 0	.360 0	.3461	.333 3	.3214	3103
ဓ္ဌ	300 0	.2903	.2813	.272.7	.264 7	.257 1	.2500	.243 2	.2368	.2308
40	.225 0	219 5	.2143	.2093	204 5	.200 0	.1957	.191 5	.187 5	.1837
20	.1800	.1766	.1731	.1698	.1667	.1637	7 091.	.1579	.155 2	.1525
09	.1500	.147 5	.1452	.1429	.1406	.138 5	.1364	.1343	.1324	.1304
02	.1286	.1268	.1250	.1234	.121 6	.1200	.1184	.1169	1154	.1139
8	.1125	.1111	.1098	.1084	.107 1	.1059	.1047	.1033	.1023	.101
6	1000	6 860	8 260	8 960	.095 7	094.7	.093 8	092.8	8 160	6 060

AT 9.5 VOLTS LOSS.

Current.	0	1	2	8	4	2	9	7	80	6
0	8	9.5000	4.7500	3.1667	2.3750	1.9000	1.5833	1.357 2	1.187 5	1.0556
10	.950 0	.863 6	7 167.	.7308	.678 6	.633 3	.593 7	.5588	.5278	.500
20	.4750	.4524	.4318	.4130	.3958	.380 0	.365 4	.3519	.339 3	.3276
90	.3167	.306 5	.2969	9 282.	279 4	.271 4	.263 9	.2568	.2500	.243 6
40	.237 5	.231 7	2562	.220 9	.2159	.2111	2065	2021	.1979	.193 8
26	.1900	.1863	.1827	.179 2	.1759	.1727	.1696	.1667	.1638	.1610
8	.1583	.155 7	.153 2	.1508	.1484	.1462	.1439	.1418	.1397	.137 7
2	.135 7	.1338	.1320	.1301	.1284	.1267	.1250	.1234	.121 6	.1203
 	1187	.1173	.1159	.1145	.1131	.1118	.1105	.1092	.1080	.1067
8	.1056	.1044	.1033	.102 2	.101	1000	6 860.	6 260.	6 960.	.095

AT 10 VOLTS LOSS.

Current.	0	П	61	က	4	z,	9	7	∞	6
0	8	10.000 0	5.000 0	3.333 3	2.5000	2.0000	1.6667	1.4286	1.2500	1.1111
10	1.0000	.909 1	.833 3	.7692	.7143	2 999.	.625 0	.588 2	.555 6	.5263
20	.500 0	.4762	.4545	.4348	.4167	.400 0	.384 6	.3704	.3571	.3448
8	.333 3	.3226	.312 5	.303 0	294 1	.285 7	.2778	.2703	.2632	.2564
40	.2500	.2439	.238 1	.232 6	.227 3	.222 2	.2174	.2128	.2083	.2041
20	.200	.1961	.1923	.1887	.1852	.1818	.1786	.1754	.1724	.1695
89	.1667	.1639	.1613	.1587	.1563	.1538	.151 5	.1493	.1471	.1449
20	.1429	.1408	.1389	.137 0	.1351	.1333	.1316	.1299	.1282	.1266
80	.1250	.1235	1220	.1205	.1190	.1176	.1163	.1149	.1136	.1124
06	.1111	.1099	1087	.107 5	.1064	.1053	.1042	.1031	.1020	0101
100	.1000	0 660.	0 860.	.097 1	.0962	.095 2	.0943	.093 5	.0926	7 160.
110	6 060	1060.	.089	.088 5	7 280.	0820	.0862	.085 5	.0847	.084 0
120	.0833	.0826	.082	.0813	9 080	0 080.	.079 4	7 870.	.0781	.077 5
130	6 9 20.	.0763	.0758	.075 2	.0746	.074 1	.073 5	.073 0	.0725	.071
140	.071 4	6 020.	.070	6 690.	.0694	0 690.	.068 5	0890	9 290.	.067 1
150	2 990.	.0662	.065 8	.065 4	.0649	.064 5	.0641	.063 7	.063 3	.0629
160	.062 5	.0621	.061 7	.0613	.0610	9 090.	.0602	.059	.059 5	.0592
170	.0588	.0585	.0581	.0578	.057 5	.0571	.0568	.056 5	.0562	0559
180	.0556	.055 2	.0549	.0546	.0543	.0541	.0538	.053 5	.0532	0529
190	.0526	.0524	.0521	.0518	.0515	.0513	.0510	.050 8	.050 5	.0503

LT 11 VOLTS LOSS.

6.	1.222 2	.5789	.3793	.2820	.224 5	.1864	.1594	.1392	.1236	.1111	1009	.092 4	.0853	, (10	.079 1	.079 1	.079 1 .073 8 .069 2	.079 1 .073 8 .069 2 .065 1	.079 1 .073 8 .069 2 .065 1	.0791 .0738 .0692 .0651 .0615
,	1.375 0	.611 1	.3929	.289 5	2592	1897	.1618	.1410	.1250	.1122	9 101.	.093 2	.085	1	7.670.	.0797	.0797 .0743 .0696	.0797 .0743 .0696	.0797 .0743 .0696 .0655	.069 6 .065 5 .061 8
-	1.571 5	.647 0	4074	.2973	.234 0	.193 0	.1642	.1429	.1264	.1134	.1028	.094 0	9 980.	6 000	0000	.050.	.074 8	.070 . .065 9	.070 1 .070 1 .065 9	.070 1 .070 1 .065 9 .062 1
9	1.833.3	.687.5	423 1	305.6	2391	1964	1667	1447	127.9	.1146	.103.8	.0948	.0873	6 080		.075 4	.070 5	.075 4 .070 5 .066 2	.070 5 .066 2 .062 5	.070 5 .070 5 .066 2 .062 5
2	2.2000	.733 4	.4400	.314.3	244 4	2000	1692	.1467	1294	.1158	.1048	.095 7	0880	.081 5		.075 9	0759	.075 9 .071 0 .066 7	.075 9 .066 7 .062 9	.075 9 .071 0 .066 7 .062 9 .059 5
4	2.7500	7857	4583	323 5	.250 0	.203 7	171 9	.1486	.1310	.1170	.1058	.096 5	.0887	.082		.0764	.0764	.0764	.0764 .0671 .0632	.0764 .0671 .0632 .0638
೯	3.6667	.8461	4783	3333	.255 8	.207 6	.174 6	.1507	.1325	1183	.1068	.097 5	.089 3	.082 7	0000	.076	.076 9	.076 9	.071 9 .067 5 .063 6	.070. .067 5 .063 6 .063 6
61	5.5000	7 916.	.500 0	.343.8	2619	.2115	.177 4	.1528	.1341	9611.	.107 8	.098 2	2 060	.0833	7.4.7	# 15.	.0723	.0723	.0723 .0679 .0639	.067 9 .063 9 .060 9
	11.000 0	1.000 0	.523 8	3549	.2683	.215 7	.1803	.1550	.1358	.1209	.1089	.099	6 060.	.0840	0.280	2010.	.0728	.0728	.0728 .0683 .0643	.0728 .0683 .0643 .0608
0	8	1.1000	.5500	.3667	.275 0	.220 0	.1834	.1572	.137 5	.1222	.1100	.1000	.0916	.0846	070 5	0000	.0734	0734	.073 4 .068 8 .064 7	.073 4 .068 8 .064 7 .061 2
Current.	0	10	20	30	9	20	8	2	08	6	100	110	120	130	140	P	150	150 160	150 160 170	150 150 170 180

AT 12 VOLTS LOSS.

Current.	0	г	8	က	4	2	9	4	œ	6
0	8	12.0000	0.000.9	4.000 0	3.000 0	2.4000	2.000 0	1.7144	1.5000	1.3333
10	1.2000	1.0909	1.0000	.923 0	.857 1	.800	.7500	.7058	2 999.	.631 5
8	0009.	.5714	.545 5	.5217	.500 0	.480 0	.451 6	.4444	.428 5	.4138
93	.4000	.387 1	.3750	.363 6	.3529	.3429	.3334	.3243	.3158	.307 7
4	300 0	.292 7	.285 7	279 1	.272.7	.266 6	3008	.2553	.2499	.2500
යි	.2400	.235 3	2307	.2264	.222 2	.2182	.2143	2104	.2068	.2034
8	2000	1967	.1935	.1905	.187 5	.1846	.181	1791	.1765	.1739
2	.1715	.1690	.1667	.1644	.1621	.1600	.1579	.1559	.1538	.1519
8	.1500	.1482	.1464	.1446	.1428	.1412	.1395	.1379	.1364	.1348
8	.1333	.131 9	.130 5	.1291	.127 6	.1263	.1250	.1237	.1224	.1212
100	.1200	.1188	.1176	.1165	.1154	.1143	.1132	.1122	.1112	.1101
110	.1091	.1081	.1071	.1062	.1053	.1044	.1034	.1027	.1017	300.0
120	.1000	2 660.	.0984	.097 5	8 960.	0 960.	.095 2	.094 5	.093 7	0630
130	0923	.0916	0010	.090 2	9 680.	6 880.	.0884	9 280.	0840	0863
140	.085 7	.0851	.084 5	.083	.0833	.0828	.082	.0816	.081	080.2
150	0.080	.079 4	6 8 20.	.0784	6 220.	.077 5	6940	.0764	075 9	.075 5
160	.0750	.0744	.0741	.073 6	.073 2	.0727	.0723	6 120.	.0725	.071 0
170	9 020.	.070	7 690.	.069 4	0 690.	.068 5	.0682	6 290	.067 4	.0671
180	2 990.	.0662	.0659	.065 6	.0651	.0649	.064 5	.0642	.0638	.0635
130	.063 2	.0628	.0625	.062 2	.0618	.061 5	.0612	0 190.	.060 7	060.5

AT 13 VOLTS LOSS.

	0		81	က	4	ď	9	4	œ	6
<u> </u> 	8	13.000 0	6.500 0	4.333 2	3.2500	2.6000	2.1667	1.8571	1.625 0	1.444 4
_	3000	1.1818	1.0833	1.0000	.928 6	2 998.	.8125	7647	.722 2	.684 2
	6500	.619	.590 9	.565 2	.541 7	.5200	.500 0	.481 5	.4643	.4483
	433 2	4194	.4063	.393 9	.382 2	.371 4	.361 1	.351 4	.3421	.333 3
94	.3250	.3171	.309 5	.302 2	.295 5	.2889	282 6	2766	.2708	.2653
_	2600	.254 9	.250 0	.2453	240 7	.2364	.232 1	.228 1	.224 1	.2203
	2167	.213 1	209 7	.2064	.2031	.200 0	.1970	.1940	1912	.1884
	1857	.1831	.1806	.1781	.1757	.1733	.1711	.1688	.1667	.1646
	1625	.1605	.1585	.1566	.1548	.1529	.1512	.1494	.147 7	.1461
	1444	.1429	.1413	.1398	.1383	.1368	.1354	.1340	.1327	.1313
<u> </u> _	1300	.1287	.127 4	.1262	.1250	.1238	.1226	.121 5	.1204	.1193
	1182	.1171	.1161	.1150	.1140	.1130	.1121	.1111	.1102	.1092
	1083	.107 4	0.000	.1057	.1048	.1040	.1032	.1024	.101 6	300.0
	1000	.099 2	.098 5	2 260.	0 260.	.0963	.0956	.0949	.0942	.0935
	092 9	.092 2	.091 5	6 060:	.090	.089 7	080.	.0884	.087 8	0872
	2 980	.0861	.085 5	.085	.084 4	.0839	.0833	.0828	.0823	.0818
	0813	2 080.	.080	8 620.	.0793	8 8 20.	.0783	8 220.	.077 4	6920
	0765	0920	.0756	.0751	.0747	.0743	.0739	.073 4	.0730	0726
	072.2	.0718	.071 4	0120.	.070	.070	6 690.	.069 5	.0691	6 890.
_	0684	.068 1	.0678	.0674	0.000	9 990.	.0663	0990.	.065 7	.0653

AT 14 VOLTS LOSS.

Current.	0	H	63	89	4	ıç	9	7	•	6
0	8	14.0000	7.000 0	4.6667	3.5000	2.8000	2.333 3	2.000 0	1.7500	1.555 5
20	1.4000	1.272.7	1.1667	1.0768	1.000 0	.933 3	.8750	.823 5	.777 8	.7368
ଛ	.700 0	2999.	.6363	.608 7	.5833	.560 0	.5384	.5186	.500 0	.482 7
99	.4666	.4516	.437 5	.4242	.4117	.400 0	.388	.3784	.368 5	.3590
40	.3500	.3415	.333 3	.325 6	.3182	.3110	.304 4	.297 9	.291 6	.285 7
20	.280 0	.274 5	269 2	.264 2	.2593	.254 5	.2500	.245 6	.2414	.237 3
8	.2333	.229 5	.225 8	.222 2	.2188	.2154	.2121	209 0	.205 9	202.9
2	200 0	.1972	.1945	8 161.	1891	.1867	.1842	.181	.1795	.1772
8	.1750	.1728	.1707	.1687	.1667	.1647	.1628	.1609	.1591	.1573
6	.155 5	.1538	.1522	.1506	.1490	.1474	.1458	.1443	.1429	.1414
100	.1400	.1386	.137 2	.1359	.1345	.1333	.1321	.1308	.1296	.1284
110	.1273	.1261	.1250	.1239	.1228	.1218	.1207	.1197	.1186	.117.7
120	.1167	.1157	.1148	.1138	.1129	.1120	.1111	.1102	.1094	.108 5
130	.107 7	.1069	.1061	.1053	.1045	.1037	.1030	.1022	.1015	.1007
140	1000	.0993	9860	6 260.	.097 2	.096 5	.095	.0953	.0946	.0940
150	.0933	.092 7	.0921	.0916	6 060.	.090 3	7 680.	.089	9880.	.0881
160	.087 5	6 980.	.0864	.0859	.085 4	.0848	.084 4	6 880.	.0833	0828
170	.0823	.0819	.081 4	6 080.	.080	0800	.079 5	.079	7 870.	0782
180	7 2 2 2 2	.077 4	.0768	.0765	0 920.	.075 7	.0753	.0749	.074 5	.074 1
190	.0736	.0734	.0729	.0725	.0721	.0718	.071 4	.071 1	2 020.	.0704

AT 15 VOLTS LOSS.

0 ∞ 15,000 0 7,500 0 15,000 0 10 1,500 0 1,363 6 1,250 0 1,153 8 20 7,50 0 7,14 3 681 8 652 2 30 5,00 0 7,44 3 681 8 652 2 40 375 0 365 9 365 9 3454 5 50 300 0 294 1 288 4 283 1 60 250 0 245 9 241 9 283 1 70 214 3 211 3 208 4 205 5 80 187 5 185 2 183 0 180 8 90 166 6 165 0 163 0 161 3 110 136 4 135 1 132 9 132 8 120 125 0 124 0 123 9 121 8 130 112 4 113 7 112 8	15.000 0 1.363 6 7.14 3 7.14 3 7.14 3 7.14 3 7.85 9 7.85 9 7.85 2 1.85 2 1.85 2 1.85 2 1.85 2 1.85 2	7.500 0 1.250 0 .681 8 .468 8 .357 1 288 4 .241 9	5.000 0 1.153 8 .652 2 .454 5 .348 9	3.750 0						
1500 1.363 6 1.250 0 1.250 0 1.250 0 1.250 0 1.250 0 1.250 0 1.254 1.250 0 1.255 0	1.363 6 7.14 3 7.14 3 7.14 3 7.14 3 7.14 3 7.24 1 7.24 1 7	1.250 0 .681 8 .468 8 .357 1 .288 4 .241 9	1.153 8 .652 2 .454 5 .348 9	1.071 4	3.000 0	2.5000	2.1430	1.8750	1.6667	J
.750 0 .714 3 .681 8 .500 0 .484 0 .468 8 .375 0 .365 9 .357 1 .284 1 .288 4 .250 0 .245 9 .241 9 .214 3 .211 3 .208 4 .187 5 .185 2 .185 0 .168 6 .165 0 .168 0 .125 0 .1	294 1 245 9	.6818 .4688 .3571 .2884 .2419	.652 2 .454 5 .348 9		1.000 0	.937 5	.8823	.833 3	.789 4	O
500 0 .484 0 .468 8 375 0 .365 9 .357 1 300 0 .294 1 .288 4 250 0 .245 9 .241 9 214 3 .211 3 .208 4 .187 5 .185 2 .183 0 .166 6 .165 0 .163 0 .150 0 .148 5 .147 0 .125 0 .124 0 .123 0 .154 0 .125 0 .123 0 .115 4 .113 7	284 0 245 9 245 9 245 9 211 3 186 2 165 0	.468 8 .357 1 .288 4 .241 9	.3489	.625 1	0 009	.5770	555 6	.535 6	5173	HI
	.365 9 .294 1 .245 9 .211 3 .185 2 .165 0	.357 1 .288 4 .241 9 .208 4	.3489	.441 1	.428 6	.4167	4054	.394 7	.384 6	١
.300 0 .294 1 .288 4 .251 0 .245 9 .241 9 .2	2941 2459 2113 1852 1650	.288 4 .241 9 .208 4		.3409	.333 3	.326 1	.3192	.3125	.3061	А.
250 0 245 9 241 9 2143 2143 2185 2 188 0 166 6 166 0 148 5 148 5 135 1 155 0 125 0 125 0 115 4 115 4 115 4 113 7	.245 9 .211 3 .185 2 .165 0	.241 9 .208 4	.283 1	.277 8	.272.8	.2680	.2631	.2586	.254 2	K
	.2113 .1852 .1650	2084	.238 1	.234 4	.2308	.227 3	.223 9	.220 6	.217 4	OF
.1875 .1852 .1830 .1666 .1650 .1630 .1500 .1485 .1470 .1250 .1240 .1230 .1154 .1137	.185 2 .165 0		.205 5	.2026	.2000	.1974	1949	.1923	.1900	В
.166 6 .165 0 .163 0 .150 0 .148 5 .147 0 .136 4 .135 1 .133 9 .125 0 .124 0 .123 0 .115 4 .113 7	.148 5	.1830	.1808	.1785	.1765	.1744	.1724	.1705	.1686	LΙ
.150 0 .148 5 .147 0 .136 4 .135 1 .133 9 .125 0 .124 0 .123 0 .115 4 .115 4 .113 7	.1485	.1630	.1613	.1596	.1579	.1562	.1546	.1530	.1515	NU
.1364 .1351 .1339 .1250 .1240 .1230 .1154 .1145 .1137	-	.1470	.1456	.1443	.1429	.1415	.1403	1390	.1376	i S
.1250 .1240 .1230 .1154 .1145 .1137	1001.	.1339	.1328	.1316	.130 5	.1293	.1281	.127 1	.1260	.5
115 4 .114 5 .113 7	.1240	.123 0	.121 9	.121 0	.1200	.1190	.1181	.1171	.1163	Or
0 101	.1145	.1137	.1128	.1120	.1111	.1103	.1095	.1087	.1079	G
9 601. 4 901. 1 701.	.1064	0.1056	.1049	.1041	.103 5	.1028	.1020	.101 4	0.000	C
7 300. 099 3 .098 7	.099 3	7 860.	0860	.097 4	8 960.	.0961	.095 5	.0949	.094 4	υ.
.0938 .0931 .0926	.093 1	.0926	0920	.091 5	6 060.	.0903	6 680.	.089	8888	
.0883 .0878 .0871	.0878	.087 1	2 980.	.0862	.085 7	.0853	.0848	.0843	.083	
.083 4 .082 8 .082 4	.0828	.082 4	.082	.081 5	.081 1	.080	.080	8 640.	.079 4	
079 0 078 6 078 1	9 8 20.	.078	8 220.	.077 4	6 9 20.	.076 5	.0762	.0758	.075 5	

AT 16 VOLTS LOSS.

Current.	0	٦	81	ಣ	4	ro	9	4	œ	6
0	8	15,000 0	8.0000	5.333 3	4.000 0	3.2000	2.6667	2.285 7	2.000 0	1.777 8
10	1.6000	1.4545	1.333 2	1.2207	1.1428	1.0668	1.000 0	.941 1	0 688.	.8420
20	0 008.	6 192	.727 3	.695 7	.666	.640 0	.6154	.5926	.5713	.5517
90	.5333	.5162	.500 0	.484 8	.4706	.457 2	.444 5	.432 4	.421 0	.4102
40	.400 0	3903	380 9	.372 1	.363 6	3.55	.3478	.340 5	.333 3	.3265
20	.320 0	.3137	.307 7	.3019	2963	290 9	.2858	280 7	.275 8	2712
8	2667	.2623	.2580	.254 0	-2500	.2462	.242 5	.2388	.235 3	2319
2	.2286	.225 3	.222 2	2192	.2162	.2133	.2105	.2078	.2051	202.5
08 5	.2000	.197.5	.1951	.1928	.1905	.1882	.1860	.1839	.1818	.1798
6.	.1778	.1758	.1740	.1720	.1702	.1684	.1663	.1649	.163 2	.1616
100	.1600	.1584	.1568	.155 3	.153 9	.1523	.1509	.1495	.148 2	.1468
110	.1455	.1441	.1429	.1416	.1404	.1391	.1379	.1367	.1356	.1344
120	.1333	.132 2	.131 2	.1300	.1290	.1280	.127 0	.1260	.1250	.1241
130	.1231	.1221	.121 2	.1205	.1194	.1185	.1177	.1168	.1160	.1151
140	.1143	.1135	.1127	6 111.	1111	.1104	.1096	.1089	.1081	.107 4
150	.1067	.1059	.1053	.1046	.103 9	.103 2	.1025	9 101.	.1012	.1007
160	0.000	.0993	8 860.	.0981	9 2 60.	0 260.	.0963	.0958	.095 2	.0946
170	.094 1	.093	0630	.092 5	.092 0	.091 4	6 060.	.090	6 680.	.089
180	6 880.	.0884	6 280.	.087 4	6 980.	.086 5	.0861	.085 7	.0851	.084 7
190	.0842	.0838	.0833	.082	.0824	.082	.0816	.0813	6 080.	.0804

AT 17 VOLTS LOSS.

$ \begin{array}{c ccccccccccccccccccccccccccccccccccc$	Current.	. 0	1	7	eo	4	2	9	7	œ	6
$\begin{array}{c ccccccccccccccccccccccccccccccccccc$	0	8	17.0000	8.5000	5.6667	4.2500	3.4000	2.8333	2.428 6	2.1250	1.8889
$\begin{array}{c ccccccccccccccccccccccccccccccccccc$	10	1.7000	1.5454	1.4166	1.3077	1.2143	1.1333	1.0625	1.000 0	.944	894 7
$\begin{array}{c ccccccccccccccccccccccccccccccccccc$	8	.8500	.809 5	.7727	.7391	708 4	0 089	.653 9	.629 6	.607 2	.5862
.340 .333 .3270 .3864 .3777 .3696 .3617 .3542 .340 .3333 .3270 .3208 .3148 .3091 .3036 .2982 .2937 .2429 .2787 .2742 .2698 .2656 .2615 .2576 .2537 .2500 .2429 .2784 .2861 .2829 .2297 .2266 .2537 .2508 .2179 .188 .188 .1828 .2024 .2000 .1977 .1954 .1932 .170 .1683 .1666 .1650 .1635 .1771 .1753 .1754 .140 .1405 .1393 .1382 .1371 .1405 .1393 .1374 .130 .1297 .1288 .1278 .1269 .1250 .1241 .113 .111 .111 .111 .111 .1104 .1090 .1083 .1076 .106 .108 .108 .0977 .0966 .0969 .0969	ဓ	.5667	.5484	.5313	.515 1	2000	.485 7	.472.2	459 5	4474	435 9
$\begin{array}{c ccccccccccccccccccccccccccccccccccc$	9	.4250	.4146	.4048	.395 4	.3864	.377 7	.369 6	361 7	.3542	.3469
$\begin{array}{c ccccccccccccccccccccccccccccccccccc$	20	.340 0	.333 3	.327 0	.3208	.314.8	.3091	.303 6	2982	.293 1	288 1
$\begin{array}{c ccccccccccccccccccccccccccccccccccc$	8	.2833	2787	.2742	8 698	.265 6	.2615	.257 6	.253 7	.2500	2464
$\begin{array}{c ccccccccccccccccccccccccccccccccccc$	2	.2429	.2394	.2361	.232 9	7 623	.226	.223 7	.220 8	9 212	.215 2
$\begin{array}{c ccccccccccccccccccccccccccccccccccc$	8	.2125	506 6	.2073	2048	202	.200	.197 7	.1954	.193 2	0.191
$\begin{array}{c ccccccccccccccccccccccccccccccccccc$	8	.1889	.1868	.1848	.1828	.180	.179 0	.1771	.1753	.1735	.171 7
$\begin{array}{c ccccccccccccccccccccccccccccccccccc$	100	.1700	.1683	.1666	.1650	.1635	.1619	.1604	.1589	.1574	.1560
$\begin{array}{c ccccccccccccccccccccccccccccccccccc$	110	.1545	.1531	.1518	.1504	.1490	.1478	.1465	.1453	.1440	.1429
$\begin{array}{c ccccccccccccccccccccccccccccccccccc$	120	.1416	.1405	.1393	.1382	.1371	.1360	.1349	.133 9	.1328	.1318
$\begin{array}{c ccccccccccccccccccccccccccccccccccc$	130	30.8	.1297	.1288	.1278	.1269	.1259	.1250	.1241	.123 2	.1223
.1133 .1126 .1118 .1111 .1104 .1097 .1090 .1083 .1076 .1063 .1056 .1050 .1043 .1037 .1037 .1023 .1018 .1012 .1000 .0994 .0988 .0983 .0977 .0971 .0966 .0960 .0965 .0896 .0899 .0884 .0881 .0876 .0973 .0914 .0993 .0909	140	.1214	.1206	1197	.1189	.1181	.1172	.1164	.115 6	.1149	.1141
.106 3 .105 6 .105 0 .104 3 .103 7 .103 0 .102 3 .101 8 .101 2 .100 0 .099 4 .098 8 .098 3 .097 7 .097 1 .096 6 .096 0 .096 5 .094 4 .093 9 .093 4 .092 9 .092 4 .091 9 .091 4 .090 9 .090 4 .089 5 .089 0 .088 1 .087 6 .087 2 .086 7 .086 3 .086 3 .085 9	150	.1133	.1126	.1118	.1111	.1104	.1097	.1090	.1083	.107 6	.1069
$\begin{array}{c ccccccccccccccccccccccccccccccccccc$	160	.1063	1056	.1050	.1043	.103 7	.1030	.1023	.1018	.1012	0.000
. 094 4 . 093 9 . 093 4 . 092 9 . 092 4 . 091 9 . 091 4 . 090 9 . 090 4 . 089 5 . 089 0 . 088 5 . 088 1 . 087 6 . 087 2 . 086 7 . 086 3 . 085 9	170	.1000	.099 4	8 860.	.0983	2 260.	.097 1	9 960:	0 960.	.095 5	0950
0895 .0896 .0885 .0881 .0872 .0872 .0863 .0859	180	.094 4	.0939	.093 4	.0929	.092 4	9 160.	.091 4	6 060	.090	6 680.
	190	.089	0.680 -	.088 5	.0881	9 280.	.087 2	.086	.0863	082 9	.085 4

AT 18 VOLTS LOSS.

Current.	0	-	63	က	4	z,	9	4	∞	6
0	8	18.000 0	0.000.6	0.000.0	4.5000	3.6000	3.000 0	2.571 4	2.2500	2.000 0
10	1.800 0	1.6363	1.5000	1.384 6	1.2857	1.2000	1.1250	1.0588	1.000 0	.947 4
200	0006	857 1	8182	782.6	750 0	.720 0	.692.3	2 999	.6429	.6207
<u>ج</u>	0009	580 7	562.5	7.5	5994	5143	5000	.486 5	.473 7	.4615
9	.4500	.439 0	.428 6	.418 6	4091	.400 0	.3913	.383 0	.3750	.3673
520	360.0	359.9	346 2	339.6	333.3	397.3	321 4	315.8	.3103	. 3051
88	3000	2951	2903	285 7	2813	2769	2727	2687	.264 7	.2609
2	.257 1	253 5	2500	2466	243 2	2400	.2368	.233 8	.2308	.227 8
£	225 0	222 2	2195	2169	2143	2117	2093	2069	204 5	202.5
8	200 0	.1978	1957	.193 5	.1915	.1895	.187 5	.1856	.183 7	.1818
100	.1800	.1783	1765	.174.8	.173.1	.171 4	1698	.1682	.1667	.1651
110	.1636	.1622	1607	.1593	157 9	.1566	.1552	.1540	.1525	.1513
120	.1500	1488	147.5	1463	1452	.1440	.1429	.1417	.1406	.1395
130	.1385	.1374	.1364	135.3	.1343	.1333	.1323	.1314	.130 5	.1295
140	.128 5	.127 7	.1268	.125 9	.1250	.1241	.1233	.122 4	.121 6	.1208
150	.1200	.119.2	1184	117.7	.1169	.1161	.1153	.1147	.1139	.1132
160	.1125	.1118	1111	1104	1098	1001	.1084	.1078	.1071	.1065
170	.1059	.1052	1046	181	1034	.1029	.1023	7 101.	.101	000.00
180	1000	0994	6 860	0983	8 260	.0973	8 960.	.0962	.095 7	.0952
130	.0947	.0942	7 860.	.093 3	.092 7	.0923	.0918	.091 4	6 060.	090.2

AT 19 VOLTS LOSS.

	301	T 1.4	А.	n) II	D.	LI.	NO		Ö	O.	a	C	υ.				
6	2.1111	.655 2 487 2	.387 7	.3220	.275 4	2405	.2135	9191.	.1743	.1596	.1473	.1367	.1274	.1195	.1124	.1061	.1006	.0955
∞	2.375 0 1.055 5	.678 6	.3958	.327 6	2795	.243 6	.215 9	.1938	.1760	.1610	.1484	.137 7	.1284	.1203	.1131	.1067	.101	0 960
-	2.7144	7037	.4043	.333 3	.283 6	.2468	.2184	.1958	.1775	.1624	.1496	.1387	.1292	.121 0	.1138	.107 4	.101	.096 5
9	3.1667	.7308	.4130	.339 3	9 282	.250 0	.220 9	.197 5	.179 2	.1637	.1508	.1397	.1302	.121.7	.1144	.1085	.1022	6 960.
ro	3.800 0	760 0	422 2	.345 5	.2923	.2532	.2235	.200 0	.181	.1652	.1520	.1407	.1310	.1226	.1152	.1086	.1027	.097 4
4	4.7500	.791 7	.4318	.3518	6 967	.2567	.226 2	2021	.1827	.1667	.153 2	.1418	.131	.1234	.1159	1092	.103 2	6 260.
က	6.333 3 1.461 5	.8261	.4419	.358 5	.301 6	.2603	.229 0	.2043	.1844	.1682	.1544	.1428	.1329	.1242	.1166	.1098	.1038	.098 4
83	9.500 0 1.583 3	.863 6 793 8	.4523	.365 4	.3064	.2640	.231 7	.206 5	.1862	.1696	.1558	.1439	.1338	.1250	.1173	.1105	.1043	6 860.
H	19.000 0	.904 7	4634	.3726	.3115	.267 6	.234 6	.208 8	.1881	.171	.1570	.1450	.1347	.1258	.1180	.1112	.1048	.099 5
0	1.900 0	.950 0	.4750	.380 0	.3167	.271 5	.237 5	.2111	.190 0	.1737	.1582	.1462	.135 7	.1267	.1189	.1118	$9\bar{c}01$.	.100 0
Current.	0 01	ଛଛ	9	20	99	2	08	8	100	110	120	130	140	150	160	170	180	190

AT 20 VOLTS LOSS.

10 2.000 20 1.000 30 .666 7 40 .500 0	20.000 0 1.818 2 .952 4 .645 2 .487 8	10.000 0							
		1 666 7	0.000	5.0000	4.000 0	3.333 3	2.857 1	2.5000	2.222 2
		-	1.5384	1.4286	1.3333	1.2500	1.1764	1.1111	1.0526
		0 606:	9 698.	.833 3	0 008:	769 2	.7408	.7142	9 689.
_ _	_ _	.625 0	0 909.	.5882	.571 4	.555 6	.540 5	.5264	.5128
_	<u> </u>	.4762	.465 2	.454 6	4444	.4348	.425 6	.4167	.4082
		.3846	.3774	.3704	.363 6	.357 2	.3508	.3448	.339 0
	_	.322 6	.317.5	.3125	.307 7	.303 0	.298 5	.2942	289 9
	_	.2778	.274 0	.2703	.266 7	.263 2	.259 7	.2564	.2532
		.2439	.241 0	.238 1	.235 3	.2326	.229	.227 3	.224 7
	_	.217 4	.2151	.2128	2105	.208 4	2002	.2041	.202 0
_	!-	.1961	.1942	.1923	.1905	.1887	.1869	.1852	.1834
		.178 6	.1770	.1754	.1739	.1724	1709	.169 5	.1681
		.1639	.1626	.1613	.1600	.1587	.1575	.1563	.1550
		.151 5	.1504	.1493	.1481	.147 1	.1460	.1449	.1439
		.1408	.1399	.1389	.1379	.137 0	.1361	.1351	.1342
 -	_	.1316	.1307	1299	129 0	.1282	.127 4	.1266	.1258
		.123 5	.122 7	.1220	.121 2	.1205	.1198	1190	.1183
		.1163	.1156	.1149	.1143	.1136	.1130	.1124	.1117
		1097	.1093	.1086	.1081	.107 5	.1070	.1064	.1058
		.1042	103 6	.103 1	1026	.1020	.1016	.1010	.100 5

LELES SHOWING BESISTANCE OF VARIOUS SIZES OF WIRES (B. & S. GAUGE) AT DIFFERENT LENGTHS AT 70° F.

RESISTANCE OF NO. 0000 COPPER WIRE.

0 .000 498 .000 996 .001 494 .001 992 .002 988 200 .004 980 .010 458 .010 956 .011 454 .011 952 .007 470 .007 968 200 .009 960 .010 458 .010 956 .011 454 .011 952 .012 450 .012 948 300 .019 920 .020 418 .020 916 .021 414 .021 912 .027 410 .027 908 500 .024 900 .025 338 .025 896 .026 394 .026 892 .027 410 .022 908 600 .024 900 .025 398 .025 896 .036 854 .038 856 .032 837 .032 889 .037 888 600 .034 860 .040 836 .041 334 .041 832 .042 839 .042 828 900 .044 820 .050 796 .051 294 .051 792 .057 788 1 000 .044 820 .050 298 .050 796 .051 792 .057 798 1 000 .044 820 .050 298 .050 796 .051 792 .052 790 .052 788	0000 0000 0000 0000 0000 0000 0000 0000 0000						.003 486 .008 466 .013 446 .018 426	.003 984	.004 482
.004 980 .005 478 .005 976 .006 474 .006 972 .007 470 .007 .009 960 .010 458 .010 956 .011 454 .011 952 .012 450 .012 410 .022 410 .032 510 .032 510 .042 510 .042 510 .042 510 .042 5	0.0000000000000000000000000000000000000								- 7
.009 960 .010 458 .010 956 .011 454 .011 952 .012 450 .012 .014 940 .015 438 .015 936 .016 434 .016 932 .017 430 .017 .019 920 .020 418 .020 916 .021 414 .021 912 .022 410 .022 .029 880 .025 398 .025 896 .026 892 .027 390 .027 .039 880 .030 876 .030 874 .031 872 .037 370 .037 .039 880 .040 836 .041 834 .041 832 .047 330 .042 .044 820 .045 318 .045 316 .046 314 .046 812 .047 310 .047 .049 800 .050 298 .050 796 .051 792 .051 792 .052 290 .052 .049 800 .055 278 .056 776 .056 772 .057 770 .057 .067 730 .052 .054 780 .051 289 .051 284 .051 284 .051 284 .051 280 .052 .052 .052 .052 .052 .052 .052	010. 020. 020. 030. 030. 040. 040.								
.014 940 .015 438 .015 936 .016 434 .016 932 .017 430 .017 .019 920 .020 418 .020 916 .021 414 .021 912 .022 410 .022 .024 900 .025 398 .026 394 .026 892 .027 390 .027 .029 880 .030 378 .035 856 .036 852 .037 330 .037 .039 880 .040 886 .045 318 .041 832 .042 330 .042 .044 820 .045 318 .045 316 .046 314 .046 812 .042 330 .042 .049 800 .050 298 .050 796 .051 794 .051 792 .052 290 .047 .054 780 .055 278 .056 776 .056 274 .056 772 .057 270 .057 .054 740 .065 278 .066 274 .066 720 .067 284 .067 284 .067 280 .067 280 .067 280 .059 760 .070 781 .070 716 .071 712 .071 712 .072 210 .072 .059 770 .077 806 .077 806 <	020 020 030 030 040 040								7
.019 920 .020 418 .020 916 .021 414 .021 912 .022 410 .022 .024 900 .025 398 .025 886 .026 892 .027 390 .042 390 .042 390 .042 390 .042 390 .042 390 .042 390 .042 390 .042 390 .042 390 .047 310 .047 310 .047 310 .047 310 .047 310 .047 310 .047 310 .047 310 .047 310 .047 310 .047 310 .047 310 .047 310 .052 250 .052 250 .052 250 .052 250 .052 250 .052 250 .052 250 .052 250 .052 250 .052 250 .052 250 .052 250 .052 2	020 035 035 040 040 040								•
.024 900 .025 398 .026 896 .026 892 .027 390 .027 390 .029 880 .030 378 .030 876 .031 374 .031 872 .032 370 .032 .039 880 .035 358 .035 856 .036 854 .036 852 .037 350 .037 .039 840 .040 338 .040 836 .041 834 .041 832 .042 330 .042 .044 820 .045 318 .045 816 .046 812 .047 310 .047 .047 .049 800 .050 278 .050 796 .051 274 .051 279 .052 270 .057 270 <t< th=""><th>.035 .035 .040 .045</th><th></th><th></th><th></th><th></th><th>1</th><th></th><th></th><th>•</th></t<>	.035 .035 .040 .045					1			•
.029 880 .030 378 .030 876 .031 374 .031 872 .032 370 .032 870 .034 860 .035 358 .035 856 .036 834 .036 852 .037 350 .047 310 .042 318 .042 818 .042 818 .042 318 .042 818 .0	08.9.9.9. 04.9.0.0.0.0.0.0.0.0.0.0.0.0.0.0.0.0.0.0						1 7 7		-
.034 860 .035 858 .035 856 .036 834 .036 852 .037 350 .037 .039 840 .040 338 .040 836 .041 334 .041 832 .042 330 .042 .044 820 .045 218 .045 816 .046 812 .047 310 .047 .049 800 .050 298 .050 776 .056 274 .051 792 .052 290 .050 .054 780 .055 278 .056 274 .056 772 .052 20 .052 .064 70 .060 258 .065 736 .066 234 .061 752 .062 250 .067 .069 720 .070 218 .070 716 .071 214 .071 712 .072 210 .072 .074 700 .077 198 .075 666 .076 194 .071 679 .072 210 .077 .079 680 .080 178 .080 676 .071 112 .071 119 .077 190 .077	.035 .040 .045 .050			:			.033366	033864	
.039 840 .040 838 .040 836 .041 832 .042 330 .062 330 .067 330 .067 330 .067 330 .067 330 .067 330 .067 330 .072 310 .072 310 .072 310 .072 310 .072 310 .072 310 .072 310 .072 310 .072 310 .072 310 .072 310 .072 310	3.3.				-				-
.044 820 .045 318 .045 816 .046 812 .046 812 .047 .047 .047 .049 800 .050 298 .050 796 .051 294 .051 792 .052 290 .052 .054 780 .055 278 .056 776 .056 274 .056 772 .057 270 .057 .054 740 .066 278 .066 234 .066 234 .067 230 .067 30 .067 30 .067 30 .067 30 .067 30 .067 30 .067 30 .067 30 .067 30 .067 30 .072 </th <th>540.</th> <th></th> <th>-</th> <th></th> <th></th> <th></th> <th></th> <th></th> <th></th>	540.		-						
049 800 0.50 298 0.50 796 0.51 294 0.51 792 0.52 290 0.55 278 0.54 780 0.65 278 0.66 274 0.66 272 0.67 270 0.6	050		_		: -				_
.054 780 .055 278 .056 274 .056 772 .057 270 .057 .059 760 .060 258 .060 756 .061 254 .061 752 .062 250 .062 .064 740 .065 238 .065 736 .066 234 .066 732 .067 230 .067 .069 720 .070 218 .070 716 .071 214 .071 712 .072 210 .072 .074 700 .075 198 .075 696 .076 114 .076 692 .077 190 .077 .079 680 .080 178 .080 676 .081 174 .081 672 .082 170 .082		1 -	1	Ι	1	1 -		.053 784	.054 282
.059 760 .060 258 .060 756 .061 254 .061 752 .062 250 .062 250 .062 250 .062 250 .062 250 .062 250 .065 238 .065 736 .066 732 .067 230 .067 230 .067 230 .067 230 .067 230 .067 230 .067 230 .067 230 .067 230 .067 230 .067 230 .067 230 .072 210	.055			-		_	.058266		Ξ.
.064 740 .065 238 .065 736 .066 234 .066 732 .067 230 .067 230 .069 720 .070 218 .070 716 .071 214 .071 712 .072 210 .072 210 .074 700 .075 198 .075 696 .076 194 .076 692 .077 190 .077 190 .079 680 .080 178 .080 676 .081 174 .081 672 .082 170 .082	990	_		٠.		Ξ.			٠.:
.069 720 .070 218 .070 716 .071 214 .071 712 .072 210 .072 20 .074 700 .075 198 .075 696 .076 194 .076 692 .077 190 .07	.065			-		-			Ξ.
777 700 074 700 075 198 075 696 0.076 194 0.076 692 0.082 170 089 0.082 170	020.	_	٠.			-		.073 704	• •
.079 680 .080 178 .080 676 .081 174 .081 672 .082 170 .082	075		1:-		11.	1.	.078 186	.078 684	.079 182
	080	_		Ξ.					_
.084 660 .085 158 .085 656 .086 154 .086 652 .087 150 .087	.080	_			1.			-	-
089 640 .090 138 .090 636 .091 134 .091 632 .092 130 .092	060	_		Ξ.					_
790. 011 790. 011 790. 011 10.	.095	_			: '				_

RESISTANCE OF NO. 000 COPPER WIRE.

Feet.	0	10	20	88	40	. 02	09	20	08	06
0	l	.000 628	.001 256	.001 884	1 -1	.003 140	.003 768	.004 396	.005 024	1
100	٠.	٠.				-	Ξ	_		- :
200					. =	_	•••			
300	.018 840	•	-	_						- 1.
400		• -		_	.027632		.028 888	-	_	.030772
200	١٠.	.032 028		1	-		.035 168	1.0		1
009		•••		_		=	٠.	~		
200					•		: -			
800	.050240	~	.051496	.052124	.052752	.053380		.054 636	.055 264	.055892
006		: '	-		.059 032	Ξ		_		
1 000	1 ==				.065 312	046 290.		11	1 .	.068 452
1 100	080 690.	804 690.	.070 336	.070 964	.071 592	1.	.072 848	.073 476	.074 104	.074732
1 200								_	_	
1 300	т.	-:								
1 400				_		_	_			
1 500	1	.094 828			.096 712	.097 340	896 260.		1 - 1	_
1 600		1 1			Ξ.					
1 700	.106760		010801	.108 644	.109272	.109 900	.110528	.111 156	.111 784	.112412
1800									_	
1 900		Ξ.								

RESISTANCE OF NO. 00 COPPER WIRE.

Feet.	0	10	20	30	40	26	09	20	08	8
0			1 .	1	1	1 -				1 ' '
100	٠.				_					_
200	•				-:	-				
300	• -								_	
400	.031 640	.032431	.033222	.034 013	.034 804	.035 595	036386	.037 177	.037 968	.038759
200		.040 341	.041 132	.041 923	.042 714	.043 505		.045 087	1	.046 669
909	•				_		$.052\ 206$	Ξ:	.053788	
200	•••			-		_	_	_	Ξ.	
908	• •			_					_	
006				-			.075 936		.077 518	.078309
1 000	4.		.080 682		.082 264	_	1	1 -	1.1	1 -
1 100	_				_					
1 200		.095 711	.096 502	.097 293	.098 084	.098 875	999 660.	.100457	.101 248	.102039
1 300			- 1.				-		·_ ·	-
1 400	• -	.111531				.114 695	.115 486	.116 277	_	
1 500	.118 650		1 -	1 -		1	1	.124 187		-
1 600				-:	_					
1 700	.134 470	$.135\ 261$.136052	.136 843	.137634	.138425	.139216	.140 007	.140 798	.141589
1800	• •						: '			
1900	• •				.153454	.154 245	.155036			

RESISTANCE OF NO. 0 COPPER WIRE.

Feet.	0	10	8	30	40	26	8	22	8	06
0		1 =	1	1	1 7.	1			1.	1
100	-	.010 978	011976	.012 974	013972	.014 970		•••		.018962
200	-	Ξ	_					•		•
300	٠.	=	- 1					•••		
400	.039 920	=			.043912	•	.045 908	.046 906	.047 904	.048902
200	1 =	_	1		1			1	1	
009		_								
902		-	٠.							
908	.079 840	.080 838	081836	.082834		.084 830		.086 826	.087824	088822
<u>6</u>		818000.		.092814	.093812		.095 808	908 960.		098802
1 000	1	.100 798	1 .	1 -	.103 792	.104 790	.105 788	.106 786	17	.108 782
1 100	٠.			_	7.		_	• -	7	• -
1 200	_			_	7.		_	•	7	• -
1 300	•			_			_	-		• -
1 400	.139720	.140 718	.141 716	.142 714	.143 712	.144 710	.145 708	.146 706	.147 704	• -
1 500	.149 700	1 =	1.	1	1 -	1	1 1	.156 686	1.	
1 600	_	_	Ξ.		-	٠				
1 700	_	_	Ξ.				-			
1800	.179640	.180638	.181636	.182634	.183632	.184630	.185628	.186626	.187624	.188622
1 900	Ξ	_	_				_			

RESISTANCE OF NO. 1 COPPER WIRE.

Feet.	0	10	82	8	40	20	99	70	8	6 6
0		1 7 3	1		1.7	1			1 -	1
100			· _				_	•		•
200					_	٠.	4 -	•		
900	.037 770	039029							.047 842	.049 101
400	.050 360	051619	.052878	.054 137	.055 396	.056655	.057 914	.059 173	.060432	
200	1			17.	-	1 .	I -	.071 763	.073 022	.074 281
909									.085 612	.086871
92		_						•-		_
8	_			Ξ.					_	
<u>0</u> 6			.115 828	.117 087	.118 346	.119605	.120 864	.122 123		
1 000	.125 900	.127 159	.128 418	.129 677	.130 936		1	.134 713	-	.137 231
1 100	.1	`_`	.141 008				.146 044		.148 562	.149821
1 200	т.									
1 300						_		•		_
1 400			-	_		.182555	.183 814	.185 073	.186332	
1 500	.188 850	1'-'		.192 627	1	11.1	1 -	.197 663	198 922	.200 181
1 600	.201 440	202 699	203958	.205217	.206476	.207 735	208 994	210253	.211512	.212771
1 700	_	• •	-							
1 800	_	•	_							
1 900		7							_	_

RESISTANCE OF NO. 2 COPPER WIRE.

Feet.	0	10	8	8	40	20	9	20	8	06
0		1	I	1	1	1.	.009 522			
100		. "	_	_	Ξ:					٠
200	-	.033327	.034 914	.036 501	.038 088	.039 675	.041262	.042 849	.044 436	.046023
300	_		_					-		~
400	.063 480	_		.068 241		٠.				.077763
200		1 -	1		_					_
009	٠.									
200	_	_			. •				7	
800	.126960	.128 547	_					_	_	
		.144 417	.146 004	.147 591	.149 178	.150765	.152352	.153939	.155526	.157113
1 000	1 -	-	.161 874	1 7	.165 048	.166 635		.169 809	.171 396	.172 983
1 100	.174570	.176157	.177 744	.179331	.180918	.182 505	.184 092	.185 679		
1 200	•	_								
1300				_				4	_	
1 400		-						٠.		•
1 500	.238 050	_	1	1	1	1	1.	I '	-	1 1 1
1 600	.253920	.255 507	.257 094	.258 681	.260 268	.261 855	.263 442	.265 029	.266 616	268203
1 700	_		-				_			-
1 800				•	_			_		_
1 900		·		.306 291	.307 878			_	٠.	-

RESISTANCE OF NO. 3 COPPER WIRE.

Feet.	0	10,	8	8	40	20	8	20	8	8
0		1	1 -	1 -	1 -	1 -	1	1		
100	Ξ		~	_		_				
200	.040 000	0.042000	.044 000	.046 000		.050 000	.052000	.054 000	.056 000	00080
300	Ξ		~	_		_		Ξ.		
400	000 080.	.082 000	.084 000	_	000 880.	_	.092 000	.094 000		
200	_	_	_	.106 000	.108 000		_	.114 000		.118 000
009	00000	_	_	_			_			
200	_	_	_	_			_			
908	_	_	_	_			_	Ξ.		
06	.180 000	000 281	.184 000	.186000		.190 000	000 261	Ξ.	000961	.198000
1 000	_		204 000	.206 000	.208 000	.210 000	.212 000	.214 000		
1 100	220000	.222 000		226000	-		.232000			.238000
1 200	=			_			_			
1300	=			_			_			
1 400	_	282000	.284 000	_	.288 000	.290 000	_		.296 000	298000
1 500	300 000	1	.304 000	306 000	308 000	.310 000	_	.314 000		
1 600	.320 000	322000	.324000	.326000	.328 000	.330 000	.332 000	.334 000	.336 000	.338 000
1 700			_	_			_			
1 800			_	_			_			
1900		_	_	_			_			

RESISTANCE OF NO. 4 COPPER WIRE.

Feet.	0	10	50	90	40	22	8	92	8	06
0		1	_	1.		1	1			1 -
8							_			
8	_		-						_	
900					-		_			
400	.100 960	.103 484		.108532	.111056	.113580	.116 104	.118 628	.121 152	.123 676
200	.126 200		.131 248	.133 772	1					1
8	٠.			_		Ξ.				
20 20		_				_				
- 008	٠.			_						
006		_				_	•-		.247 352	.249 876
000	.252 400		1.	.259 972	.262 496	_	' . "	1 =	٠	1 .
100		_			7	Ξ.				
200				_	7.			_		-
300	-	_				_				
1400	.353 360	.355 884	.358 408	.360 932	-	.365 980	.368 504	.371 028	.373 552	376 076
200	.378 600	1 .	.383 648	.386 172	388 696	.391 220		.396 268	.398 792	1
				٠.				٠.		
202	Ξ	+431604	.434 128			.441 700	.444 224		.449 272	.451 796
 908 1					-					
 06_	_		_		_	-		į.	_	-

RESISTANCE OF NO. 5 COPPER WIRE.

Feet.	0	10	8	8	40	22	8	20	8	8
0			1		1 -			1 11		
100		. =								
200			_							
900	.1	.098 673		.105 039	.108222			.117 771	.120954	
400	.127 320	.130503	.133686		.140052	.143235	.146418	.149 601	-	.155967
200	.159 150		1		1	.175 065	.178 248	٠.		
909	086061	.194 163	.197346	.200 529	_	.206 895		٠.	.216 444	
200			_					_		
8	_		т.					-		
006	•	.289 653	.292836		299 202		.305 568	.308 751		
1 000			1	1.	1 -			1 _		
1 100	.350 130	.353 313		.359679			.369 228	- 1	.375 594	.378 777
1 200	••									
1 300	• -		_							
1 400	_		.451 986	.455 169	.458352	.461 535	.464 718	.467 901	.471 084	.474 267
1 500	1.4			.486 999		1		.499 731	.502 914	
1 600	.509 280	.512463	.515 646	.518829	.522012	$.525\ 195$.528 378	.531561	.534 744	.537 927
1 700	٠:			.550 659		_		: :		
1800				.582 489						
1 900				.614319		_				

RESISTANCE OF NO. 6 COPPER WIRE.

Feet.	•	10	8	90	6	ಜ	99	70	8	8
0		ı	1 -	_	1.5			1		
901		٠								
8	-			••						- 2
8			- 1	•						
400	.160560	.164 574	.168 588	.172602	.176 616	.180 630	.184 644	.188 658	.192 672	.196686
200	200 700	1	1	17.	1	_	I	1	1	۔۔ ا
8	=					_				
200	.280 980	.284 994	289 008	.293 022	.297 036	.301050	.305 064	.309 078	.313092	.317106
008	٠:	:-:	_					-		
2 6	-:		_		.377 316			-		
1 000	1.	1.1			1 -	Ι.	-	1 2		.437 526
1 100	.441 540		.449 568	.453 582			_	=	.473 652	.477666
1 200	_				-		_	_		
1300	=						_	_		-
1400	.561 960	.565 974	.569 988	.574 002	.578 016	.582030	.586 044	.590 058	.594 072	-
1500	.602 100	.606 114	.610 128	1	.618 156	.622 170	.626 184	.630 198	.634 212	
1 600	.642 240			.654 282				.670 338	.674352	
1 700				•				-		
1800	_			_						
1 900	_	_	.770 688	.774 702	.778 716	.782 730	.786 744	-		.798 786

RESISTANCE OF NO. 7 COPPER WIRE.

	0	2	8	8	40	26	8	0,	8	06
>		1 -	1 ' '	1 ' '			1 -	1 4	1 2	.045 549
100	=	_		_		-	_		_	
500			•••	•						
300			.161 952	.167013	.172 074		.182 196	.187 257	.192318	.197379
400	.202 440	.207 501	212 562	.217 623	.222 684	.227 745				
200		1 ' '						1 . 1	_	
009		-					_			Ξ.
200	.354 270						.384 636	389 697	.394 758	.399819
800		•						_		
006		.460551	.465 612	.470 673	475 734	.480 795	.485 856	_		Τ.
1000	1 -			1 .		1 -	1 -	1-0	1 -	-
1 100	.556 710						.587 076	.592137	.597 198	.602259
1 200				_ :			_	1.		
1 300										-
.1400	.708 540	.713 601	.718662	.723 723	.728 784	.733 845	.738 906		=	
1500	-			1		1 7	1 -	1	I -	_
1 600	092 608.	.814 821	.819 882	.824 943	.830 004	.835 065	.840 126	.845 187	.850 248	.855309
1 700	_		-			_			_	_
1 800	_						-	-1	٠.	-
1 900			_				-			

RESISTANCE OF NO. 8 COPPER WIRE.

									-	
Feet.	0	10	8	8	40	£	8	2		8
0			1				1			.057 43
100										.12125
200			_			_				.18507
300	-				.216 98		_			.248 89
400	.255 28	.261 66	.268 04	.274 42	.280 80	.287 19	.293 57	299 95	.306 33	31271
200	.319 10		Ι.				۱.		.370 15	.376 53
009		.389 30			.408 44	.414 83	.421 21			.440 35
200			_				_			.504 17
- 008 6								_		.567 99
000	.574 38	.580 76	.587 14	.593 52	.599 90		.612 67	.619 05	.625 43	.631 81
1 000			_	1.	1					
1 100	.702 02	.708 40	.714 78		.727 54	.733 93	.740 31	.746 69	.753 07	.75945
1 200										
1 300										
1 400				.912 62	_					
1 500			1	٠		_		1.		1.014 73
1 600	1.021 12	1.027 50	1.03388	1.04026	1.046 64	1.05303	•	1.06579	1.07217	1.07855
1 700		٠.			_			_	-	1.14237
1 800						_			_	1.20619
1 900		-					1.25087	1.25725		1.27001

RESISTANCE OF NO. 9 COPPER WIRE.

Feet.	0	10	20	30	40	20	8	02	፟፠.	96
0		_				-	1		1	
100	_	-				_				
200	_			_			_			
300	.241 38	249 42		.265 51	.273 56	.281 61	.289 65	.297 70	.305 74	
400	.321 84	.329 88	.337 93	-	.354 02	362 07	_	.378 16		.394 25
200		.410				1	_			
98	.482 76	.490 80	.498 85	.506 89	.514 94	.522 99	.53103	.539 08	.547 12	.555 17
200		.571	_						-	
908		.651	_							
006		.732	_				••			.796 55
1 000	.804 60	.812	! -	1 -	.836.78	1	.852 87	l _		1 -
1 100	.885 06	.893		-		_	.933 33			-
1 200	.965 52	.973 56	1981 61	.989 65	02 266.	1.00575	1.01379	1.021 84	1.02988	1.03793
1 300	1.045 98	1.054	•	_			1.09425			
1 400	1.12644	1.134	1.14253	_			1.174 71			
1 500	1.206 90	1.214	!	١.	1.239 08	1	1.255 17		1.271 26	
1 600	1.287 36	1.295			1.31954		1.33563			
1 700	1.36782	1.375			1.400 00	_	141609			
1800	1.44828		1.46437	1.47241	1.48046	1.48851	1.49655	1.504 60		1.52069
1 900	1.528 74	1.536		••	1.56092		1.57701			

RESISTANCE OF NO. 10 COPPER WIRE.

Feet.	0	10	8	8	94	26	8	92	8	8
0		.010 15		۱ ـ		I -	1 -			
100		.111 65							Ξ.	
200		.213 15	- 3							
300	.304 50	.314 65							.385 70	
400	.406 00	.41615	.426 30	.436 45	.446 60	456 75	.466 90	.477 05	.487 20	.49735
500			1				1 .1		1	
909	_					_	_	_		
200							٠.		Ξ.	
908	.812 00	.822 15	.832 30	.842 45	.852 60	.862 75	.872 90	.883 05	.893 20	.90335
<u>0</u> 6	- 1				.954 10		.974 40	.984 55		
1 000	1.015 00		1.2		1	1			1	
1 100	1.11650	1.12665	1.13680			1.16725			7	1.20785
1 200	1.21800		: -					_		
1 300	1.31950				_			_		
1 400	1.42100			1,451 45	1.46160	1.471 75	1.48190	1.49205	1.50220	1.51235
1 500	1.52250	1.532 65	1				1.583 40		1.603 70	1.61385
1 600		1.63415	1.644 30	1.654 45	1.66460	1.674 75	1.68490	1.69505		1.71535
1 700										1.81685
1800										1.91835
1900										2.01985

RESISTANCE OF NO. 11 COPPER WIRE.

-	67	ಣ	4	z,	9	2	œ	6
					1 -		1	
				_	-		_	
					.046 04	.047 32	.048 60	.049 88
	.053 71	.054 99	.056 27	.057 55				.062 67
					ı –			
					٦.			
					- 1			
					Ξ.	.111 27	.112 55	.11383
88		118 94	12022	.121 50	.122 78	.124 06		
	.130 45	.131 73	.133 01		1	.136 85	.138 13	.13941
				.185 45	.186 73	.188 01	.189 29	
15		195 68	.196 96			200 80	.202 08	.203 36
			_			-		
	232		.235 33	.236 61	.237 89			
	245				_			

RESISTANCE OF NO. 12 COPPER WIRE.

Feet.	•	-	6	8	4		9	1	o o	æ
0			1	1			1 =	1 .		.014 52
10		.017 75	01936	.020	02259	.024 21	.02582	.027 43	.029 05	.030 66
20	.032 28						Τ.			.04680
80			_				-	_		.062 94
40	.064 56		_	.069 40						80 640.
33	_			1 -			-	1 -		1
8	.096 84	.098 45	.100 06		103 29	.104 91	.10652	.108 13	.109 75	.11136
20										-
8	٠									
8			.148 48	.150 10						.15978
100	1 .		.164 62	.166 24		1 -	.171 08			
110		.179 15	.180 76		.183 99	.185 61	.187 22		.19045	
120										
130										
140		.227 57						.237 25	.238 87	.240 48
150	.242 10	.243 71	1	i		1 -				.256 62
160			-			_		_		
170				_						
180		.292 13	.293 74	.295 36	296 97	.298 59	.300 20	.301 81	.303 43	
190	-									

RESISTANCE OF NO. 13 COPPER WIRE.

Feet.	0	-	7	ಣ	4	2	9	7	o c	6
<u> </u>		1				1 -				
	_	.022 38	.024 42	02645	.028 49	.03052	03256		.036 63	03866
	.040 70	Ξ.				_			-	
	_									
	.081 40	.083 43		.087 50		.091 57	.093 61	.095 64		12 660.
<u>' </u>						1 .				.120 06
	12210	.124 13	.12617	.12820	.13024	.13227	.134 31	.13634	.138 38	.14041
										.16076
				•-						.181 11
				-,			.19536	.197 39	.199 43	.20146
1		1 .	.207 57	_				217 74		.221 81
				•••						
	.244 20	.246 23	.248 27	.25030	.25234	.254 37	.256 41	.258 44	.260 48	.26251
			- 1	_						
	•		٠.	_						
1	1	1.		1		1			1 .	
	_			_						
	.345 95	.347 98	.350 02	.35205	.354 09	.35612	.35816	.360 19	.362 23	.364 26
	-			7.						

RESISTANCE OF NO. 14 COPPER WIRE.

Feet.	0	-	63	8	4	ıc	9	7	•	G
0								1.		.023 10
10								- 1		.048 77
20	.05134	.053 90	.056 47	.059 04	.061 60	.064 17	.066 74	.06930	.071 87	.074 44
30										.100 11
40								_		.125 78
20							.143 75			
99							.169 42	-		
2	.179 69	$.182\ 25$.18482	.187 39	.189 95	19252	.195 09	.197 65	.200 22	202.79
08							.220 76			
8		.233 59				.243 86	.246 43	.248 99	.251 56	
100				1			.272 10	I	1 .	
110	.282 37	.284 93	.287 50	.290 07	.29263	.295 20	.297 77	.300 33	.302 90	.30547
120									_	
130								т.		
140			-						-	
150	.385 05	.387 61	390 18	.392 75			400 45			.408 15
160	.410 72									.433 82
170	.436 39		-							.45949
180	.462 06	.464 62			.472 32	.474 89	.477 46	.480 02	.482 59	.485 16
190	.487 73									.51083

RESISTANCE OF NO. 15 COPPER WIRE.

Feet.	0	-	81	es	~	ro.	9	-	∞	6
0							.019 41			
2							.051 76			
28							.084			
<u>چ</u>							.11646			
9	.129 40	.132 63	.135 87	.139 10	.14234	.145 57	.148 81	.152 04	.155 28	.15851
25				.171 45	174 69		.181 16	.18439	.187 63	
8						.210 27	.213 51	.21674		
28		_				242 62	.245 86	.249 09		
2 2						.274 97	.278 21	.281 44		
8	291 15	294 38	297 62			.307 32	.310 56	.313 79	.317 03	
8								.34614	.349 38	
100								.378 49		
120						404 37		41084		
130								.443 19		
140	.452 90	.45613	.459 37	.462 60	.465 84	469 07	.472 31	475 54	.478 78	.482 01
150					498 19		.504 66		.51113	.51436
160						_				
170	_			_						
180	58230	585 53	.588 77	.592 00	.595 24	.598 47	.601 71	46 409.	.608 18	
6										

RESISTANCE OF NO. 16 COPPER WIRE.

Feet.	0	1	61	es	4	r.	9	7	œ	o
0			l		1 7 7	1 -	1 7.			
10	_									
8			_					_		
8			_		-	- : :		_		
9	.163 20	.167 28	.171 36	.175 44	.179 52	.183 60	.187 68	.191 76	.195 84	.199 92
20	.204 00	_		.216 24	_		1		1	-
8							_		-	
25		_		.297 84	.301 92		_	.314 16	.318 24	.322 32
8		-			•-		_		_	
8	.367 20	.371 28	.375 36			.387 60	.391 68	.395 76		.40392
100	408 00	1	1	_						1
110		.452 88	.456 96	.461 04	.465 12			.477 36	.481 44	.485 52
120						_				_
130						-				
140	.57120	.575 28	.579 36	.583 44	.587 52	.591 60	.595 68	.599 76	:::	.607 92
150	.612 00	1 -	_	1 .:			1 . 1	-	I	
160			_		_					
170	.693 60	.697 68	.701 76	.705 84	.709 92	.714 00	.718 08	.722 16	.726 24	.73032
180					_			Ξ.	_	.771 12
190		-			- 1					

RESISTANCE OF NO. 17 COPPER WIRE.

0 10 10 10 20 102 88 30 1154 32 40 205 76 50 306 64 70 360 08	.005 14 .056 58 .108 02 .159 46 .210 90 .262 34 .313 78 .365 22 .416 66	.010 28 .061 72 .113 16 .164 60 .216 04 .267 48 .318 92 .370 36	.015 43 .066 87 .118 31 .169 75 .221 19 .272 63	.020 57 .072 01 .123 45	.025 72	.030 86			
.102 .154 .205 .308 .308									
.154 .205 .308 .308 .360							.138 88	.144 03	.149 17
.205. .308. .368.					_			•	
.308	l =			-					
308.				1 -		1	1		.303 49
.360				.32921	.334 36	.339 50	.344 64	.349 79	.35493
				_		_			
.411					_ `				
.462				-					
.514	_		1 =		1 -	1			
	.570 98	.576 12	.581 27	.586 41	.591 56	.596 70	.601 84	66 909.	.61213
.617			Ξ.						
899.		_		_	- 1	_			
.720		_		_					
.771	.776 74	1 .	1.		1 -	1	١.	ı	
		.833 32	.838 47	.843 61	.848 76	.853 90	.859 04	.864 19	.869 33
.874	_		_		_	_	_		-
.925	_							_	
.977		_							_

RESISTANCE OF NO. 18 COPPER WIRE.

0 .006 42 10 .064 25 .070 67 20 .128 50 .134 92 30 .192 75 .134 92 30 .257 05 .263 42 50 .321 25 .327 67 60 .385 50 .391 92 70 .449 75 .456 17 80 .514 00 .520 42 90 .578 25 .584 67 100 .642 50 .648 92 110 .706 75 .771 42 120 .771 60 .771 42 130 .835 25 .841 67	142 .012 (92 .141 17 .205 142 .269 (62 .384 (62 .388 17 .462 17 .462 17 .462	35	.025 70 .089 95 .154 20					
	67 117 42 67 17 17	.083 .147 .212 .276 .276 .404 .469						
.128 50 .134 .192 75 .199 .257 00 .263 .321 25 .327 .385 50 .391 .449 75 .456 .518 25 .524 .642 50 .648 .771 00 .777 .835 25 .841	92 17 42 67 17 42	. 147 . 212 . 212 . 276 . 340 . 404 . 469						
. 192 75 . 199 . 257 00 . 263 . 321 25 . 327 . 385 50 . 391 . 449 75 . 456 . 514 00 . 520 . 574 00 . 584 . 771 00 . 777 . 835 25 . 841	17 42 67 17 42	.340 .469 .469						
	45 67 17 42 42	.340 .404 .469			.231 30	.237 72		
321 25 385 50 349 75 349 75 3514 00 5714 00 5718 25 642 50 642 50 771 00 771	67 17 42	.340 404 469		289 12		.301 97	.308 40	.31482
.385 50 .391 .449 75 .456 .514 00 .520 .578 25 .584 .642 50 .648 .771 00 .777 .835 25 .841	92 71 72	469. 469.				1		
	17	.469				•		
.514 00 .520 .578 25 .584 .642 50 .648 .706 75 .713 .771 00 .777 .835 25 .841	45	664	.475 45	.481 87	.488 30	.494 72		
.578 25 .584 .642 50 .648 .706 75 .713 .771 00 .777 .835 25 .841		3						
.642 50648 .706 75713 .771 0077 .835 25841	29	.597					.629 65	
.706 75 .713 .771 00 .777 .835 25 .841	92		1	1	.681 05			.700 32
.771 00 .777 .835 25 .841		60 .726 02	.732 45	.738 87	.745 30	.751 72	.758 15	
.835 25 .841	42	62.						
	29	854	_					
.899 50	92	.918	-					
.963 75	17 .976	.983	I -			~	٠.	
1.028 00 1.034	42 1.040	85 1.047 27	1.05370	1.06012	1.06655	1.07297	1.07940	1.08582
1.092 25 1.098	67 1.105	1.111					~~	
1.156 50 1.162	92 1.169	1.175				- 1		
1.22075 1.227	17 1.233	1.240		•			^	

RESISTANCE OF NO. 19 COPPER WIRE.

Feet.	0		73	es	4	ıo	9	7	o o	6
						1 -				-
		_				_				•
26										
3 6				_						.319 02
39	.327 20	335 38	.343 56	.351 74	359 92	.368 10	.376 28	.384 46	392 64	
5				.433 54		449 90		.466 26		
3 8									.556 24	.564 42
2 6			_							
88	.736 20	.744 38	.752 56		.768 92					.809 82
18			.834 36		,	1	_			.891 62
120			91616			_				.97342
25			96 266				_			1.05522
130			1.079 76		-					1.13702
148	1.145 20		1.16156	1.16974	-	1.18610				1.21882
155	1 227 00	1.235 18	1.243 36		1.259 72	1	1.276 08	1.284 26	1.292 44	1.300 62
9			1.32516	1.33334		1.34970				138242
122										1.46422
26										1.54602
160					_	٠				1.62782

RESISTANCE OF NO. 20 COPPER WIRE.

Feet.	0	. 1	83	က	4	22	9	7	•	6
0				.030 93	.041 24		.06186			
10				·						
20										
စ္တ	.309 30	.319 61	.329 92	.340 23		.360 85	.37116	.381 47		
40	.412 40								.494 88	.505 19
20				.546 43					.597 98	
99	.618 60	.628 91	.639 22	.649 53	.659 84	.670 15	.680 46	22 069.	.701 08	
22							- 1		.804 18	
8			•	_					.907 28	
8									1.01038	
100				١.					1.113 48	1.123 79
110	1.13410	1.144 41	1.15472	1.16503	1.17534		1.19596		1.21658	
120									1.31968	
130	_								1.42278	
140					1.48464	1.49495		1.51557	1.52588	
150			1.567 12	1.577 43	1.587 74	1.59805	1.608 36	1.618 67	1.628 98	1 -
160	1.64960	1.65991	1.67022	1.68053						1.74239
170										
180										- 1
190				_						

WIRING CHART.

The resistance in any circuit may be determined either by the length and size of the conductor composing it, or by the current and fall of potential along the conductor. In the first case, the resistance is directly as the length and inversely as the cross-section. In the second, it is directly as the fall of potential and inversely as the current.

The consideration of these principles has led to a graphic method of determining the sizes of wire necessary to carry certain currents over any given distance when the fall of potential is known. To say that the resistance is directly as one quantity and inversely as another, determines that if these quantities be plotted along any pair of rectangular coördinates, then lines of equal resistance will be straight lines radiating from the origin of the coördinates, and if these two separate sets of quantities be plotted along the same coördinates, the lines of equal resistance will be common to both pairs.

The diagram shown has been plotted with falls of potential in volts and distances in feet along the vertical, and with currents in amperes and areas in circular mils along the horizontal. Resistance lines have also been drawn, which are common to both sets of quantities. If now we wish to determine the size of a wire necessary to carry a certain current at a known fall of potential over a given distance, we follow the line of the resistance determined by the current and fall of potential till it intersects the line corresponding to the given distance, and this point determines the area of the copper wire required.

If, as an instance, it is required to find the wire necessary to carry a current of eighty amperes over a circuit of sixteen hundred feet at a hundred volts, the allowable loss of potential being five per cent, we immediately see that the line of .0625 resistance is determined by a current of eighty amperes and five volts loss, and if now this line is followed till it intersects the horizontal line corresponding to 1600 feet, we find that a copper wire of 269,768 C. M. has the required cross-section.





The most available form of this diagram for every-day work is one where the resistance lines have been drawn to correspond to the loss of potential generally allowed, thus avoiding the confusion of a number of useless resistance lines. The resistance lines we have chosen are those corresponding to a fall of potential of either $2\frac{1}{2}$, 5, 10 or 15 volts.

CARRYING CAPACITY OF COPPER WIRES.

Very many tables and formulæ have been offered for evidence in determining the carrying capacity of copper wires for electrical currents, and since the original limit set by the London Board of Trade, 1,000 amperes per square inch, nearer and nearer approximations to what may be called a true figure have been arrived at through the experimental results of the various physicists whose attention has been turned to this problem.

For long lines in the air carrying moderate amounts of current the wire in which the loss of electromotive force is not excessive will ordinarily be of sufficient size as regards heating, but where the amounts of current to be carried become large, or where short lengths are to be run, the closest attention needs be paid to this particular.

It need not be urged that especial care be taken where lights are run over wires concealed in mouldings or under the plaster of a house.

Fortunately, the formulæ at present at the disposal of the electrician are so safe that a fire from an overheated wire in normal running has become entirely an unknown thing, and with the most ordinary care must be impossible.

We have selected the formulæ of Forbes and Kennelly in calculating the following tables, the former relating entirely to wires suspended out of doors in the free air, while the formulæ of Kennelly discuss the problem of interior insulated and concealed wiring, the rise of temperature being in all cases 18° F. It will be noticed that the carrying capacity of a wire is increased by its insulating coating—this is a phenomenon observed by all experimenting along this line, and is explained by the greater radiating surface offered by the insulation as well as by the increased radiating power of the dark surfaces.

CARRYING CAPACITY OF WIRES.

		For	BES.		K	ENNELY	· .		ıre
S.ze, B. & S. Gauge.	Circular Mils.	Bright.	Black.	Paneled Wire.	Bright Wire sus- pended in Room.	Black Copper suspended in Room.	Bright Copper sus- pended Out-doors.	Black Copper suspended Out-doors.	1000 Amperes per Square Inch.
	600 000	271.	374.	381.	288.	370.	706.	744.	471.
	550 000	254.	350.	357.	272.	349.	662.	698.	432.
	500 000	236.	326.	332.	255.	329.	618.	652.	393.
	450 000	218.	301.	307.	238.	303.	572.	602.	353.
	400 000	200.	276.	281.	220.	280.	524.	552.	314.
0000	350 000	181.	250.	254.	202.	255.	476.	500.	275.
	300 000	161.	222.	227.	183.	229.	425.	447.	236.
	250 000	141.	194.	198.	163.	203.	372.	391.	196.
	211 600	124.	171.	174.	146.	181.	329.	346.	166.
	167 805	104.	144.	146.	127.	155.	278.	292.	132.
00	133 079	88.	121.	123.	110.	133.	236.	247.	105.
0	105 584	74.	102.	103.	95.	114.	199.	209.	83.
1	83 694	63.	86.	88.	83.	98.	169.	177.	66.
2	66 373	52.	72.	73.	72.	85.	141.	148.	52.
3	52 633	44.	60.	61.	63.	73.	121.	127.	41.
· 4	41 742	37.	51.	52.	55.	63.	103.	108.	33.
5	33 102	30.8	43.	43.	48.	55.	88.	91.	26.
6	26 250	25.9	36.	36.	42.	47.	75.	78.	20.6
7	20 817	21.8	30.	31.	37.	41.	63.	66.	16.3
8	16 509	18.3	25.3	25.7	32.	36.	54.	56.	13.0
9	13 094	15 4	21.2	21.6	28.2	31.	46.	48.	10.3
10	10 381	12.9	17.8	18.2	24.9	27.2	40.	41.	8.2
11	8 234	10.9	15.0	15.3	21.9	23.8	34.	35.	6.5
12	6 530	9.1	12.6	12.8	19.3	20.8	29.	30.	5.1
13	5 178	7.7	10.6	10.8	17.0	18.3	25.	25.8	4.1
14	4 107	6.4	8.9	9.1	15.0	16.0	21.5	22.2	3.2
15	3 257	5.4	7.5	7.6	13.3	14.1	18.5	19.1	2.6
16	2 583	4.6	6.3	6.4	11.8	12.4	16.0	16.5	2.0
17	2 048	3.8	5.2	5.4	10.4	10.9	13.8	14.2	1.6
18	1 624	3.2	5.0	5.1	9.2	9.6	12.0	12.3	1.3
19 20	1 288 1 022	2.7 2.3	3.7 3.1	3.8	8.2 7.2	8.5 7.5	10.4 9.0	10.7 9.2	1.0

TABLE OF DIAMETER OF WIRES IN STRAND

REA IN	A									res.
275 000	250 000	225 000	200 000	175 000	150 000	125 000	100 000	75 000	50 000	of Wires.
TER OF	DIAME							!		Š
524.4		474.3	447.2	418.3	387.3	353.5	816.2	273.8	223.6	1
302.7		273.8	258.1	241.5	223.6	204.1	182.5	158.1	129.1	1 3 7
198.2		179.2	169.0	158.1	146.3	133.6	120.3	103.5	84.5	77
120.8 86.2	114.7 82.1	108.8 77.9	102.5 73.5	95.9 68.7	88.9 63.6	81.1 58.1	72.5 51.9	62.8 45.0	51.3 36.7	19 87
67.1	64.0	60.7	57.2	53.6	49.6	45.2	40.5	35.1	28.6	61
57.2	54.5	51.7	48.7	45.6	42.2	38.5	34.5	29.8	24.3	61 84 91
54.9	52.4	49.7 42.1	46.8	43. 8	40.6	87.0	33.1	28.7	23.4	91
46.5	44.3	42.1	39.6	37.1	34.3	81.5	28.0	24.3	19.9	127
45.4	43.3	41.1	38.7	36.2	33.5	30.6	27.3	23.7	19.3	133
40.3	38.4	36.4	34.4	32.1	29.7	27.1	24.3	21.0	17.2	169 217
85.5	3 3.9	32.2	30.4	28.3	26.2	24.0	21.4	18.5	15.1	217

reg.								A	REA IN
of Wires.	550 000	575 000	600 000	625 000	650 000	6 75 00 0	700 000	725 000	750 000
No.		•	· · ·	'		<u> </u>		DIAME	TER OF
1	741.6	758.2	774.6	790.5	806.2	821.5	836.6	851.4	866.0
1 3 7	428.1	437.8	447.2	456.4	465.4	474.3	483.1	491.4	500.0
7	280.3	286.6	292.7	298.8	304.7	310.5	316.3	321.8	327.3
19 37	170.1	173.9	177.6	181.3	184.9	188.4	191.9	195.3	198.6
37	121.9	124.6	127.3	129.9	132.5	135.0	137.5	139.9	142.3
61 84 91	94.9	97.1	99.1	101.2	103.2	105.1	107.1	109.0	110.8
84	80.9	82.7	84.5	86.2	87.9	89.6	91.2	92.9	94.4
91	77.7	79.4	81.2	82.8	84.5	86.1	87.7	89.2	90.7
127	65.8	67.2	68.7	70.1	71.5	72.9	74.2	75.5	76.8
133	64.2	65.7	67.1	68.5	69.9	71.2	72.5	73.8	75.0
169	57.1	58.3	59.5	60.8	62.0	63.1	64.3	65.4	66.6
217	50.3	51.4	52.5	53.6	54.7	55.7	56.7	57.8	58.8

EQUIVALENT TO GIVEN CIRCULAR MILAGES.

	AR MIL	8.							
300 000	325 00	350 00	375 00	0 400 00	0 425 00	450 00	475 000	500 000	525 000
Wires	IN MILE	3.		·	<u> </u>	· <u>·</u>			
547.7	7 570.	1 591.	612.	4 632.	4 651.9	670.	689.2	707.1	724.5
316.2	2 329.	1 341.	353.	5 365.	1 376.3	387. 1 253.	2 398.0	408.2	418. 273.
207.0	0 215.	5 223.		4 239.	0 246.	253.	260.5	267.2	273.
125.6		7 135.	140.		0 149.	158.	158.1	162.2	166.
90.0	93.	7 97.	100.	.6 103.	9 107.	110.	118.8	116.2	119.
70.1			78.	4 80.			88.2	90.5	
59.8								L 77.1	
57.4	4 59.		64.	1 66.		3 70.	72.2	74.1	
48.6	50.		54.			59.			
47.4	49.	4 51.:	2 53.	.0 54.	8 56.	58.	1 59.7	61.3	62.
42.1	1 43.	45.	47.	1 48.	6 50.1	51.	53.0	54.3	55.
37.1									
Стрепт	AR MIII								
	AR MILE 800 000		850 000	875 000	900 000	925 000	950 000	975 000	1 000 000
775 000	₁	825 000	850 000	875 000	900 000	925 000	950 000	975 000	1 000 000
775 000 WIRES	800 000 IN MILE 894.4	825 000	921.9	935.4	948.6	961.7	974.6	975 000	1 000.0
775 000 WIRES	800 000 IN MILE 894.4 516.3	825 000 3. 908.3 524.4	921.9 582.2	935.4 540.1	948.6 547.7	961.7 555.2	974.6 562.7	987.4 570.0	1 000.0
775 000 WIRES 880.3 508.2 332.7	800 000 IN MILE 894.4 516.3 838.0	825 000 3. 908.3 524.4 343.3	921.9 532.2 348.4	935.4 540.1 853.5	948.6 547.7 858.5	961.7 555.2 363.5	974.6 562.7 368.4	987.4 570.0 873.2	1 000.0 577.1 377.0
775 000 WIRES 880.3 508.2 332.7 201.9	894.4 516.3 838.0 205.0	825 000 3. 908.3 524.4 343.3 208.3	921.9 582.2 348.4 211.5	935.4 540.1 853.5 214.5	948.6 547.7 358.5 217.6	961.7 555.2 363.5 220.6	974.6 562.7 368.4 223.6	987.4 570.0 873.2 226.5	1 000.6 577.3 377.0 229.4
775 000 WIRES 880.3 508.2 332.7	800 000 IN MILE 894.4 516.3 838.0	825 000 3. 908.3 524.4 343.3	921.9 532.2 348.4	935.4 540.1 853.5	948.6 547.7 858.5	961.7 555.2 363.5	974.6 562.7 368.4	987.4 570.0 873.2	1 000.6 577.3 377.0 229.4
775 000 WIRES 880.3 508.2 332.7 201.9 144.7 112.7	800 000 IN MILE 894.4 516.3 838.0 205.0 147.0 114.5	825 000 3. 908.3 524.4 343.3 208.3 149.3	921.9 582.2 348.4 211.5 151.5	935.4 540.1 353.5 214.5 153.7	948.6 547.7 858.5 217.6 155.9	961.7 555.2 363.5 220.6 158.1	974.6 562.7 368.4 223.6 160.2	987.4 570.0 873.2 226.5 162.3	1 000.0 577.1 377.0 229.4 164.4
775 000 WIRES 880.3 508.2 332.7 201.9 144.7 112.7 96.0	894.4 516.3 838.0 205.0 147.0 114.5 97.5	825 000 3. 908.3 524.4 343.3 208.3 149.3 116.2 99.1	921.9 582.2 348.4 211.5 151.5 118.0 100.5	935.4 540.1 353.5 214.5 153.7 119.7 102.0	948.6 547.7 858.5 217.6 155.9 121.4 103.5	961.7 555.2 363.5 220.6 158.1 123.1 104.9	974.6 562.7 368.4 223.6 160.2 124.7 106.3	987.4 570.0 873.2 226.5 162.3 126.4 107.1	1 000.6 577.3 377.6 229.6 164.4
775 000 WIRES 880.3 508.2 332.7 201.9 144.7 112.7 96.0 92.2	800 000 IN MILE 894.4 516.3 838.0 205.0 147.0 114.5 97.5 93.7	825 000 3. 908.3 524.4 343.3 208.3 149.3 116.2 99.1 95.2	921.9 582.2 348.4 211.5 151.5 118.0 100.5 96.6	935.4 540.1 353.5 214.5 153.7 119.7 102.0 98.0	948.6 547.7 858.5 217.6 155.9 121.4 103.5 99.5	961.7 555.2 363.5 220.6 158.1 123.1 104.9 100.8	974.6 562.7 368.4 223.6 160.2 124.7 106.3 102.1	987.4 570.0 873.2 226.5 162.3 126.4 107.1 103.5	1 000.6 577.3 377.6 229.4 164.4 128.6 109.1
775 000 WIRES 880.3 508.2 332.7 201.9 144.7 112.7 96.0 92.2 78.1	800 000 IN MILE 894.4 516.3 338.0 205.0 147.0 114.5 97.5 93.7 79.3	825 000 3. 908.3 524.4 343.3 208.3 149.3 116.2 99.1 95.2 80.5	921.9 582.2 348.4 211.5 151.5 118.0 100.5 96.6 81.8	935.4 540.1 353.5 214.5 153.7 119.7 102.0 98.0 83.0	948.6 547.7 858.5 217.6 155.9 121.4 103.5 99.5 84.1	961.7 555.2 363.5 220.6 158.1 123.1 100.8 85.3	974.6 562.7 368.4 223.6 160.2 124.7 106.3 102.1 86.4	987.4 570.0 873.2 226.5 162.3 126.4 107.1 103.5 87.6	1 000.0 577.3 377.0 229.4 164.4 128.0 109.1 104.8 88.7
775 000 WIRES 880.3 508.2 332.7 201.9 144.7 112.7 96.0 92.2	800 000 IN MILE 894.4 516.3 838.0 205.0 147.0 114.5 97.5 93.7	825 000 3. 908.3 524.4 343.3 208.3 149.3 116.2 99.1 95.2	921.9 582.2 348.4 211.5 151.5 118.0 100.5 96.6	935.4 540.1 353.5 214.5 153.7 119.7 102.0 98.0	948.6 547.7 858.5 217.6 155.9 121.4 103.5 99.5	961.7 555.2 363.5 220.6 158.1 123.1 104.9 100.8	974.6 562.7 368.4 223.6 160.2 124.7 106.3 102.1	987.4 570.0 873.2 226.5 162.3 126.4 107.1 103.5	1 000.6 577.3 377.6 229.4 164.4 128.6 109.1
775 000 WIRES 880.3 508.2 332.7 201.9 144.7 112.7 96.0 92.2 78.1	800 000 IN MILE 894.4 516.3 338.0 205.0 147.0 114.5 97.5 93.7 79.3	825 000 3. 908.3 524.4 343.3 208.3 149.3 116.2 99.1 95.2 80.5	921.9 582.2 348.4 211.5 151.5 118.0 100.5 96.6 81.8	935.4 540.1 353.5 214.5 153.7 119.7 102.0 98.0 83.0 81.1	948.6 547.7 858.5 217.6 155.9 121.4 103.5 99.5 84.1	961.7 555.2 363.5 220.6 158.1 123.1 100.8 85.3	974.6 562.7 368.4 223.6 160.2 124.7 106.3 102.1 86.4	987.4 570.0 873.2 226.5 162.3 126.4 107.1 103.5 87.6	1 000.0 577.3 377.6 229.4 164.4 128.0 109.1 104.8 88.7

Note.—To find the size wire necessary to make a strand of given Circular Milage and of a given number of wires find from above table the diameter in mils of wire corresponding to size of strand and number of wires in strand. Then, by inspection of any table showing sizes in B. & S. Gauge, the desired gauge of wire can be found.

TABLE SHOWING DIAMETER IN MILS OF A GIVEN NUMBER OF WIRES LAID UP IN STRANDS.

2	181.9 105.0 68.7 41.7 29.9	25.9 19.9 15.7
4	204.3 117.9 77.2 46.9 33.6	29.2 26.1 22.3 21.4 17.7
က	229.4 132.4 86.7 52.6 37.7	25.8 25.0 24.0 19.9
5	257.6 148.7 97.3 59.1 42.3	36.8 32.9 28.1 27.0 22.3
1	289.3 167.0 109.3 66.3 47.5	41.3 37.0 30.3 25.0
0	324.9 187.5 122.8 74.5 53.4	46.4 41.6 85.4 34.0 28.2
8	364.8 210.6 137.9 83.7 59.9	52.1 46.7 39.8 38.2 31.6
000	409.6 236.5 154.8 93.9 67.3	58.5 52.4 42.9 35.5
0000	460. 265.6 173.9 105.5 75.6	65.7 58.9 50.2 39.9
0000	650.5 375.6 245.9 149.2 106.9	92.9 70.9 68.2 56.4
8 0000	796.7 460.0 801.1 182.7 131.0	113.8 102.0 86.9 83.5 69.0
4 0000	920.0 531.2 346.2 211.1 151.2	131.4 117.8 100.3 96.4 79.7
No. of Wires.	1 3 7 19 37	84 22 92 ESI

82	32. 18.4 12.1 7.3	
19	35.9 20.7 13.6 8.2	
18	40.3 15.2 9.2	
17	45.3 26.1 17.1 10.3	
16	50.8 29.3 11.7	
15	57.1 32.9 21.6 13.0	
14	64.1 37.0 14.7	
13	72. 27.2 16.5	
12	80.8 46.7 30.5 18.5	
11	90.7 52.4 34.3 20.8	
10	101.9 58.9 28.5	16.8 14.5 13.0 11.1 10.7 8.8
6	114.4 66.0 43.3 26.3	18.8 14.6 11.9 9.9
80	128.5 74.2 48.6 29.5	21.1 18.4 16.4 13.5 11.1
7	144.3 83.3 54.5 33.1	20.6 18.5 15.7 12.7
မှ	162.0 93.5 61.2 37.2	26.6 23.1 20.7 17.7 16.9 14.0
No. of wires.	19 19	8 6 2 2 2 E

TABLES OF LENGTHS AND STRAINS IN SPANS OF WIRE AND SUSPENSION CABLES.

The tables of lengths and strains in spans of wire and cables here given are calculated from the formulæ derived from the equation of a parabola, which is the curve assumed by a wire hanging between two points of suspension unloaded, except by its own weight.

Since telegraph poles are ordinarily spaced by the number per mile, and the distance on an electric railroad or city lighting plant are laid out by the foot, two tables are given based on the usage in the two different cases, which also has determined the selection of different proportionated deflections.

It has been found by observation that the practice with telegraph lines is to allow a deflection of about .005 of the span. though there is no rule set, and the actual amount depends upon the lineman and the appliances for tightening the line which are at his disposal; with the heavier soft copper wires the custom has been to allow two or three times this deflection. and in some of our cities the unsightliness of the overhead wires is largely due to lack of attention to the possibilities of uniformity and small deflection in the spans. The table of lengths gives the actual lengths of wire between the points of suspension required by each different amount of deflection. and the table of strains is one in which a factor is given by which the weight per foot of the suspended wire is to be multiplied in order to ascertain the total strain at the center of the span. The strain at the point of suspension is slightly greater, but the difference is negligable in comparison with the chafing and cutting effect of the tie wire by which the line is fastened to the insulators.

In the case of a weight suspended at the center of the span, as is the case with arc lamp and trolley wire suspenders, the general solution is too intricate for tabulation, and either half the weight may be added to the total tension, or the weight per foot be increased by a proportionate amount of the extra suspended weight, and the factor of safety be increased as with either method the result obtained will be somewhat too low.

TABLE OF TOTAL LENGTH OF WIRE CORRES

e.	i ii					PER CENT.
Poles to Mile.	Spans in Feet.	.004	.006	.008	.010	.015
20	264.0	264.011	264.025	264.045	264.070	264.158
21	251.4	251.410	251.424	251.442	251.466	251.550
22 23	240.0	240.010	240.023	240.040	240.063	240.144
23	229.5	229.509	229.522	229.539	229.561	229.637
24	220.0	220.009	220.021	220.037	220.058	220.132
25	211.2	211.209	211.202	211.236	211.256	211.326
26	203.0	203.008	203.019	203.034	203.053	203.121
27	195.5	195.508	195.518	195.533	195.552	195.617
28 29	188.5	188.508	188.518	188.532	188.550	188.613
29	182.0	182.007	182.017	182.031	182.048	182.109
30	176.0	176.007	176.016	176.030	176.046	176.105
31 32	170.3	170.307	170.316	170.329	170.345	170.402
32	165.0	165.007	165.015	165.028	165.043	165.099
33	160.0	160.006	160.015	160.027	160.042	160.096
34	155.3	155.306	155.314	155.326	155.341	155.393
35	150.8	150.806	150.814	150.825	150.840	150.890
36 37	146.6	146.606	146.614	146.625	146.638	146.687
37	142.7	142.706	142.713	142.724	142.737	142.785
38 39	138.9	138.905	138.913	138.923	138.937	138.983
39	135.4	135.405	135.412	135.423	135.436	135.481
40	132.0	132.005	132.012	132.022	132.035	132.079
41	128.8	128.805	128.812	128.821	128.834	128.877
42	125.7	125.705	125.712	125.721	125.733	125.775
43	122.8	122.805	122.811	122.820	122.832	122.873
44	120.0	120.005	120.011	120.020	120.031	120.072
45	117.3	117.305	117.311	117.320	117.331	117.370
46	114.7	114.704	114.711	114.719	114.730	114.768
47	112.3	112.304	112.310	112.319	112.329	112.367
48	110.0	110.004	110.010	110.018	110.029	110.066
49	107.7	107.704	107.710	107.718	107.728	107.764
50	105.6	105.604	105.610	105.618	105.628	105.663

PONDING TO A GIVEN PERCENTAGE DEFLECTION.

DEFLECTIONS.

.020	.025	.030	035،	.040	.045	.050
264.281	264.440	264.633	264.862	265.126	265.425	265.760
251.668	251.819	252.003	252.221	252.472	252.757	253.076
240.255	240.400	240.576	240.784	241.024	241.296	241.600
229.744	229.882	230.050	230.249	230.479	230.739	231.030
220.234	220.366	220.528	220.718	220.938	221.188	221.466
211.424	211.552	211.706	211.889	212.101	212.340	212,608
203.216	203.338	203.487	203.663	203.866	204.096	204.353
195.708	195.825	195.969	196.138	196.334	196.555	196.803
188.700	188.814	188.952	189.115	189.304	189.517	189.756
182.193	184.803	182.436	182.594	182.776	182.982	183.213
176.187	176,193	176,422	176.574	176,750	176.950	177,173
170.481	170.583	170.708	170.856	171.026	171.219	171.435
165.176	165.275	165.396	165.539	165.704	165.891	166.100
160.170	160.266	160.384	160.522	160.682	160.864	161.066
155.465	155.558	155.672	155.807	155.962	156.138	156.335
150.960	151.051	151.161	151.292	151.443	151.614	151.805
146.756	146.844	146.951	147.078	147.225	147.391	147.577
142.852	142.937	143.042	143.166	143.308	143.470	143.651
139.048	139.131	139.233	139.353	139.492	139.650	139.826
135.544	135.625	135.724	135.842	135.977	136.131	136.302
132.140	132,220	132,316	132,431	132,563	132.712	132,880
128.937	129.014	129.109	129.220	129.349	129.495	129.658
125.834	125.909	126.001	126.110	126.236	126.378	126.538
122.930	123.004	123.094	123.201	123.323	123.463	123.618
120.128	120.200	120.288	120.392	120.512	120.648	120.800
117.425	117.495	117.581	117.683	117.800	117.933	118.082
114.822	114.891	114.975	115.074	115.189	115.319	115.464
112.419	112.487	112.569	112.666	112.779	112.906	113.048
110.116	110.183	110.264	110.359	110.469	110.594	110.733
107.814	107.879	107.958	108.051	108.159	108.281	108.418
105.712	105.776	105.853	105.944	106.050	106.170	106.304

TABLE OF TOTAL LENGTH OF WIRE CORRES

t.						:	PER CENT.
Spans 1 Feet.	.010	.015	.020	.025	.030	.035	.040
10	10.002	10.006	10.010	10.016	10.024	10.032	10.042
20	20.005	20.012	20.021	20.033	20.048	20.065	20.085
30	30.008	30.018	30.032	30.050	30.072	30.098	30.128
40	40.010	40.024	40.042	40.066	40.096	40.130	40.170
60 70	50.013 60.016 70.018	50.030 60.036 70.042	50.053 60.064 70.074	50.083 60.100 70.116	50.120 60.144 70.168	50.163 60.196 70.228	50.213 60.256 70.298
80	80.021	80.048	80.085	80.133	80.192	80.261	80.341
90	90.024	90.054	90.096	90.150	90.216	90.294	90.384
100	100.026	100.060	100.106	100.166	100.240	100.326	100.426
110	110.029	110.066	110.117	110.183	110.264	110.359	110.469
120	120.032	120.072	120.128	120.200	120.288	120.392	120.512
130	130.034	130.078	130.138	130.216	130.312	130.424	130.554
140	140.037	140.084	140.149	140.233	140.336	140.457	140.597
150	150.040	150.090	150.160	150.250	150.360	150.490	150.640
160	160.042	160.096	160.170	160.266	160.384	160.522	160.682
170	170.045	170.102	170.181	170.283	170.408	170.555	170.725
180	180.048	180.108	180.192	180.300	180.432	180.588	180.768
190	190.050	190.114	190.202	190.316	190.456	190.620	190.810
200	200.053	200.120	200.213	200.333	200.480	200.653	200.853

s in						P	ER CENT.
Spans in Feet.	.085	.090	.095	.100	.110	.120	.130
10 20 30 40	10.192 20.385 30.578 40.770	10.216 20.432 30.648 40.864	10.240 20.481 30.722 40.962	10.266 20.533 30.800 41.066	10.322 20.645 30.968 41.290	10.384 20.768 31.152 41.536	10.450 20.901 31.352 41.802
50 60 70 80 90	50.963 61.156 71.348 81.541 91.734	51.080 61.296 71.512 81.728 91.944	51.203 61.444 71.684 81.925 92.166	51.333 61.600 71.866 82.133 92.400	51.613 61.936 72.258 82.581 92.904	51.920 62.304 72.688 83.072 93.456	52.253 62.704 73.154 83.605 94.056
100 110 120 130	101.926 112.119 122.312 132.504	102.160 112.376 122.592 132.808 143.024	102.406 112.647 122.888 133.128 143.369	102.666 112.933 123.200 133.466 143.733	103.226 113.549 123.872 134.194	103.840 114.224 124.608 134.992	104.506 114.957 125.408 135.858
140 150 160 170 180	142.697 152.890 163.082 173.275 183.468	163.456 173.672 183.888	153.610 163.850 174.091 184.332	164.266 174.533 184.800	144,517 154 840 165,162 175,485 185,803	145.376 155.760 166.144 176.528 186.912	146.309 156.760 167.210 177.661 188.112
190 200	193.660 203.853	194.104 204.320	194.572 204.813	195.066 205.333	196.130 206.453	197.296 207.680	198.562 209.013

PONDING TO A GIVEN PERCENTAGE DEFLECTION.

DEFLECTION.

.045	.050	.055	.060	.065	.070	.075	.080
10.054	10.066	10.080	10.096	10.112	10.130	10.150	10.170
20.108	20.133	20.161	20.192	20.225	20.261	20.300	20.341
30.162	30.200	30.242	30.288	30.338	30.392	30.450	30.512
40.216	40.266	40.322	40.384	40.450	40.522	40.600	40.682
50.270	50.333	50.403	50.4 80	50.563	50.653	50.750	50.853
60.324	60.400	60.484	60.576	60.676	60.784	60.900	61.024
70.378	70.466	70.564	70.672	70.788	70.914	71.050	71.194
80.432	80.533	80.645	80.768	80.901	81.045	81.200	81.365
90.486	90.600	90.726	90.864	91.014	91.176	91.350	91.536
100.540	100.666	100.806	100.960	101.126	101.306	101.500	101.706
110.594	110.733	110.887	111.056	111.239	111.437	111.650	111.877
120.648	120.800	120.968	121.152	121.352	121.568	121.800	122.048
130.702	130.866	131.048	131.248	131.464	131.698	131.950	132.218
140.756	140.933	141.129	141.344	141.577	141.829	142.100	142.389
150.810	151.000	151.210	151.44 0	151 690	151.960	152.250	152.560
160.864	161.066	161.290	161.536	161.802	162.090	162.400	162.730
170.918	171.133	171.371	171.632	171.915	172.221	172.550	172.901
180.972	181.200	181.452	181.728	182.028	182.352	182.700	183.072
191.026	191.266	191.532	191.824	192.140	192.482	192.850	193.242
201.080	201.333	201.613	201.920	202.253	202,613	203.000	203.413

DEFLECTION.

				1		
.140	.150	.160	.170	.180	.190	.200
10.522	10.600	10.682	10.770	10.864	10.962	11.066
21.045	21.200	21.365	21.541	21.728	21.925	22.133
31.568	31.800	32.048	32.312	32.592	32.888	33.200
42.090	42.400	42.730	43.082	43.456	43.850	44.266
52.613	53.000	53.413	53.853	54.320	54.813	55.333
63.136	63,600	64.096	64.624	65.184	65,776	66,400
73.658	74.200	74.778	75.394	76.048	76,738	77.466
84.181	84.800	85.461	86.165	86.912	87.701	88.533
94.704	95,400	96.144	96,936	97.776	98.664	99.600
105.226	106.000	106.826	107.706	108.640	109.626	110.666
115.749	116,600	117.509	118,477	119,504	120,589	121,733
126.272	127.200	128.192	129.248	130.368	131.552	132.800
136.794	137.800	138.874	140.018	141.232	142.514	143.866
147.317	148,400	149.557	150.789	152.096	153,477	154.933
157.840	159.000	160.240	161.560	162.960	164.440	166.000
168.362	169,600	170.922	172,330	173.824	175,402	177.066
178.885	180,200	181.605	183,101	184.688	186.365	188,133
189.408	190.800	192.288	193.872	195.552	197.328	199,200
199.930	201.400	202.970	204.642	206.416	208.290	210.166
210.453	212.000	213.653	215.413	217.280	219.253	221.333

TABLE OF ACTUAL DEFLECTIONS OF WIRE PERCENTAGE

	1	Γ				
ŝ						PER CENT.
Poles to Mile.	Length of Span in Feet.	.004	.006	.008	.010	.015
Pol	12.88				r	EFLECTIONS
20	264.0	1.05	1.58	2.11	2.64	3.96
21	251.4	1.01	1.51	2.01	2.51	3.77
22	240.0	0.96	1.44	1.92	2.40	3.60
23	229.5	0.92	1.38	1.84	2.29	3.44
24	220.0	0.88	1.32	1.76	2.20	3.30
25	211.2	0.85	1.27	1.69	2.11	3.17
26	203.0	0.81	1.22	1.62	2.03	3.04
27	195.5	0.78	1.17	1.56	1.95	2.93
28	188.5	0.75	1.13	1.50	1.88	2.83
29	182.0	0.73	1.09	1.45	1.82	2.73
30	176.0	0.70	1.05	1.41	1.76	2.64
31	170.3	0.68	1.02	1.36	1.70	2.55
32	165.0	0.66	0.99	1.32	1.65	2.47
33	160.0	0.64	0.96	1.28	1.60	2.40
34	155.3	0.62	0.93	1.24	1.55	2.33
35	150.8	0.60	0.90	1.21	1.51	2.26
36	146.6	0.59	0.88	1.17	1.47	2.20
37	142.7	0.57	0.86	1.14	1.43	2.14
38	138.9	0.55	0.83	1.11	1.39	2.08
39	135.4	0.54	0.81	1.08	1.35	2.03
40	132.0	0.53	0.79	1.05	1.32	1.98
41	128.8	0.52	0.77	1.03	1.29	1.93
42	125.7	0.50	0.75	1.01	1.26	1.88
43	122.8	0.49	0.74	0.98	1.23	1.84
44	120.0	0.48	0.72	0.96	1.20	1.80
45	117.3	0.47	0.70	0.94	1.17	1.76
46	114.7	0.46	0.69	0.92	1.15	1.72
47	112.3	0.45	0.67	0.90	1.13	1.68
48	110.0	0.44	0.66	0.88	1.10	1.65
49	107.7	0.43	0.65	0.86	1.08	1.62
50	105.6	0.42	0.63	0.84	1.06	1.58

IN FEET CORRESPONDING TO A GIVEN DEFLECTION.

EFLECTIO	ns.					
.020	.025	.030	.035	.040	.045	.050
N FEET.	· · · · · · · · · · · · · · · · · · ·	!		!		
5.28	6.60	7.92	9.24	10.56	11.88	18.20
5.03	6.29	7.54	8.80	10.05	11.31	12.57
4.80	6.00	7.20	8.40	9.60	10.80	12.00
4.59	5.74	6.88	8.03	9.18	10.33	11.47
4.40	5.50	6.60	7.70	8.80	9.90	11.00
4.22	5.28	6.33	7.39	8.44	9.50	10.56
4.06	5.08	6.09	7.10	8.12	9.14	10.16
3.91	4.89	5.86	6.84	7.82	8.80	9.77
3.77	4.71	5.65	6.60	7.54	8.48	9.42
3.64	4.55	5.46	6.37	7.28	8.19	9.10
3.52	4.40	5.28	6.16	7.04	7.92	8.81
3.41	4.26	5.11		6.81	7.66	8.51
3.30	4.12	4.95	5.96 5.77	6.60	7.42	8.25
3.20	4.00	4.80	5.60	6.40	7.20	8.00
3.11	3.88	4.66	5.44	6.21	6.99	7.76
3.02	3.72	4.52	5.28	6.03	6.79	7.54
2.92	3.66	4.39	5.13	5.86	6.60	7.33
2.85	3.57	4.28	4.99	5.70	6.42	7.13
2.77	3.47	4.16	4.86	5.55	6.25	6.94 6.77
2.71	3.38	4.06	4.74	5.41	6.09	6.77
2.64	3.30	3.96	4.62	5.28	5.94	6.60
2.57	3.22	3.86	4.51	5.15	5.80	6.44
2.51	3.14	3.77	4.40	5.02	5.66	6.28
2.45	3.07	3.68	4.30	4.91	5.53	6.14
2.40	3.00	3.60	4.20	4.80	5.40	6.00
2.34	2.93	3.52	4.11	4.69	5.28	5.86
2.29	2.87	3.44	4.01	4.58	5.16	5.73
2.25	2.81	3.38	3.94	4.49	5.05	5.61
2.20	2.75	3.30	3.85	4.40	4.95	5.50
2.15	2.69	3.23	3.77	4.30	4.85	5.38
2.11	2.64	3.16	3.70	4.22	4.75	5.28

TABLE OF ACTUAL DEFLECTIONS OF WIRE PERCENTAGE

						P	ER CENT.
; ;	.010	.015	.020	.025	.030	.085	.040
Feet.						DEI	LECTION
10 20 30 40	.1 .2 .3 .4 .5	.150 .300 .450 .600	.200 .400 .600 .800	.250 .500 .750 1.000	.300 .600 .900 1.200	.350 .700 1.050 1.400	.400 .800 1.200 1.600
50 60 70	.6	.750 .900 1.050	1.000 1.200 1.400	1.250 1.500 1.750	1.500 1.800 2.100	2.100 2.450	2.400 2.800
80 90 100 110	.8 .9 1.	1.200 1.350 1.500 1.650	1.600 1.800 2.000 2.300	2.000 2.250 2.500 2.750	2.400 2.700 3.000 3.300	2.800 3.150 3.500 3.850	3.200 3.600 4.000 4.400
120 130 140 150	1.2 1.3 1.4 1.5	1.800 1.950 2.100 2.250	2.400 2.600 2.800 3.000	3.000 3.250 3.500 3.750	3.600 3.900 4.200 4.500	4.200 4.550 4.900 5.250	4.800 5.200 5.600 6.000
160 170 180 190 200	1.6 1.7 1.8 1.9 2.	2.400 2.550 2.700 2.850 3.000	3.200 3.400 3.600 3.800 4.000	4.000 4.250 4.500 4.750 5.000	4.800 5.100 5.400 5.700 6.000	5.600 5.950 6.300 6.650 7.000	6.400 6.800 7.200 7.600 8.000

]	PER CENT
اند	.085	.090	.095	.100	.110	.120	.130
Feet.		·			<u>'</u>	DE	FLECTION
10	.850	.900	.950	1.000	1.100	1.200	1.300
20	1.700	1.800	1.900	2.000	2.200	2.400	2.600
30	2.550	2.700	2.850	3.000	3.300	3.600	3.900
40	3.400	3.600	3.800	4.000	4.400	4.800	5.200
50	4.250	4.500	4.750	5.000	5.500	6.000	6.500
60	5.100	5.400	5.700	6.000	6.600	7.200	7.800
70	5.950	6.300	6.650	7.000	7.700	8.400	9.100
80	6.800	7.200	7.600	8.000	8.800	9.600	10.400
90	7.650	8.100	8.550	9.000	9.900	10.800	11.700
00	8.500	9.000	9.500	10.000	10.000	12.000	13.000
110	9.350	9.900	10.450	11.000	11.100	13.200	14.300
20	10.200	10.800	11.400	12.000	12.200	14.400	15.600
30	11.050	11.700	12.350	13.000	13.300	15.600	16.900
40	11.900	12.600	13.300	14.000	14.400	16.800	18,200
50	12.750	13.500	14.250	15.000	15.500	18.000	19.500
160	13.600	14.400	15.200	16.000	16.600	19.200	20.800
170	14.450	15.300	16.150	17.000	17.700	20.400	22.100
180	15.300	16.200	17.100	18.000	18.800	21.600	23.400
190	16.150	17.100	18.050	19.000	19.900	22.800	24.700
200	17.000	18.000	19,000	20.000	21.000	24.000	26.000

IN FEET CORRESPONDING TO A GIVEN DEFLECTION.

DEFLECT	ions.									
.045	.050	.055		.060	.0	65	.070		.075	.080
IN FEET		!	·		!					
.450	.500	.550		.600		650	.70		.750	.800
.900	1.000	1.100		1.200		300	1.40		1.500	1.600
1.350 1.800	1.500 2.000	1.650 2.200		$1.800 \\ 2.400$		950 600	2.10 2.80		2.250 3.000	2.400 3.200
2.250	2.500	2.750		3.000		250	3.50		3.750	4.000
2.700	3.000	3.300	- 8	3.600	3.9	900	4.20	0	4.500	4.800
3.150	3.500	3.850		4.200		550	4.90		5.250	5.600
3.600 4.050	4.000 4.500	4.400 4.950		4.800 5.400		200 850	5.60 6.30		6.000 6.750	
4.500	5.000	5.500		5.400 6.000		500 500	7.00		7.500	7,200 8,000
4.950	5,500	6.050	-	6.600		150	7.70		8,250	8.800
5.400	6.000	6.600		7.200		800	8.40		9.000	9.600
5.850	6.500	7.150		7.800		450	9.10		9.750	10.400
6.300	7.000	7.700		8.400		100	9.80		10.500	11.200
6.750	7.500	8.250		9.000	9.7	750	10.50	_	11.250	12.000
7.200	8.000	8.800		9.600	10.4		11.20		12.000	12.800
7.650 8.100	8.500 9.000	9.350 9.900		0.200 0.800	11.0	700	11.90 12.60		12.750 13.500	13.600 14.400
0.100										
8.550 9.000 DEFLECT	9.500 10.000	10.450 11.000	11	1.400 2.000	12.3 13.6	350	13.30 14.00	0	14.250 15.000	15.200 16.000
8.550 9.000 DEFLECT	9.500 10.000	10.450	112	1.400	12.3	350	13.30	0	14.250 15.000	15.200 16.000
8.550 9.000	9.500 10.000	10.450	112	1.400	12.3	350	13.30	0	14.250	15.200
8.550 9.000 DEFLECT	9.500 10.000 TIONS.	10.450	112	1.400	12.3	350	13.30	0	14.250 15.000	15.200 16.000
8.550 9.000 DEFLECT .140	9.500 10.000	10.450 11.000	000	1.400 2.000	700	350 000	180	0	14.250 15.000	15.200 16.000
8.550 9.000 DEFLECT .140 EN FEET 1.400 2.800	9.500 10.000 TONS	.160	000	1.400 2.000	700 400	350 000	13.30 14.00	0	14.250 15.000 .190 1.900 3.800	.200 2.000 4.000
8.550 9.000 DEFLECT .140 EN FEET 1.400 2.800 4.200	9.500 10.000 TONS. .150 1.500 3.000 4.500	.160 11.000 .160	0000000	1.400 2.000	700 400 100	350 0000	13.30 14.00 180 1.800 3.600 5.400	0	14.250 15.000 .190 1.900 3.800 5.700	.200 2.000 4.000 6.000
8.550 9.000 DEFLECT .140 EN FEET 1.400 2.800	9.500 10.000 TONS	.160 11.000 .160	00 00 00 00 00 00	1.400 2.000	700 400	350 000	13.30 14.00	0	14.250 15.000 .190 1.900 3.800 5.700 7.600	.200 2.000 4.000 8.000
8.550 9.000 DEFLECT .140 N FEET 1.400 2.800 4.200 5.600 7.000	9.500 10.000 10.000 	.160 1.160 .160 .160 .160 .160 .160 .160	00 00 00 00 00 00 00 00 00 00 00 00 00	1.400 2.000	700 400 100 800 500	350 000	180 1.800 3.600 5.400 7.200 9.000	0	14.250 15.000 .190 .190 3.800 5.700 7.600 9.500	.200 2.000 4.000 6.000 10.000
8.550 9.000 DEFLECT .140 1.400 2.800 4.200 5.600 7.000 8.400	1.500 10.000 10.000 10.000 1.500 1.500 4.500 6.000 7.500 9.000	.160 11.000 .160 .160 .160 .160 .160 .16	000 000	1.400 2.000	700 400 100 800 500 200	350 000	1.800 1.800 3.600 5.400 7.200 9.000 0.800	00	14.250 15.000 .190 .190 1.900 3.800 5.700 7.600 9.500 11.400	.200 2.000 4.000 6.000 10.000
8.550 9.000 DEFLECT .140 N FEET 1.400 2.800 4.200 5.600 7.000	9.500 10.000 10.000 	.160 11.000 .160 .160 .160 .160 .160 .16	000 000	1.400 2.000	700 400 100 800 500	350 000	180 1.800 3.600 5.400 7.200 9.000	000	14.250 15.000 .190 .190 1.900 3.800 5.700 7.600 9.500 11.400 13.800	.200 2.000 2.000 4.000 6.000 10.000 12.000
8.550 9.000 DEFLECT .140 N FEET 1.400 2.800 4.200 5.600 7.000 9.800 11.200 12.600	1.500 1.500 1.500 1.500 1.500 1.500 1.500 12.000 13.500	10.456 11.000 160 	000 000	1.400 2.000 1.17 3.5.6.8. 10.11.13.15.	700 400 100 800 500 200 900 900 300	10 11 11 11 11 11	180 1.800 1.800 3.600 5.400 7.200 9.000 1.800 1.400 1.400 1.400	000	14.250 15.000 .190 .190 1.900 3.800 5.700 7.600 9.500 11.400 13.300 15.200 17.100	.200 2.000 4.000 6.000 10.000
8.550 9.000 DEFLECT .140 N FEET 1.400 2.800 4.200 5.600 7.000 8.400 9.800 11.200	1.500 3.000 4.500 2.000 4.500 10.500 12.000 13.500 15.000	10.456 11.000 160 	000000000000000000000000000000000000000	1.400 2.000 1.17 3.5.6.8. 10.11.13.15.	700 400 100 800 200 900 600	10 11 11 11 11 11	180 1.800 3.600 5.400 7.200 9.000 1.800 1.800 1.400	000	14.250 15.000 .190 1.900 3.800 5.700 9.500 11.400 13.300 15.200	.200 2.000 4.000 6.000 8.000 12.000 14.000
8,550 9,000 DEFLECT .140 N FEET 1.400 2.800 4.200 7.000 8.400 9.800 11.200 11.200 12.600 14.000	1.500 3.000 4.500 7.500 10.500 10.500 10.500 13.500 16.500	1.600 1.600 1.600 1.600 1.600 1.600 1.200 1.	000 000 000 000 000 000 000 000 000 00	1.400 2.000 1.17 1.3 3.5.6.8.10.11.13.15.17.17.18.	700 400 100 500 500 200 900 600 700	10 11 12 12 12 12 12 12 12 12 12 12 12 12	1.800 1.800 1.800 3.600 5.400 7.200 9.000 1.800 1.	0000	14.250 15.000 .190 .190 3.800 5.700 7.600 9.500 11.400 13.300 15.200 17.100 19.000 20.900	.200 2.000 4.000 6.000 8.000 10.000 12.000 16.000 18.000 20.000 22.000
8.550 9.000 DEFLECT .140 .N FEET 1.400 2.800 4.200 5.600 7.000 9.800 11.200 12.600 14.000 15.400 16.800	1.500 1.500 1.500 1.500 1.500 1.500 12.000 13.500 15.000 16.500 18.000	10.456 11.000 .160 .160 .160 .160 .160 .160 .160 .160 .160 .160 .176 .17	000 000 000 000 000 000 000 000 000 00	1.400 2.000 1.17 3. 5. 6. 8. 10. 11. 13. 15. 17. 18. 20.	700 400 100 800 500 200 900 600 300 000 700 400	10 11 11 11 11 12 12 12	1.800 1.800 3.600 5.400 7.200 9.000 1.800 1.	000	14.250 15.000 .190 .190 3.800 5.700 7.600 9.500 11.400 13.300 15.200 15.200 15.200 17.100 19.000 20.900	2.000 4.000 8.000 10.000 12.000 14.000 18.000 20.000 22.000 24.000
8.550 9.000 DEFLECT .140 2.800 4.200 5.600 7.000 8.400 9.800 11.200 12.600 14.000 15.400 16.800 18.200	1.500 3.000 4.500 6.000 7.500 12.000 13.500 18.000 18.000 19.500	16.456 11.000 1.160 1.160 1.160 1.281 1.28	000 000 000 000 000 000 000 000 000 00	1.400 2.000 1.17 1.3 5.6 8. 10. 11. 13. 15. 17. 18. 20. 22.	700 700 700 700 700 700 800 500 200 600 300 600 700 400 1100	10 11 11 12 22 22	1.800 1.800 1.800 3.600 5.400 7.200 9.800 1.400 3.200 3.200 3.200 3.200 3.200 3.200 3.200 3.200 3.200 3.200	000	14.250 15.000 .190 .190 3.800 5.700 9.500 11.400 18.300 17.100 19.000 20.900 22.800 22.800	.200 2.000 4.000 6.000 8.000 10.000 12.000 14.000 20.000 22.000 24.000 22.000 24.000
8.550 9.000 DEFLECT .140 .N FEET 1.400 2.800 4.200 5.600 7.000 9.800 11.200 12.600 14.000 15.400 16.800	1.500 1.500 1.500 1.500 1.500 1.500 12.000 13.500 15.000 16.500 18.000	10.450 11.000 11.000 1.160 1.160 1.120 1.00 1.0	000 000 000 000 000 000 000 000 000 00	1.400 2.000 1.17 1.3.5 5.6.8.10.11.13.15.17.18.20.22.22.22.23.8	700 400 100 800 500 200 900 600 300 000 700 400	10 11 11 11 12 22 22	1.800 1.800 3.600 5.400 7.200 9.000 1.800 1.	000	14.250 15.000 .190 .190 3.800 5.700 7.600 9.500 11.400 13.300 15.200 15.200 15.200 17.100 19.000 20.900	2.000 4.000 8.000 10.000 12.000 14.000 18.000 20.000 22.000 24.000
8.550 9.000 DEFLECT .140 1.400 2.800 4.200 7.000 8.400 9.800 11.200 12.600 14.000 15.400 16.800 18.200 19.600 21.000	1.500 3.000 4.500 6.000 7.500 10.500 12.000 18.000 18.000 18.000 19.500 21.000	10.456 11.000 1.160 1.160 1.160 1.128 1.28 1.28 1.28 1.29 1.29 1.29 1.29 1.29 1.29 1.29 1.29	000 000 000 000 000 000 000 000 000 00	1.400 2.000 11. 3. 5. 6. 8. 10. 11. 13. 15. 17. 17. 18. 20. 22. 22. 23. 25.	700 400 100 800 200 900 600 200 900 600 700 400 100 800 500	10 11 11 11 11 12 22 22 22	180 1.800 3.600 5.400 7.200 0.800 1.800 1.800 1.800 1.800 1.800 1.600 1.400 1.600 1.400 1.600 1.40	000	14.250 15.000 1.900 3.800 5.700 7.600 9.500 13.800 15.200 17.100 19.000 22.800 24.700 26.600 28.500	2.000 2.000 4.000 8.000 10.000 12.000 14.000 18.000 20.000 22.000 24.000 28.000 30.000
8.550 9.000 DEFLECT .140 2.800 4.200 5.600 9.800 11.200 12.600 11.200 15.400 16.800 18.200 21.000 22.400 23.800	1.500 10.000 10.000 10.000 10.500 10.500 12.000 13.500 15.000 18.000 19.500 22.500	10.450 11.000 1.160 1.160 1.160 1.160 1.12	000 000 000 000 000 000 000 000 000 00	1.400 2.000	7700 4400 1100 8800 600 2200 900 0000 7700 400 1100 8800 1100 8800 1100 8800 1100 8800 1100 10	11:11:11:11:12:22:22:22:22:23:33:50	180 1.800 3.600 5.400 7.200 9.000 1.80	000	14.250 15.000 .190 1.900 3.800 7.600 9.500 11.400 13.300 15.200 17.100 19.000 22.800 24.700 26.600	.200 2.000 4.000 6.000 8.000 12.000 14.000 16.000 20.000 22.000 22.000 22.000 23.000 24.000 25.000 28.000
8.550 9.000 DEFLECT .140 1.400 2.800 4.200 5.600 7.000 8.400 9.800 11.200 12.600 14.000 15.400 16.800 18.200 19.600 21.000 22.400	1.500 3.000 4.500 7.500 10.500 10.500 11.500 12.000 13.500 18.000 19.500 22.500 24.000	10.450 11.000 1.160 1.160 1.160 1.128 1.160 1.128 1.160 1.17.6	000 000 000 000 000 000 000 000 000 00	1.400 2.000 1.17 1.3 3.3 5.6 6.8 8.10.11.13.15.17.7.18.8.20.22.23.23.23.23.23.23.23.23.23.23.23.23.	700 400 100 800 500 200 600 300 600 400 100 400 100 800 500 200 200 200 200 200 200 200 200 2	350 0000 11 11 12 22 22 22 23 33	180 1.800 3.600 5.400 7.200 9.000 1.80	00	14.250 15.000 1.900 3.800 5.700 9.500 11.400 13.300 15.200 17.100 20.900 22.800 22.800 24.700 25.500 30.400	.200 2.000 4.000 6.000 8.000 10.000 12.000 14.000 12.000 22.000 24.000 22.000 23.000 30.000 32.000

TABLE OF STRAINS AT CENTER OF SPANS RESULT

	Feet.					PER CENT.
Poles to Mile.	Spans in Fe	.004	.006	.008	.010	.015
Pole	Spe					Multi
20	264.0	8 250.176	5 500.264	4 125.352	8 300.440	2 200.660
21	251.4	7 856.417	5 237.751	8 928.460	8 142.919	2 095.628
22	240.0	7 500.160	5 000.240	8 750.320	8 000.400	2 000.600
23	229.5	7 172.028	4 781.479	8 586.243	2 869.132	1 913.073
24	220.0	6 875.146	4 583.553	8 437.793	2 750.366	1 833.883
25	211.2	6 600.140	4 400.211	8 300.281	2 640.352	1 760.528
26	203.0	6 343.885	4 229.369	8 172.145	2 537.838	1 692.174
27	195.5	6 109.505	4 073.112	8 054.948	2 444.075	1 629.655
28	188.5	5 890.750	3 927.271	2 945.563	2 356.564	1 571.304
29	182.0	5 687.621	8 791.848	2 843.992	2 275.303	1 517.121
30	176.0	5 500.117	3 666.842	2 750.234	2 200.293	1 467.106
81	170.8	5 321.988	3 548.086	2 661.164	2 129.033	1 419.592
32	165.0	5 136.360	3 437.665	2 578.345	2 062.775	1 375.412
33	160.0	5 000.106	8 333.493	2 500.213	2 000.266	1 333.733
34	155.3	4 853.228	3 235.571	2 426.769	1 941.508	1 294.554
35	150.8	4 712.600	3 141.817	2 356.451	1 885.251	1 257.043
36	146.6	4 581.347	3 054.313	2 290.820	1 832.744	1 222.033
37	142.7	4 459.470	2 973.059	2 229.877	1 783.987	1 189.523
38	138.9	4 340.717	2 893.888	2 170.497	1 736.481	1 157.847
39	135.4	4 231.840	2 820.968	2 115.805	1 692.725	1 128.671
40	132.0	4 125.088	2 750.132	2 062.676	1 650.220	1 100.330
41	128.8	4 025.085	2 683.462	2 012.671	1 610.214	1 073.655
42	125.7	3 928.208	2 618.875	1 964.230	1 571.459	1 047.814
43	122.8	3 837.581	2 558.456	1 918.913	1 535.204	1 023.640
44	120.0	3 750.080	2 500.120	1 875.160	1 500.200	1 000.300
45	117.3	3 665.703	2 443.867	1 832,968	1 466.445	977.793
46	114.7	3 584.451	2 389.698	1 792,339	1 433.941	956.120
47	112.3	3 509.449	2 339.695	1 754,836	1 403.937	936.114
48	110.0	3 437.573	2 291.776	1 718,896	1 375.183	916.941
49	107.7	3 365.696	2 243.857	1 682,955	1 346.429	897.769
50	105.6	3 300.070	2 200.106	1 650,140	1 320.176	880.264

ING FROM A GIVEN PERCENTAGE DEFLECTION.

DEFLECTION	8.					
.020	.025	.030	.035	.040	.045	.050
PLIERS.				<u>'</u>	'	
1 650.880	1 321.100	1 101.320	944.397	826.760	735.818	662.200
1 572.088	1 258.047	1 048.757	899.323	787.301	700.218	630.595
1 500.800	1 201.000	1 001.200	858.542	751.600	668.466	602.000
1 435.140	1 148.456	957.364	820.981	718.717	639.221	575.662
1 375.733	1 100.916	917.766	786.997	688.966	612.761	551.839
1 320.704	1 056.880	881.056	755.517	661.408	588,250	529.760
1 269,426	1 015.845	846.848	726.184	635,728	565.410	509.191
1 222,526	978.314	815.560	699.354	612.240	544.521	490.379
1 178.753	943.285	786.359	674.314	590.319	525.024	472.820
1 138.106	910.758	759.243	658.204	569.963	506.920	456.510
1 100,586	880.733	734.213	629.598	551.173	490,208	441.466
1 064.942	852,209	710.434	609.207	533.322	474.332	427.169
1 031.800	825.687	688.325	590.248	516.725	459.570	413.87
1 000.533	800,666	667.466	572.361	501.066	445.644	401.33
971.142	777.147	647.859	555.548	486.347	432.552	389.54
943.002	754.628	629.087	539,451	472,255	420.019	378,25
916.738	733.610	611.566	524.426	459.102	408.321	367.72
892.350	714.096	595,296	510.475	446.888	397.459	357.93
868.588	695,078	579.444	496.881	434.988	386.875	348.40
846.701	677.564	564.843	484.361	424.027	377.126	339.62
825,440	660,550	550.660	472.198	413,380	367.656	331.10
805.429	644.536	537.310	460.751	403.358	358.743	323.07
786.044	629.023	524.378	449.661	393.650	350.109	315.29
767.909	614.511	512.280	439.287	384.568	342.032	308.02
750.400	600.500	500.600	429.271	875.800	334.233	301.00
733.516	586,988	489.336	419.612	367.344	326.713	294.22
717.257	573.977	478.490	410.311	359.202	319.471	287.70
702.249	561.967	468.478	401.726	351.686	312.786	281.68
687.866	550.458	458.883	393.498	844.483	306.380	275.91
673.484	538.948	449.288	385.271	337.280	299.974	270.14
660.352	528.440	440.528	377.758	330.704	294.125	264.88

Rule.—To find strain in pounds on wire of given span and deflection, multiply numbers in column answering to wire span and deflection by the weight per foot of wire.

TABLE OF STRAINS AT CENTER OF SPANS RESULTING FROM A GIVEN PERCENTAGE DEFLECTION.

					חייים	DEF LECTION.					
					PER CE	CENT. DEFLECTIONS.	TIONS.				
ns in eet.	.001	.002	£00°.	400 .	900:	900.	200.	800°	600*	.010	.015
eqs A					M	MULTIPLIERS.					
2	1 250.001	625.003	416.671	312.506	250.008	208.343	178.583	156.263	138.903	125.016	83.358
ន	쭗	1 250.006	833.343	625.013	500.016	416.686	357.166	312.526	277.807	250.033	166.716
8	33	1 875.010	1 250.015	937.520	750.025	625.030	535.749	468.790⊨	416.711	375.050	250.075
4	2 000.006	2 500.013	1 666.686	1 250.026	1 000.033	833.373	714.332	625.053	555.615	200.066	333.433
23	S	3 125.016	2 083.358	1 562.533	1 250.041	1 041.716	892.915	781.316	694.519	625.083	416.791
8	7 500.010	3 750.020	2 500.030	1 875.040	1 500.050	1250.060	_	937.580	833.423	750.100	500.150
2	8 750.011	4 375.023	2916.701	2 187.546	1750.058	1 458.403	1250	1 093.843	972.327	875.116	583.508
8	10 000 013	5 000.026	3 333.373	2 500.053	2 000.066	1 666.746	1 428	1 250.106	1111.231	1 000.133	998.999
8	11 250.015	5 625.030	3 750.045	2 812.560	2 250.075	1 875.090	1 604	1 406.370	1 250.135	1 125.150	750.225
8	12 500.016	6 250.033	4 166.716	3 125.066	2 500.083	2 083.433	1 785	1 562.633	1 389.038	1 250 166	833.583
110	13 750.018	6 875.036	4 583.388	3 437.573	2 750.091	2 291.776	1 964.414	1 718.896		1 375.183	916.941
130	15 000.020	7 500.040	2 000.060	3 750.080	3 000.100	2500.120	2 142.997	1 875.160	1 666.846	1 500.200	1 000.300
130	16 250.021	135	5416.731	4 062.586	3 250.108	2 708.463	2 321.580	2 031.423		1 625.216	1 083.658
140	17 500.023	8 750.046	5 833.403	4 375.093	3 500.116	2 916.806	2 500.163	2187.686		1 750.233	1 167.016
22	18 750.025	375	6 250.075	4 687.600	3 750.125	3 125.150	2 678.746	2 343.950		1 875.250	1 250.375
160	8	8	6 666.746	5 000.106	4 000.133	3 333.493	2 857.329	2 500.213	2 222.462	2 000.266	1 333.733
170	21 250.028	10 625.056	7 083.418	5312.613	4 250.141	3 541.836	3035.912	2 656.476	2 361.366	2 125.283	1 417.091
8	ဒ္ဓ	S	2 200.090	5625.120	4 500.150	8	3 214.495	2 812.740	2 500.269	2 250.300	1500.450
190	33	375	7 916.761	5 937.626	4 750.158	95	3 393.078	2 969.003	2 639.173	2 375.316	1 583.808
8	ş	g	8 333.433	6250.133	$5\ 000.166$	4 166.866	3571.661	3 125.266	2 778.077	2 500.333	1 667.166

TABLE OF STRAINS AT CENTER OF SPANS RESULTING FROM A GIVEN PERCENTAGE DEFLECTION—Continued.

50.041 41.716 35.772 31.316 27.852 25.083 22.818 20.933 19.839 17.973 16.791 50.041 41.716 35.772 31.316 27.852 25.083 22.818 20.933 19.839 17.973 16.791 200.106 88.433 71.546 62.683 65.765 60.166 45.687 41.866 88.678 35.947 88.689 200.106 166.866 143.090 125.266 60.166 45.687 41.866 86.758 35.947 88.689 200.106 166.866 143.090 125.266 60.166 45.687 41.866 86.758 88.947 88.689 200.106 166.866 143.090 125.268 114.044 104.666 96.695 96.956 83.966 88.966 200.106 20.8530 18.858 18.858 18.858 114.044 104.666 96.695 96.956 83.166 106.756 106.756 106.756 106.756 106.756 106.756				a	PER	PER CENT. DEFLECTIONS.	PER CENT. DEFLECTIONS.	ż				
41.716 35.772 31.316 27.852 25.083 22.818 20.933 19.339 17.973 15.545 15.705 15.705 15.200 68.456 71.865 15.705 15.200 88.453 17.545 62.805 85.705 100.339 17.973 15.540 1	.025		.030	.035	.040	.045	.050	- 929	090	.065	.070	.075
41,716 35,772 31,316 27,82 25,082 22,818 20,933 19,339 17,973 155,130 17,317 82,536 50,166 45,637 41,866 86,017 83,247 105,130 17,317 82,506 111,411 100,339 91,276 82,601 83,211 20,203 17,846 113,411 100,339 17,556 18,646 77,556 77,576 77,477 77,477 77,477 77,477				i		MULTIPL	ERS.					
83,133 71,245 62,633 65,705 60,166 45,637 41,866 88,677 83,947 165,130 113,130 113,131 100,333 64,667 68,466 68,607 88,917 83,917 202,230 113,130 113,241 100,333 114,064 114,666 96,607 83,917 202,300 214,655 113,241 110,414 114,064 114,666 96,607 89,919 202,300 214,655 113,241 110,434 115,476 116,638 115,537 17,356 11,896 202,300 214,655 120,216 194,994 175,587 186,537 146,537 175,816 185,721 146,637 147,611 187,739 315,450 222,166 220,666 184,527 222,187 183,311 179,738 173,536 147,711 186,737 183,311 179,738 183,311 179,738 183,311 179,738 183,311 179,738 183,311 179,738 186,310 186,510 186,	25	140	41.716	35.772	31.316	27.852	25.083	22.818	20.933	19.339	17.973	16.791
125,136 135,240 83,558 75,250 68,456 62,800 86,017 82,017 83,527 175,250 175,250 82,528 175,250 175,250 175,850 175,850 175,850 175,850 175,850 175,850 175,850 175,850 175,850 186,950 186,650 186,650 186,650 186,650 186,650 186,650 186,650 186,650 186,650 186,650 186,650 186,650 186,650 186,751 147,186 187,171 187,17	2	8	83.433	71.545	62.633	55.705	50.166	45.637	41.866	38.678	35.947	33.583
106.858 143.09 125.26 111.411 100.333 91.276 88.738 77.356 71.366 71.886 250.300 214.635 187.001 167.116 150.801 125.600 116.034 107.812 250.300 214.635 187.001 167.116 150.801 116.034 107.812 280.300 214.635 187.001 167.116 150.801 116.034 107.812 280.130 220.135 280.180 200.033 188.400 114.051 161.764 417.146 357.726 313.106 278.527 200.606 182.401 174.051 161.744 488.883 384.485 226.074 225.182 200.814 197.731 188.400 174.051 161.744 460.60 490.275 313.406 200.806 200.806 200.806 197.731 188.400 174.73 173.738 460.60 490.275 314.483 304.086 275.318 200.806 200.806 197.747 251.638	35	3	001.07	107.317	93.950	83.558	75.250	68.456	62.800	58.017	53.921	50.375
20.300 21.50.50 21.50.50 20.00	9,5	96	166.866	143.090 178.863	125.266	130 963	100.333	91.275	86.73 56.73	77.356	71.895	67.166
292.016 20.0440s 219.216 150.500 136.918 135.500 136.921 140.582 136.932 146.688 147.846 147.746 <	3	3	700.00	7,000	100.000	102.200	150.410	114.02	104.000	30,030	89,209	83.958
282.734 28.61.80 29.65.180 29.62.180 19.67.81 146.581 155.781 114.686 185.712 145.781 155.781 185.782 185.782 185.783 185.783 185.783 185.783 185.783 185.783 185.783 185.783 185.783 185.783 185.744 185.745 185.745 185.745 185.745 185.745 185.745 185.745 185.745 185.745 185.745 185.745 185.745 185.745 185.745 185.745	9	250	250.300	214.635	187.900	167.116	150.500	136.913	125.600	116.034	107.842	100.750
38.7.746 313.105 222.28.2 220.68.2 200.666 182.551 167.466 164.712 143.790 417.166 357.726 318.106 278.227 225.787 188.400 174.61 161.744 458.883 383.498 344.483 386.389 275.916 251.086 230.266 212.730 117.711 500.60 429.271 373.207 188.408 384.283 381.000 220.266 212.730 117.711 554.235 565.044 47.116 384.283 384.283 384.285 251.066 272.213 251.408 286.56 554.235 566.544 47.116 376.274 373.277 251.685 554.685 667.466 57.23 61 884.938 851.166 319.465 293.066 270.747 251.685 667.466 57.23 61 866.046 376.228 386.516 386.516 386.516 386.516 386.516 386.516 386.516 386.516 386.516 386.516 386.516 386.514	33	<u> </u>	292.016	250.408	219.216	194.969	175.583	159.732	146.533	135.373	125.816	117.541
477.166 377.256 280.674 225.770 206.870 188.400 114.661 167.764 458.883 383.486 280.887 275.916 275.108 290.383 183.301 179.738 458.884 383.486 344.483 306.880 775.916 275.108 280.266 215.687 562.316 455.044 407.116 380.386 275.916 271.206 222.069 215.685 564.035 506.816 407.711 380.388 381.166 319.465 280.066 270.747 251.685 657.706 506.589 460.750 417.701 376.229 382.284 374.000 290.086 270.747 251.685 667.466 57.70 417.701 376.229 382.284 384.635 386.566 270.086 270.747 251.685 667.466 57.70 566.589 460.776 476.584 487.791 376.886 387.741 376.580 770.10 576.526 67.056 607.367 476.587 38	₹	.83	333.733	286.180	250.533	222.825	200.666	182.551	167.466	154.712	143.790	134.333
417.106 357.726 313.106 278.527 250.633 228.138 209.333 193.391 179.738 495.804 498.207 376.207 250.635 200.666 220.266 212.730 197.711 500.600 465.044 407.116 382.086 286.686 220.203 221.408 221.730 221.685 542.316 465.044 407.116 382.086 320.686 220.204 220.086 220.086 657.746 556.589 460.750 417.791 376.220 320.204 220.086 220.086 667.466 572.331 400.086 220.086 220.086 220.086 220.086 709.18 608.134 522.383 473.497 426.416 887.301 865.54 320.084 320.086 709.18 608.134 582.383 473.497 476.589 476.589 387.131 865.549 320.084 320.586 709.18 608.134 620.334 476.589 456.578 476.589 456.578	<u>4</u>	375	375.450	321.953	281.850	250.674	225.750	205.370	188.400	174.051	161.764	151.125
458.883 383.498 314.483 306.380 275.916 251.006 220.266 212.730 197.711 500.60 429.271 375.800 384.233 381.000 273.827 251.408 232.636 212.730 1197.711 542.316 465.044 47.116 384.233 389.938 351.166 373.233 200.066 270.747 251.635 667.466 572.361 687.466 772.333 862.03 374.027 251.635 667.466 572.361 687.466 445.644 401.338 865.108 324.086 270.747 251.635 709.183 608.134 682.283 473.447 474.644 401.338 865.108 324.686 387.64 386.546 709.183 608.134 682.283 473.447 426.447 426.547 426.549 365.546 387.642 387.642 709.183 608.183 682.103 476.549 476.549 476.549 387.642 387.742 341.642 709.184 <td< td=""><td>3</td><td>0.416</td><td>417.166</td><td>357.726</td><td>313.166</td><td>278.527</td><td>250.833</td><td>228.189</td><td>209,333</td><td>193.391</td><td>179.738</td><td>167.916</td></td<>	3	0.416	417.166	357.726	313.166	278.527	250.833	228.189	209,333	193.391	179.738	167.916
562.316 455.044 374.235 801.000 273.827 251.200 222.069 215.685 582.316 455.044 478.118 389.388 386.166 282.064 271.685 286.656 286.066 270.747 231.685 286.656 286.066 270.747 231.685 286.666 286.066 270.046 286.066 270.747 231.635 286.066 270.046 286.066 270.046 286.066 270.046 286.066 270.046 286.066 270.046 286.066 286.067 286.066 286.067 286.066 286.067 286.066 286.067 286.066 286.067 286.	687.866 55	0.458	458.883	393.498	344.483	306.380	275.916	251.008	230.266	212.730	117.711	184.708
542.351 465.044 407.116 362.086 326.065 296.646 772.133 251.408 238.659 684.035 564.035 566.589 466.736 417.791 376.234 319.466 270.146 238.659 667.466 572.361 500.006 445.644 401.332 865.103 384.833 309.425 287.560 709.185 608.134 562.385 473.497 426.416 887.921 855.866 328.744 306.554 709.185 608.134 622.385 471.347 426.416 887.921 855.866 328.744 306.554 709.185 608.134 622.385 451.500 410.749 876.800 388.142 316.554 894.333 715.452 626.335 657.055 601.666 456.578 418.666 386.782 389.476		0.500	200,600	429.271	375.800	334.233	301.000	273.827	251.200	232.069	215.685	201,500
64.736 56.586 438.433 389.938 351.166 319.466 270.747 251.633 62.5760 556.586 460.750 417.791 376.236 342.234 314.000 290.066 290.066 667.466 57.2361 60.01.066 417.791 376.236 385.103 349.697 387.783 709.185 608.134 582.383 473.497 426.418 387.211 355.866 387.741 387.569 790.186 608.134 582.383 473.497 426.418 461.500 410.748 387.848 387.741 383.585 792.616 679.679 585.016 580.322 476.583 438.569 387.733 387.442 341.502 843.333 715.422 626.335 567.056 501.666 456.378 418.666 386.778 389.479		0.541	542.316	465.044	407.116	362.086	326.083	296.646	272.133	251.408	233.659	218.291
625, 750 566,589 469,750 417,791 376,220 382,224 314,000 290,086 269,667 667,466 67,2361 607,066 445,644 401,338 385,103 384,938 390,425 287,569 760,9188 688,137 682,789 476,589 387,513 365,846 387,574 365,546 7750,907 683,707 476,589 476,589 387,189 387,189 382,589 715,452 626,533 565,016 476,589 387,789 387,189 381,189 844,333 715,452 626,333 567,035 501,686 456,578 386,779 386,779		.583	584.033	500.816	438.433	389.938	351.166	319.465	293.066	270.747	251.633	235.083
667,466 572,861 501.066 445.644 401.383 865.103 334.983 309.425 287.580 709.185 608.134 622.383 473.497 426.416 887.921 355.866 326.764 305.554 750.900 643.907 563.700 563.202 476.554 487.559 387.733 871.442 385.52 854.333 715.452 626.335 567.055 501.666 456.378 418.666 386.782 359.476		.625	625.750	536.589	469.750	417.791	376.250	342.284	314.000	290.086	269.607	251.875
709.183 608.134 582.383 473.497 426.416 887.921 855.866 828.764 805.554 750.900 648.907 568.700 501.349 451.500 410.740 876.800 348.118 323.558 772.616 674.679 805.016 65.000 568.900 668.900 406.800 406.800 848.182 811.502 884.333 715.452 626.833 657.055 501.666 456.878 418.666 886.782 859.476	000.533 800	999	667.466	572.361	501.066	445.644	401.333	365.103	334.933	309.425	287.580	268,666
750.200 643.907 643.700 501.349 451.500 410.740 876.800 345.118 323.559 792.616 679.679 686.016 620.329 476.583 423.559 897.733 867.442 941.592 894.333 715.452 626.333 657.055 501.666 456.578 418.666 386.792 559.476		.708	709.183	608.134	532.383	473.497	426.416	387.921	355.866	328.764	305.554	285.458
792,616 679,679 596,016 529,202 476,583 433,559 397,733 867,442 341,502 884,333 715,452 626,333 557,055 501,666 456,378 418,666 386,782 359,476		750	750.900	643.907	563.700	501.349	451.500	410.740	876.800	348.103	323.528	302.250
834.333 715.452 626.333 657.055 501.666 456.378 418.666 386.782 359.476		.791	792.616	629.629	595.016	529.505	476.583	433.559	397.733	367.442	341.502	319.041
	_	88	834.333	715.452	626.333	557.055	501.666	456.378	418.666	386.782	359.476	335.833

TABLE OF STRAINS AT CENTER OF SPANS RESULTING FROM A GIVEN PERCENTAGE DEFLECTION—Continued.

							LEE CENT		TEL TEL TOWN						
ni si is	080	.085	060.	.095	.100	.110	.120	.130	.140	.150	.160	.170	.180	.190	.200
Spar							Mu	MULTIPLIERS.	18.						
10	15.758	14.847	14.058	13.316	12.666	11.546	10.616	9.832	9.161	8.583	8.079	7.636	7.244	6.895	6.583
38	31,516	29,635	42,116	20,022	38.000	34.640	81.850	29,496	27,485	25.750	24,237	20.202	21.733	20.686	19.750
99	63,033	59.390	56.155	53.264	50.066	46.187	42,466	39.328	36.647	34.333	32.316 40.895	38,181	28.977	27 582	26.333
202	94.550	89.085	84,233	79.897	76.000	69.281	63.700	68.992		51.500	48.475	45.817 53.453	43.466 50.711	41.378	39.500
98	126,066	133,627	126.350	119.846	101.333	92.375	96.550	78.656 88.488	78.295	77.250	72,712	61.090	65,199	55.164	59.250
100	157.583	148.475	140,388	135,162	126,666	119,469	106,166	100 150	- 12	89,883	80.791	76.362	72.444	68.956	65.833
150	189.100	178.170		159.794		138,563	127.400	117.984	109.942	103.000	96,950	91.635	86.933	82.747	79.000
130	201.858	193.018	182,505	178,110	164,666	150,110	138,016	127.816	128,266	120.166	105.029	106.907	94.177	89.642	85.583
150	236.375	222,713		199.743		178.204	159.250	147.480	137.428	128.750	121,187	114.544	108.666	103.434	98.750
160	252,133	237.560	224.622	213,059	202,666	184.751	169.866	157.312	146.590	187.333	129.266	122,180	115.911	110.329	105.333
180	283,650	267.255	252,700	239.692	228.000	207.845	191.100	176.976	164.914	154.500	145.425	187,452	130.399	124.121	118,500
190	315.166	282.103	266,738	253,008	240,666	219,392	201,716	186.808	174.076	163.083	153,504	145.089	187.644	131,016	125.083

RULE.—To find strain in pounds on wire of given span and deflection, multiply numbers in column answering to wire span and deflection by the weight per foot of wire.

WEIGHTS OF INSULATED WIRE.

		WEIGHT	r PER 10	00 FEET.	WEIG	HT PER M	ILE.
Size, B. & S. Gauge.	Circular Mils.	Bare Wire.	Double-Braided Weatherproof.	Triple-Braided Weatherproof.	Bare Wire.	Double-Braided Weatherproof.	Triple-Braided Weatherproof.
•••••	500 000. 450 000. 400 000.	1 600 1 440 1 280	•••••	1 867 1 680 1 493	8 448 7 603 6 758		9 858 8 870 7 883
·····	350 000. 300 000.	1 280 1 120 960		1 307 1 120	5 914 5 069		6 901 5 914
0000	250 000. 211 600. 167 805.	800 641	703	933 739 598	4 224 3 386 2 685	3712	4 926 3 902 3 157
00	133 079.2 105 534.0	508 403 320	565 454 366	485 395	2 129 1 688	2 983 2 397 1 932	2 561 2 086
1 2	83 694.0 66 373.0	254 201	288 232	313 251	1 339 1 062	1 521 1 225	1 653 1 325
1 2 3 4 5	52 633.4 41 742.5 33 102.3	160 126 100	187 152 123	205 168 139	842 668 530	987 803 649	1 082 887 734
6 7	26 250.5 20 817.0	80 63	100 77	113 88	420 333	528 407	597 465
- 10	16 509.0 13 094.0 10 381.0	50 40 31	63 52 43	74 61 51	264 210 166	333 275 227	391 322 269
11 12	8 234.1 6 529.9	25 20	36 29	43 37	132 105	190 ;153	227 195

GALVANIZED STRANDS.

		WEIG	HT PEI FEET.	R 1000	Bu			WEIG	нт реі Геет.	R 1000	ng
Seven Wires.	Diameter.	Bare Strand.	Double-Braided Weatherproof.	Triple-Braided Weatherproof.	Estimated Breaking Strength.	Seven Wires.	Diameter.	Bare Strand.	Double-Braided Weatherproof.	Triple-Braided Weatherproof.	Estimated Breaking Strength.
No. 8	1	500	010	077	0.000	No.	,	100	140	100	1 000
9	12 52 6 8 5 6 9 27 4 18 7 1 8 8 5 6 9 27 4	$\frac{520}{420}$	616 510	677 561	$8320 \\ 6720$	15 16	1472 114694 1588 1589 1588 1588 1588 1588 1588 1588	100 80	148 122	163 134	1 600 1 280
10 11 12	32 7 ₈	360	444	488	5 720	17	32	60	96	105	960
11	38	290	362	398	4 640	18	11 i	43	76	84	688 528
12	5 16	210	270	2 97	3 360	19	9 64	33	60	66	528
13	$\frac{9}{32}$	160	214	2 35	·2 560	20	8	24	48	53	384
14	64	120	171	188	1 920	21	$\frac{3}{32}$	20	38	42	320

TABLE OF GALVANIZED E. B. B. TELEGRAPH WIRE.

Size, B. W. G.	Weight per Mile.	Resistance per Mile in Ohms.	Breaking Weight.	Twists in 6 inches.	Size, B. W. G.	Weight per Mile.	Resistance pèr Mile in Ohms.	Breaking Weight.	Twists in 6 inches.
4	730 540	6.34	1 898	18	10	260	17.79	676	24
6	540	8.45	1 404	19	11	214	21.61	556	25
8	380	12.17	988	18 19 21 22	12	165	28.03	429	27
9	330	14.01	988 858	22	14	96	48.18	250	24 25 27 28

WROUGHT-IRON WELDED STEAM, GAS AND WATER PIPE. Table of Standard Dimensions, as manufactured by National Tube Works Company.

inch of Screw. 28844 00 00 00 00 00 သြားသည္ကေတာ့ Vo. of Threads рег 7.536 9.001 10.665 12.340 14.502 18.762 23.271 28.177 33.701 40.065 435581 1585581 1.668 2.244 2.678 3.609 5.739 Pounds. per foot. Nominal Weight 166.9 96.25 70.66 80.10 85.8828 85.8828 Cubic foot. 513.0 383.3 751.2 472.4 270.0 containing one Length of Pipe OF PIPE. FT. OF 25.025 25 14.15 10.49 7.73 6.13 4.635 84448 3.645 2.768 2.871 1.848 1.547 Surface. Internal LENGTH C £35.85.78 7.075 5.657 4.547 3.637 2.904 2.301 1.608 1.328 Surface External .071 7 .124 9 .166 3 .249 2 .332 7 .495 .668 .797 1.074 1.708 2.243 2.679 3.174 3.674 4.316 5.584 6.926 8.386 10.030 11.924 Metal. TRANSVERSE AREAS. 2.038 2.038 3.356 4.784 7.388 9.887 12.730 15.961 19.990 5252525 **883888** Internal. 888888 9.621 12.566 15.904 19.635 24.306 34.472 45.664 58.426 72.760 90.763 2283338 2.1358 2.164 2.835 6.492 External. ģ .848 1.144 1.552 1.957 2.589 9.636 11.146 12.648 14.162 15.849 19.054 25.068 25.076 38.076 3.292 4.335 5.061 6.494 7.753 Inches CIRCUMFERENCE Internal. 788883 1788883 5.215 5.215 5.969 7.461 9.032 25.272 25.253 25.253 25.253 25.253 Inches External. ន្តន្តន្តន្ត Inches. 26442 25822 25822 25822 25822 25822 25822 25822 25822 25822 25822 2582 2 888255 822348 Thickness. 6.065 7.023 7.982 8.937 10.019 22422 1.048 1.380 1.611 2.067 2.468 3.067 3.548 4.026 5.045 Inches, Internal. Actual DIAMETER. 33633 1.315 1.660 1.900 2.375 2.875 8.500 4.500 5.563 5.563 6.625 8.625 9.625 0.750 Inches. External. Actual Internal Nominal

WEIGHTS AND DIMENSIONS OF LEAD-ENCASED ELECTRIC-LIGHT CABLES.

	res lire	/ire	ar	Jead.	PAPER INSU- LATION.		FIBRE INSU- LATION.	
Size, B. & S.	Number of Wires	Diameter of Wire in Mils.	Area in Circular Mils.	Thickness of Lead.	Outside Diameter.	Weight per 1000 Feet.	Outside Diameter.	Weight per 1000 Feet.
	61 61 61 61 37	99 95 91 86 104	600 000 550 000 500 000 450 000 400 000	10 10 10 10 10	$1\frac{7}{16}$ $1\frac{13}{32}$ $1\frac{3}{8}$ $1\frac{5}{16}$ $1\frac{9}{32}$	4 280 4 060 3 745 3 570 3 345	$1\frac{1}{2}$ $1\frac{5}{3}$ $1\frac{7}{6}$ $1\frac{8}{3}$ $1\frac{1}{3}$	4 475 4 245 4 030 3 755 3 520
0000	37 27 27 19 19	97 105 96 106 94	350 000 300 000 250 000 211 600 167 805	10 10 10 10 3 3 32 8	$\begin{array}{c} 1_{\frac{7}{3^{\frac{1}{2}}}} \\ 1_{\frac{8}{16}} \\ 1_{\frac{1}{8}} \\ 1_{\frac{1}{3^{\frac{1}{2}}}} \\ 1 \end{array}$	3 070 2 850 2 585 2 300 2 050	$1\frac{9}{3^{\frac{1}{2}}}$ $1\frac{1}{4}$ $1\frac{3}{16}$ $1\frac{3}{3^{\frac{1}{2}}}$ $1\frac{1}{16}$	3 240 3 020 2 755 2 425 2 175
00 0 1 2 3	19 19 7 7 7	84 75 109 98 87	133 079 105 534 83 694 66 373 52 633	8 82 5 64 64 16 16	567-243-6 128-1-1-24-32-32-32-32-32-32-32-32-32-32-32-32-32-	1 845 1 480 1 315 1 035 950	1 292 292 205 123 123 232	1 955 1 575 1 415 1 120 1 035
4 5 6	1 1 1	204 182 162	41 743 33 102 26 250	16 16 16 16	2 1 2 2 2 8 9 6 4	875 805 745	232 116 464	960 890 825

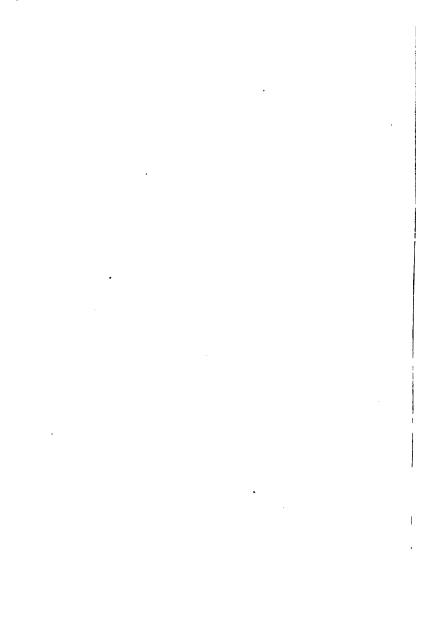
WEIGHTS AND DIMENSIONS OF LEAD-ENCASED TELEPHONE CABLES.

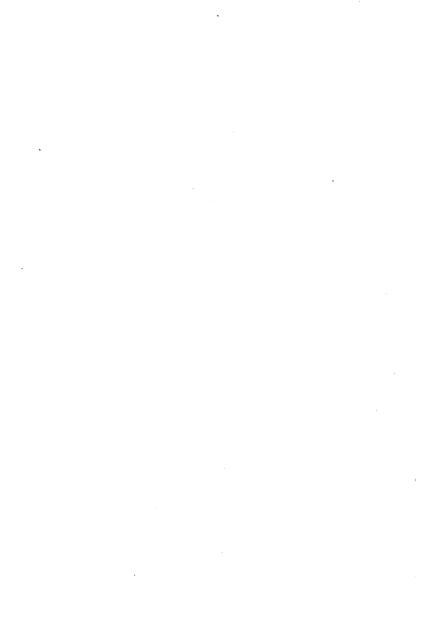
Number of Pairs.	Outside Diameter.	Weight per 1000 Feet.	Number of Pairs.	Outside Diameter.	Weight per 1000 Feet,
5 7 12 16 19 27 33 37	1 15 14 250 14 2	775 1 105 1 680 1 990 2 285 2 655 2 995 3 305	48 56 61 75 85 91 100	$1\frac{7}{8}$ $1\frac{1}{1}\frac{5}{16}$ 2 $2\frac{1}{4}$ $2\frac{5}{16}$ $2\frac{1}{2}$	3 970 4 215 4 415 5 125 5 525 5 865 6 250

WEIGHTS AND DIMENSIONS OF LEAD-ENCASED TELEGRAPH CABLES.

Con-	PAPER I	NSULATION.	COTTON INSULATION.		
Number of C ductors.	Outside Diameter.	Weight per 1000 Feet	Outside Di a meter.	Weight per 1000 Feet.	
5 10 15 20 25 30 40 50 65 75 85	95-15-25-55-75-75-75-75-75-75-75-75-75-75-75-75	880 1 200 1 520 1 860 • 2 210 3 020 3 520 4 020 4 640 5 160 5 690 6 330	1 1 1 1 1 1 1 1 1 1 1 1 1 1 1 1 1 1 1	1 280 1 620 1 960 2 770 3 170 3 580 4 110 4 650 5 310 5 860 6 430 7 110	







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